



Clarence-Rockland

**CORPORATION OF THE CITY OF
CLARENCE-ROCKLAND
COMMITTEE OF THE WHOLE**

March 19, 2019, 8:00 pm
Council Chambers
415 rue Lemay Street, Clarence Creek, Ont.

Pages

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| 6. Notice of Motion | |
| 6.1 Notice of motion presented by Mayor Guy Desjardins regarding the Mayor's Golf Tournament | |
| 7. Comment/Question Period | |
| Note: Members of the public may come forward to the podium and after seeking permission from the Presiding Officer, shall state their name and direct their question/comment on any matter which is related to any item included in this agenda to the Presiding Officer. | |
| The maximum time allowed in all circumstances for a question/comment shall be three (3) minutes per person per meeting. There shall be a maximum of 30 minutes dedicated to the question/comment period. Any unasked questions/comments due to the time restriction may be submitted in writing to the Clerk. | |
| At no time shall this question period be taken by members of the audience to make speeches or accusations. | |
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Clarence-Rockland

**CORPORATION DE LA CITÉ DE
CLARENCE-ROCKLAND
COMITÉ PLÉNIER**

le 19 mars 2019, 20 h 00

Salle du Conseil
415 rue Lemay Street, Clarence Creek, Ont.

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| 7. | Période de Questions/Commentaires | |
| | Note: Les membres du public sont invités à se rendre au podium et après avoir reçu la permission du président de l'assemblée, doivent se nommer et adresser leur question et/ou commentaire sur tout sujet qui est relié à n'importe quel item qui figure à l'ordre du jour au président de réunion. Le temps maximal accordé pour une question/commentaire dans toutes circonstances est de trois (3) minutes par personne par réunion. Il y aura un maximum de 30 minutes consacrés à la période de questions/ commentaires. Toutes questions et/ou commentaires qui n'ont pas été adressés par faute de temps peuvent être soumis par écrit à la greffière. En aucun cas, cette période de questions/ commentaires ne peut être utilisée par les membres du public pour faire des discours ou porter des accusations. | |
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| 10. | Autres items | |
| 11. | Ajournement | |



Clarence-Rockland

Declaration of pecuniary interest Déclaration d'intérêt pécuniaire

| | |
|--|--|
| Date of meeting Date de la réunion: | |
| Item Number Numéro de l'item: | |
| Subject of the item: Sujet de l'item : | |
| Name of Council Member Nom du membre du conseil | |

I, _____, hereby declare a pecuniary interest in the matter identified above for the following reason :

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Je, _____, déclare un intérêt pécuniaire en ce qui concerne l'article ci-haut mentionné, pour la raison suivante :

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| |

| Name (print) | Signature | Date |
|--------------|-----------|------|
| | | |

This declaration is filed in accordance with the *Municipal Conflict of Interest Act* and will be recorded in the meeting minutes and will be made available in a public registry. / Cette déclaration est soumise sous la *Loi sur les conflits d'intérêt municipaux* et sera enregistrée dans le procès-verbal de la réunion et sera disponible dans un registre public.

Excerpt from the Municipal Conflict of Interest Act, R.S.O. 1990, c. M.50

DUTY OF MEMBER

When present at meeting at which matter considered

5 (1) Where a member, either on his or her own behalf or while acting for, by, with or through another, has any pecuniary interest, direct or indirect, in any matter and is present at a meeting of the council or local board at which the matter is the subject of consideration, the member,

- (a) shall, prior to any consideration of the matter at the meeting, disclose the interest and the general nature thereof;
- (b) shall not take part in the discussion of, or vote on any question in respect of the matter; and
- (c) shall not attempt in any way whether before, during or after the meeting to influence the voting on any such question. R.S.O. 1990, c. M.50, s. 5 (1).

Where member to leave closed meeting

(2) Where the meeting referred to in subsection (1) is not open to the public, in addition to complying with the requirements of that subsection, the member shall forthwith leave the meeting or the part of the meeting during which the matter is under consideration. R.S.O. 1990, c. M.50, s. 5 (2).

Extrait de la Loi sur les conflits d'intérêts municipaux, L.R.O. 1990, chap. M.50

OBLIGATIONS DU MEMBRE

Participation à une réunion où l'affaire est discutée

5 (1) Le membre qui, soit pour son propre compte soit pour le compte d'autrui ou par personne interposée, seul ou avec d'autres, a un intérêt pécuniaire direct ou indirect dans une affaire et participe à une réunion du conseil ou du conseil local où l'affaire est discutée, est tenu aux obligations suivantes :

- a) avant toute discussion de l'affaire, déclarer son intérêt et en préciser la nature en termes généraux;
- b) ne pas prendre part à la discussion ni voter sur une question relative à l'affaire;
- c) ne pas tenter, avant, pendant ni après la réunion, d'influencer de quelque façon le vote sur une question relative à l'affaire. L.R.O. 1990, chap. M.50, par. 5 (1).

Exclusion de la réunion à huis clos

(2) Si la réunion visée au paragraphe (1) se tient à huis clos, outre les obligations que lui impose ce paragraphe, le membre est tenu de quitter immédiatement la réunion ou la partie de la réunion où l'affaire est discutée. L.R.O. 1990, chap. M.50, par. 5 (2).

Le 4 mars 2019

Monsieur Guy Desjardins
Maire La Cité Clarence-Rockland
(Madame Maryse St-Pierre/ Greffière adjointe)
1560, rue Laurier
Rockland ON K4K 1P7

Objet : Gratuité de la salle communautaire de l'aréna de Clarence Creek

Monsieur Desjardins et membres du conseil,

Suite à la réception de la résolution 2019-35, nous constatons que vous nous permettez d'utiliser la salle communautaire de l'aréna de Clarence Creek à un tarif réduit. Par contre, malgré ce coût de location nous ne pourrions offrir le dîner communautaire mensuel aux citoyens de Clarence-Rockland.

Afin de permettre un coût raisonnable aux clients, il serait impératif d'avoir accès à la salle gratuitement. Certaines municipalités de la région de Prescott et Russell nous permettent l'accès à leur salle sans frais afin que la clientèle puisse participer aux dîners communautaires qui ont un mandat de socialisation, de réseautage et éducatif.

Nous nous demandons s'il serait possible de reconsidérer votre décision. Nous sommes disponibles à vous rencontrer et faire une présentation si vous le jugez opportun.

En vous remerciant de l'attention que vous porterez à cette demande.



Sylvie Leclair
Directrice générale



REPORT N° AMÉ-19-34-R

| | |
|---------------------|---|
| Date | 07/03/2019 |
| Submitted by | Claire Lemay |
| Subject | Zoning By-law Amendment – 600 du Golf Road – Hammond Golf |
| File N° | D-14-520 |

1) NATURE/GOAL :

The goal of this report is to present a Zoning By-law Amendment in order to add “food production” to the list of permitted uses for the property located on the north-east corner of Joanisse Road and du Golf Road. The property owner, 1618566 Ontario Inc. (Hammond Golf) has the intention of opening a small-scale micro-brewery associated with the restaurant in the golf club house if the amendment is approved.

2) DIRECTIVE/PREVIOUS POLICY :

N/A

3) DEPARTMENT'S RECOMMENDATION :

WHEREAS the proposed amendment to the City of Clarence-Rockland Zoning By-law for 600 du Golf Road is consistent with the Provincial Policy Statement and conforms to the Official Plan of the United Counties of Prescott and Russell;

THAT the Committee of the Whole recommends that Council adopts a By-law to amend Zoning By-law 2016-10, in order to add “food production” to the list of permitted uses in the zoning category “Tourist Commercial – Exception 2 (CT-2) Zone” in order to permit a micro-brewery, limited to 85m² floor area, as recommended by the Planning Committee.

ATTENDU QUE l'amendement proposé au Règlement de zonage de la Cité de Clarence-Rockland pour le 600 chemin du Golf est conforme à la Déclaration de principes provinciale et au Plan officiel des Comtés unis the Prescott et Russell;

QUE le Comité plénier recommande au Conseil Municipal d'adopter un règlement pour modifier le Règlement de Zonage 2016-10 afin d'ajouter « production alimentaire » à la liste des usages permis dans la catégorie de zonage « Zone commerciale touristique – Exception 2 (CT-2) » afin de permettre une micro-brasserie, restreint à une superficie de plancher de 85m², tel que recommandé par le Comité d'aménagement.

4) BACKGROUND :

Hammond Golf submitted an application for a zoning by-law amendment on February 14th, 2019 in order to permit a micro-brewery on the property of

the golf course at 600 du Golf Road (at the corner of du Golf and Joanisse). The property is serviced by private well and septic system.

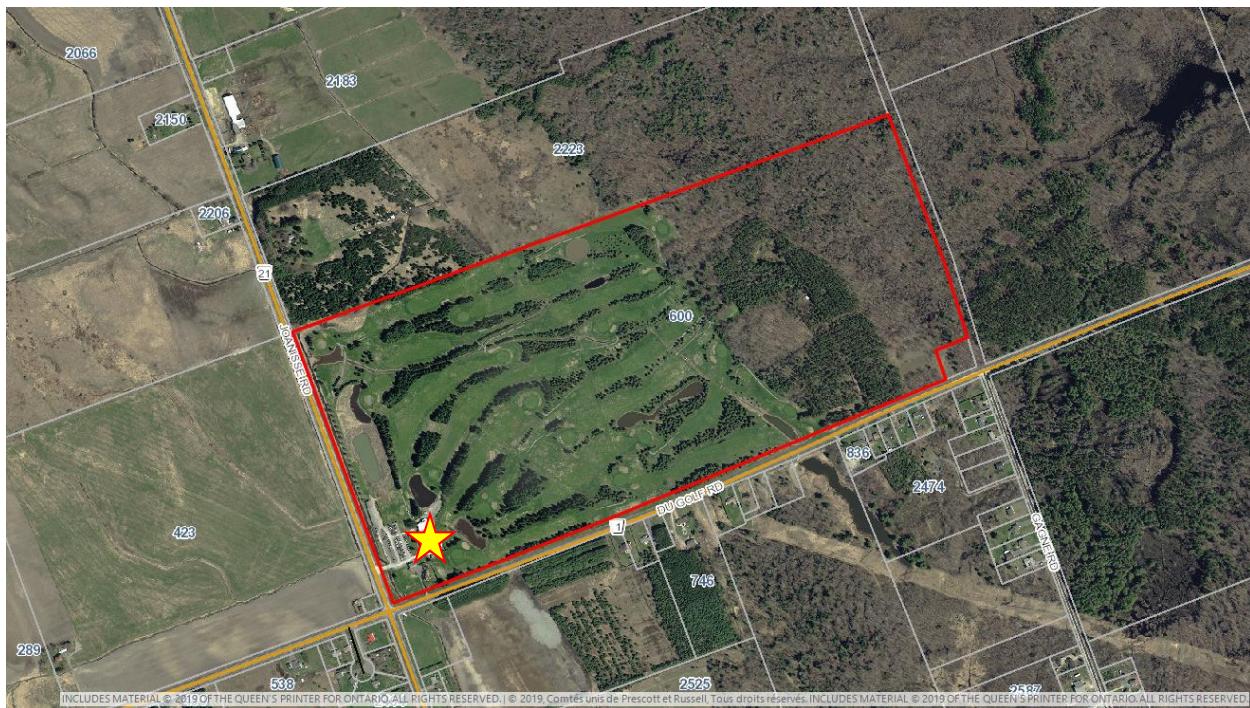


Figure 1: Location of subject property

Details of the proposal:

| | |
|---|---------------------------------------|
| Number of litres of water permitted to be used by the clubhouse: | 40,000 L/day |
| Number of barrels of beer proposed to be produced: | 7 barrels, 4 times per week |
| Number of litres of beer proposed to be produced: | 3284 L/week 170,768 L/year |
| Maximum number of litres possible within floor area restriction (7 batches/week): | 5,747 L/week 298,844 L/year |
| Floor area to be occupied by the micro-brewery use: | 900 square feet 83.6 square metres |

The proposed micro-brewery is small-scale and will be located entirely within the existing Clubhouse building. No addition to the existing Clubhouse building is proposed and no modifications to the parking area are required for this additional proposed use.

A copy of the golf course's permit to take water as well as the hydrogeological study and other background information regarding quantities of water used on the site have been provided to support the application.

The golf course already has a Permit to Take Water from the Ontario Ministry of Environment and the additional water use required for the proposed micro-brewery is within the quantity approved for this property. A total of 40,000L of water is permitted to be used per day by the Clubhouse according to the Permit to Take Water. The pump for the Clubhouse well cannot pump more than 28L/minute; therefore, it is not possible for the water consumption of the Clubhouse (including the proposed micro-brewery) to exceed the maximum permitted amount ($28 \times 60 \times 24 = 40,320$). Ongoing monitoring of test wells is required by the Ministry as part of the Permit to Take Water. Should water consumption exceed sustainable levels, the Ministry will take action to ensure the protection of local groundwater resources.

The existing septic system has sufficient capacity to accommodate the proposed micro-brewery use.

5) DISCUSSION : PROVINCIAL POLICY STATEMENT

The subject property is located on rural lands, as defined by the Provincial Policy Statement. Permitted uses on rural lands include "resource-based recreational uses" which includes the golf course and associated restaurant. Section 1.1.5.3 of the Provincial Policy Statement states that: "Recreational, tourism and other economic opportunities should be promoted." Adding a micro-brewery to the existing uses at the golf course club house is consistent with the goal of promoting tourism.

OFFICIAL PLAN OF THE UNITED COUNTIES OF PRESCOTT AND RUSSELL

The subject property is located within the "Rural Policy Area" according to Schedule A of the Official Plan of the United Counties of Prescott and Russell. "Tourism commercial uses" and "recreational commercial uses such as marinas, golf courses and campgrounds" are included in the list of permitted Commercial and Industrial Uses within the Rural Policy Area, as per section 2.5.3 of the Official Plan.

CITY OF CLARENCE-ROCKLAND ZONING BY-LAW 2016-10

The subject property is located in the "Tourist Commercial – Exception 2 (CT-2) Zone" according to Schedule A of the Zoning By-law 2016-10. Section 7.4.1 lists the permitted uses for the Tourist Commercial Zone, including: retail store, sports and recreation facility, restaurant, personal service establishment, place of entertainment, farmer's market, golf course, etc. The proposed amendment would modify section 7.4.3 (b) of the Zoning By-law 2016-10 in order to add "food production" to the list of permitted uses. Part 3 of the Zoning By-law defines "food production" as:

"a premises for the specialized production or preparation and packaging of a limited number of food and beverage products for sale to the public primarily for consumption off the premises such as catering establishments, make-your-own wine and beer establishments, test kitchens, bulk meal preparation, bakeries, and butchers"

It is the opinion of the Infrastructure and Planning Department that this defined use "food production" includes micro-breweries and micro-distilleries. The beverages produced on the site could then be sold or served through an associated retail store or restaurant, which are already permitted uses in the "Tourist Commercial – Exception 2 (CT-2) Zone".

In conclusion, the proposed amendment to the Zoning by-law is consistent with the Provincial Policy Statement and conforms to the Official Plan of the United Counties of Prescott and Russell. The proposed use of a micro-brewery on the property is desirable and in the public interest as it will increase tourism opportunities in the region.

6) CONSULTATION:

A public notice was sent to all property owners within 120m of the subject property and a notice was posted on the site on February 14th, 2019. A public meeting of the Planning Committee was held on March 6th, 2019, at which time members of the public had the opportunity to provide comments on the proposed amendment.

During the public meeting, the owner of the property at 2223 Joannis Road, located immediately to the north of the Golf Course lands, stated his objections to the proposed Zoning by-law amendment. His objections were primarily in relation to the quantity of water required for the micro-brewery and the potential impacts this proposed use might have on the quantity of water available in the wells of adjacent properties. He indicated that there have been water quantity issues in the past for his and another nearby property, which he believes are related to the golf course. He also voiced concerns regarding the potential future expansion of the proposed micro-brewery into a large-scale industrial use.

Members of the Planning Committee requested further information from the property owner and his partners in the proposed micro-brewery business regarding the proposed scale of the micro-brewery, water consumption, and septic system capacity. The following information was provided:

- The proposed micro-brewery consists of the re-opening of a small-scale micro-brewery previously located on Canotek Road in Ottawa.
- The proposed micro-brewery will produce three batches per week, with each batch consisting of 7 barrels (220 gallons).
- There are no plans to expand the micro-brewery beyond the scale currently proposed.
- The equipment required for the micro-brewery is very expensive and will therefore not be replaced or upgraded in the foreseeable future.

- This equipment is of a size to be able to fit in the existing clubhouse building. Any larger equipment which would be required if production were to be increased would not fit within the existing building.
- In preparing their business plan, the partners in the micro-brewery business set out to ensure that certain environmental criteria were met for their brewery, of which the re-use of water is a key component.
- Water used for the brewing process will be re-used multiple times before being treated and released back into the irrigation ponds for the golf course in order to ensure a minimal impact on the local water table.
- The partners had previously looked at a location in Cumberland for their micro-brewery, where they would have had to truck in water from outside sources for the business. This remains an option at the proposed location at the Hammond Golf Course if the micro-brewery's demand exceeds the amount they are permitted to use.
- The quantities of beer to be produced on site are suitable for on-site consumption in the associated restaurant but will not be exported for sale elsewhere.
- The golf course's permit to take water from the provincial Ministry of Environment requires ongoing testing and monitoring. Over the past 10 years, water levels have varied by less than 1.5m in the shallow aquifer and less than 0.5m in the deep aquifer.
- The capacity of the current septic system is adequate for the water to be discharged from the proposed micro-brewery; an additional filter is required.
- The Golf Course typically has between 25,000 and 30,000 rounds of golf played per year.

7) RECOMMENDATION FROM PLANNING COMMITTEE :

THAT the Planning Committee recommends to Committee of the Whole to recommend Council to amend Zoning By-law 2016-10, in order to add "food production" to the list of permitted uses in the zoning category "Tourist Commercial – Exception 2 (CT-2) Zone" in order to permit a micro-brewery once additional information has been provided.

QUE le Comité d'aménagement recommande au Comité plénier de recommander au Conseil Municipal d'approuver le règlement modifiant le Règlement de Zonage 2016-10 afin d'ajouter « production alimentaire » à la liste des usages permis dans la catégorie de zonage « Zone commerciale touristique – Exception 2 (CT-2) » afin de permettre une micro-brasserie une fois que des renseignements additionnels ont été fournis.

8) FINANCIAL IMPACT (expenses/material/etc.):

There are no direct financial implications associated with the approval of the zoning amendment. In the event the zoning amendment is refused and appealed, an external planner and external legal counsel would be retained.

9) LEGAL IMPLICATIONS :

In accordance with Bill 139, if the proposed zoning by-law is adopted, it can only be appealed to the Local Planning Appeals Tribunal on the basis of inconsistency with the Provincial Policy Statement or lack of conformity with the Official Plan. Were the zoning by-law appealed, the preparation of the necessary documentation for the Tribunal and the making of submissions to the Tribunal could be done within staff resources.

If the zoning amendment is refused, reasons must be provided. For an appeal of a refusal of a zoning application to succeed, the appellant must first show that the existing zoning is inconsistent with the Provincial Policy Statement and/or does not conform to the Official Plan. The City Clerk and Chief Administrative Officer would seek to retain an external planner to provide an affidavit in support of the refusal for the initial Tribunal review of the item should an appeal of the refusal be forthcoming. External legal counsel would also be retained to represent the City at the Tribunal.

10) RISK MANAGEMENT :

N/A

11) STRATEGIC IMPLICATIONS :

N/A

12) SUPPORTING DOCUMENTS:

By-law 2019-XX

RÈGLEMENT DE ZONAGE N° 2019-XX

Amendant le Règlement de zonage n° 2016-10

Corporation de la Cité de Clarence-Rockland

Partie du lot 10 concession 9
600 chemin du Golf
rédigé par

Cité de Clarence-Rockland
1560, rue Laurier
Rockland (Ontario)
K4K 1P7
(613) 446-6022

ZONING BY-LAW NO. 2019-XX

Amending Zoning By-Law No. 2016-10

The Corporation of the City of Clarence-Rockland

Part of Lot 10 Concession 9
600 du Golf Road

prepared by

City of Clarence-Rockland
1560 Laurier Street
Rockland, Ontario
K4K 1P7
(613) 446-6022

LA CORPORATION DE LA CITÉ DE CLARENCE-ROCKLAND

RÈGLEMENT N° 2019-XX

RÈGLEMENT AMENDANT LE RÈGLEMENT DE ZONAGE N° 2016-10;

ATTENDU QUE le Règlement de zonage n° 2016-10 réglemente l'utilisation des terrains, la construction et l'utilisation des bâtiments et structures sur le territoire de la Cité de Clarence-Rockland; et

ATTENDU QUE le Conseil de la Corporation de la Cité de Clarence-Rockland considère qu'il est opportun d'amender le Règlement de zonage n° 2016-10, tel qu'il suit;

PAR LA PRÉSENTE, le Conseil de la Corporation de la Cité de Clarence-Rockland donne force de loi à ce qui suit:

Article 1: La propriété décrite comme étant une partie du lot 10, concession 9, soit le 600 chemin du Golf, et identifiée à la cédule « A » ci-jointe, et faisant partie du présent règlement, est le terrain concerné par ce règlement.

Article 2: L'article 7.4.3 (b) du Règlement de zonage n. 2016-10, est par la présente modifiée pour lire comme suit :

« (b) CT-2, 600, chemin du Golf, partie du lot 10, concession 9

Nonobstant toute disposition contraire en vertu du présent Règlement, les terrains zonés CT-2 doivent être utilisés conformément aux dispositions ci-après :

(i) Utilisations additionnelles permises :

- Habitation isolée
- Production alimentaire

(ii) Superficie de plancher maximale pour production alimentaire : 85 m²

Article 3: Le présent règlement entrera en vigueur à la date de son adoption par le Conseil sous réserve de l'approbation du Tribunal ou suite à la date limite pour le dépôt des avis d'opposition, selon le cas.

FAIT ET ADOPTÉ EN RÉUNION PUBLIQUE, CE 19^{ÈME} JOUR DE MARS 2019.

Guy Desjardins, maire

Monique Ouellet, greffière

THE CORPORATION OF THE CITY OF CLARENCE-ROCKLAND

BY-LAW NO. 2019-XX

BEING A BY-LAW TO AMEND ZONING BY-LAW NO. 2016-10;

WHEREAS Zoning By-Law no. 2016-10 regulates the use of land, and the use and erection of buildings and structures in the City of Clarence-Rockland; and

WHEREAS the Council of the Corporation of the City of Clarence-Rockland considers appropriate to amend Zoning By-Law No. 2016-10, as described;

NOW THEREFORE, the Council of the Corporation of the City of Clarence-Rockland enacts as follows:

Section 1: The property described as part of Lot 10, Concession 9, 600 du Golf Road, identified on Schedule "A" attached to and forming part of this by-law shall be the lot affected by this by-law.

Section 2: Section 7.4.3 (b) of the Zoning By-law No. 2016-10 is hereby modified to read as follows:

"(b) CT-2, 600 du Golf Road, Part of Lot 10, Concession 9

Notwithstanding the provisions of this By-law to the contrary, the lands zoned CT-2 shall be used in accordance with the following provision(s):

(i) Additional permitted uses:

- detached dwelling
- food production

(ii) Maximum floor area for food production use: 85 m²

Section 3: This by-law shall become effective on the date of passing hereof, subject to the approval of the Tribunal or following the last date for filing objections as the case may be.

DATED AND PASSED IN OPEN COUNCIL, THIS 19TH DAY OF MARCH, 2019.

Guy Desjardins, Mayor

Monique Ouellet, Clerk

NOTE EXPLICATIVE

But et effet du Règlement

Le but du présent règlement consiste à modifier le Règlement de zonage n° 2016-10, afin d'ajouter la production alimentaire à la liste des utilisations permises afin de permettre une micro-brasserie.

Pour tous renseignements supplémentaires relativement à cette modification au Règlement de zonage n° 2016-10, veuillez communiquer avec Mme Claire Lemay, urbaniste municipale du Service d'infrastructure et aménagement du territoire à l'Hôtel de ville situé au 1560, rue Laurier ou par téléphone au numéro (613) 446-6022, poste 2267.

EXPLANATORY NOTE

Purpose and Effects of this By-Law

The purpose of the by-law is to amend Zoning By-Law No. 2016-10 in order to add food production to the list of permitted uses in order to permit a micro-brewery.

For further information concerning the amendment to Zoning By-Law No. 2016-10, you may contact Mrs. Claire Lemay, Municipal Planner for the Infrastructure and Planning Department, at the Town Hall, 1560 Laurier Street or by telephone at (613) 446-6022, ext. 2267.

CÉDULE « A » / SCHEDULE "A"



| | |
|---|--|
| <p> Terrains(s) touché(s) par ce règlement Area(s) affected by this by-law</p> <p>Certification d'authenticité Certificate of Authentification</p> <p>Ceci constitue le plan Cédule « A » du Règlement de zonage n° 2019-XX, adopté le 19 mars 2019.</p> <p>This is plan Schedule "A" to Zoning By-Law No. 2019-XX, passed the 19th day of March, 2019.</p> <p>Guy Desjardins, Maire / Mayor</p> | <p>Plan Cédule «A» du règlement n° 2019-XX</p> <p>Schedule "A" to By-Law No. 2019-XX</p> <p>600 du Golf Road</p> <p>600 chemin du Golf</p> <p>Cité de Clarence-Rockland City</p> <p>Préparé par/prepared by Cité de Clarence-Rockland City 1560, rue Laurier Street Rockland, Ontario K4K 1P7</p> <p>Pas à l'échelle/Not to scale</p> <p>Monique Ouellet, Greffière / Clerk</p> |
|---|--|



RAPPORT N° FIN 2019-009

| | |
|---------------------|---|
| Date | 11/03/2019 |
| Soumis par | Frédéric Desnoyers |
| Objet | État des transactions du fonds de réserve des redevances d'aménagement de l'année 2018/ Statement of development charges 2018 |
| # du dossier | Cliquez ici pour entrer du texte. |

1) **NATURE / OBJECTIF :**

Faire état des transactions du fonds de réserve des redevances d'aménagement de l'année 2018.

2) **DIRECTIVE/POLITIQUE ANTÉCÉDENTE :**

La section 18 du règlement 2010-47, étant un règlement pour imposer des frais de redevances d'aménagement, stipule que le (la) Trésorier (ère) de la municipalité doit remettre chaque année au Conseil de la municipalité, des états financiers sur les règlements de redevances d'aménagement et sur les fonds de réserve créés aux termes de l'article 33. 1997, chap. 27, par. 43 (1) de la Loi de 1997 sur les redevances d'aménagement.

3) **RECOMMANDATION DU SERVICE:**

ATTENDU QUE le Trésorier de la municipalité doit remettre chaque année au Conseil de la municipalité, des états financiers sur les règlements de redevances d'aménagement et sur les fonds de réserve créés aux termes de l'article 33. 1997, chap. 27, par. 43 (1) de la Loi de 1997 sur les redevances d'exploitation, par conséquent

QU'IL SOIT RÉSOLU que le conseil municipal de la Corporation de la Cité de Clarence-Rockland accepte l'état des fonds de réserve des redevances d'aménagement pour l'année 2018 tel que présenté dans le rapport FIN2019-009

WHEREAS the Treasurer of the municipality must submit annually to the Municipal Council, financial statements on development charge by-law and on reserve funds established under section 33. 1997, C. 27, para. 43(a) of the Development Charges Act, therefore

BE IT RESOLVED that the Municipal Council of the City of Clarence-Rockland accept the statement of development charges reserve funds for the 2018 year-end as presented in report FIN2019-009

4) **HISTORIQUE :**

Les redevances d'aménagement ont été approuvées en 2015 et, en vertu de la Loi sur les municipalités, nous devons produire des rapports à la province annuellement.

5) **DISCUSSION :**

Vous trouverez ci-joint l'état consolidé des fonds de réserve des redevances d'aménagement (résidentiels et non résidentiels) pour l'année 2018 et un sommaire :

CITÉ DE CLARENCE-ROCKLAND
Redevances d'aménagement - 2018

| | <u>Amount</u> |
|--------------------------------------|------------------|
| BALANCE DEC 31 2017 | <u>3,982,286</u> |
| <u>LEVIES COLLECTED</u> | |
| RESIDENTIAL - city wide charge | 104,043 |
| RESIDENTIAL - waterworks | 103,907 |
| RESIDENTIAL - fully serviced | 1,808,687 |
| NON - RESIDENTIAL - city wide charge | 0 |
| NON - RESIDENTIAL - waterworks | 0 |
| NON - RESIDENTIAL - fully serviced | <u>154,350</u> |
| TOTAL | <u>2,170,986</u> |
| INTEREST | 71,090 |
| Total levies collected and interest | <u>2,242,076</u> |
| <u>PROJECTS FINANCED</u> | |
| Total projects financed | 2,235,930 |
| BALANCE DEC 31, 2018 | <u>3,988,432</u> |

Le solde au 31 décembre 2018 était de 3 982 286 \$. Nous avons perçu 2 170 986\$ de redevances d'aménagement durant l'année et le fonds a généré 71 090 \$ d'intérêts pour un total de 2 242 076 \$ de revenus. Les projets financés au cours de l'année totalisent 2 235 930 \$. La balance des fonds de réserve des redevances d'aménagement totalise 3 988 432 \$ au 31 décembre 2018.

Selon le rapport FIN2017-023, une prévision de 175 nouvelles

constructions résidentielles a été établie.

En 2018 il y a eu 170 unités résidentielles pour lesquelles des redevances d'aménagement ont été collectées, comparativement à 184 en 2017.

En 2019, la nouvelle étude des redevances d'aménagement devra être complétée afin d'avoir un nouveau règlement effectif le 1er janvier 2020.

6) **CONSULTATION :**

N/A

7) **RECOMMANDATION OU COMMENTAIRES DU COMITÉ :**

N/A

8) **IMPACT FINANCIER (monétaire/matériaux/etc.):**

Le solde du fonds de réserve au 31 décembre 2018 est de 3 988 432 \$.

9) **IMPLICATIONS LÉGALES :**

N/A

10) **GESTION DU RISQUE (RISK MANAGEMENT) :**

N/A

11) **IMPLICATIONS STRATÉGIQUES :**

N/A

12) **DOCUMENTS D'APPUI:**

Schedule A – Sommaire des projets en capitaux 2018 dans le fond de redevances d'aménagement.

Schedule B - Redevances d'aménagement sommaire – 2018

Schedule C - Redevances d'aménagement 2018 – Résidentielle

Schedule D - Redevances d'aménagement 2018 - Non- Résidentielle

CORPORATION OF THE CITY OF CLARENCE-ROCKLAND

CONSOLIDATED STATEMENT OF TREASURER

Schedule A - Statement of Capital Fund Activity in 2018 of Development Charge related Projects

| Année/ Year | Compte/ Account | TITLE / TITRE | --- A --- Année a date/ Year To Date 31-12-2018 | Budget | FINANCEMENT (COLONNE "A") / FUNDING (COLUMN "A") | | | | | | | Unfinanced |
|----------------|--------------------|--------------------------------------|--|---------------|--|---|-----------------|-------------------------|-------------------------|-----------------|--------------|--------------|
| | | | | | Growth Dev. Charge | General Fund reserve Reserve -Fond général | Roads Routes | Planning Aménagement | Equipment Équipement | Federal Gas tax | Cash-In-Lieu | |
| 2017 | 2-4-2140-9221 | Rockland Fire Station Expansion | 1,022,058.95 | 3,534,135.00 | 322,921.34 | | | | | | | 699,137.61 |
| 2017 | 2-4-2140-9897 | Bourget New Fire station | 1,206,942.94 | 3,000,000.00 | 676,414.90 | | | | | | | 530,528.04 |
| 2016 | 2-4-3110-9626 | Municipal garage expansion | 202,766.70 | 707,394.00 | 152,447.13 | | | | 33,381.00 | | | 16,938.57 |
| 2018 | 2-4-3200-9279 | Caron Pond | 72,612.58 | 1,000,000.00 | 46,109.06 | | | | | | | 26,503.52 |
| 2018 | 2-4-3620-9195 | St-Jean Street (Sidewalk and lights) | 270,057.16 | 300,000.00 | 216,045.73 | | 54,011.43 | | | | | 0.00 |
| 2018 | 2-4-7250-9495 | Morris Village Park | 53,487.30 | 485,000.00 | 48,138.57 | | | | | 5,348.73 | | 0.00 |
| 2018 | 2-4-7250-9182 | Lavigne Park | 23,506.05 | 75,000.00 | 21,155.44 | | | | | | 2,351 | 0.00 |
| 2018 | 2-4-1220-9212 | Development Charge Study | 19,016.26 | 75,000.00 | 17,114.63 | 1,901.63 | | | | | | 0.00 |
| 2018 | 2-4-3200-9074 | Design Poupart Road | 101,760.07 | 100,000.00 | 80,000.00 | | 20,000.00 | 1,760.07 | | | | 0.00 |
| 2017 | 2-4-3200-9277 | St-Joseph Street | 9,709.21 | 2,514,902.00 | 9,709.21 | | | | | | | 0.00 |
| 2014 | 2-4-3260-9278 | Storm Sewer Master Plan | 116,790.40 | 400,000.00 | 93,432.32 | | 23,358.08 | | | | | 0.00 |
| 2017 | 2-4-3200-9898 | Master Transportation Plan | 36,553.24 | 100,000.00 | 36,553.24 | | | | | | | 0.00 |
| 2018 | 2-4-6110-9953 | Daycare equipment | 16,482.60 | 16,482.60 | 14,834.34 | 1,648.26 | | | | | | 0.00 |
| 2018 | 2-4-8110-9252 | Review of Official Plan - Urban Area | 2,784.15 | 30,000.00 | 1,252.87 | | | 1,531.28 | | | | 0.00 |
| 2014 | 2-4-8110-9282 | Secondary Plan | 90,539.02 | 250,000.00 | 81,847.27 | 8,691.75 | | | | | | 0.00 |
| Total | | | 3,245,066.63 | 12,587,913.60 | 1,817,976.05 | 12,241.64 | 97,369.51 | 3,291.35 | 33,381.00 | 5,348.73 | 2,350.61 | 1,273,107.74 |

CORPORATION OF THE CITY OF CLARENCE-ROCKLAND
CONSOLIDATED STATEMENT OF TREASURER
Schedule B - DEVELOPMENT CHARGES SUMMARY - 2018

| | TOTAL | General Government | Fire protection | P.W. Building / Equipment | P.W. Roads | P.W. Sewers | P.W. Waterworks | Recreation | Library | Daycare | By-Law | Transit | Engineering Studies | TOTAL |
|--------------------------------------|---------------------|--------------------|--------------------|---------------------------|---------------------|---------------------|-------------------|--------------------|------------------|-------------------|-------------------|------------------|---------------------|---------------------|
| BALANCE DEC 31 2017 | 3,982,285.92 | 83,549.42 | 54,259.97 | 190,086.90 | 1,311,326.84 | 2,085,385.45 | 271,077.44 | -526,414.69 | 38,483.88 | 353,018.26 | -27,070.44 | 63,469.20 | 85,113.68 | 3,982,285.91 |
| LEVIES COLLECTED | | | | | | | | | | | | | | |
| Per By-Law 2015-13 | | | | | | | | | | | | | | |
| RESIDENTIAL - city wide charge | 104,043.00 | 2,434.61 | 10,862.09 | 9,904.89 | 45,102.64 | 0.00 | 0.00 | 31,514.62 | 2,621.88 | 0.00 | 52.02 | 1,550.24 | 0.00 | 104,043.00 |
| RESIDENTIAL - waterworks | 103,907.00 | 2,182.05 | 9,725.70 | 8,863.27 | 40,367.87 | 0.00 | 10,785.55 | 28,210.75 | 2,348.30 | 0.00 | 41.56 | 1,381.95 | 0.00 | 103,907.00 |
| RESIDENTIAL - fully serviced | 1,808,686.60 | 23,874.66 | 106,350.77 | 96,945.60 | 441,500.40 | 672,107.94 | 118,107.23 | 308,381.07 | 25,683.35 | 0.00 | 542.61 | 15,192.98 | 0.00 | 1,808,686.61 |
| NON - RESIDENTIAL - city wide charge | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| NON - RESIDENTIAL - waterworks | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| NON - RESIDENTIAL - fully serviced | 154,349.76 | 2,515.90 | 11,144.05 | 10,171.65 | 46,227.75 | 70,290.88 | 12,378.85 | 0.00 | 0.00 | 0.00 | 30.87 | 1,589.80 | 0.00 | 154,349.76 |
| TOTAL | 2,170,986.36 | 31,007.21 | 138,082.61 | 125,885.41 | 573,198.66 | 742,398.82 | 141,271.63 | 368,106.44 | 30,653.53 | 0.00 | 667.06 | 19,714.97 | 0.00 | 2,170,986.37 |
| INTEREST | 71,090.00 | 3,517.29 | -6,894.71 | 11,791.49 | -3,276.81 | 57,654.52 | 6,145.00 | -9,663.09 | 651.40 | 5,975.36 | -355.27 | 2,103.78 | 3,441.05 | 71,090.00 |
| | 2,242,076.36 | 34,524.50 | 131,187.90 | 137,676.90 | 569,921.85 | 800,053.34 | 147,416.64 | 358,443.35 | 31,304.93 | 5,975.36 | 311.80 | 21,818.75 | 3,441.05 | 2,242,076.37 |
| PROJECTS FINANCED | | | | | | | | | | | | | | |
| Rockland Fire Station Expansion | 322,921.34 | - | 322,921.34 | - | - | - | - | - | - | - | - | - | - | 322,921.34 |
| Bourget New Fire station | 676,414.90 | - | 676,414.90 | - | - | - | - | - | - | - | - | - | - | 676,414.90 |
| Municipal garage expansion | 152,447.13 | - | - | 152,447.13 | - | - | - | - | - | - | - | - | - | 152,447.13 |
| Caron Pond | 46,109.06 | - | - | - | 46,109.06 | - | - | - | - | - | - | - | - | 46,109.06 |
| St-Jean Street (Sidewalk and lights) | 216,045.73 | - | - | - | 216,045.73 | - | - | - | - | - | - | - | - | 216,045.73 |
| Morris Village Park | 48,138.57 | - | - | - | - | - | - | 48,138.57 | - | - | - | - | - | 48,138.57 |
| Lavigne Park | 21,155.44 | - | - | - | - | - | - | 21,155.44 | - | - | - | - | - | 21,155.44 |
| Development Charge Study | 17,114.63 | 17,114.63 | - | - | - | - | - | - | - | - | - | - | - | 17,114.63 |
| Design Poupart Road | 80,000.00 | - | - | - | 80,000.00 | - | - | - | - | - | - | - | - | 80,000.00 |
| St-Joseph Street | 9,709.21 | - | - | - | 9,709.21 | - | - | - | - | - | - | - | - | 9,709.21 |
| Storm Sewer Master Plan | 93,432.32 | - | - | - | 93,432.32 | - | - | - | - | - | - | - | - | 93,432.32 |
| Master Transportation Plan | 36,553.24 | - | - | - | 36,553.24 | - | - | - | - | - | - | - | - | 36,553.24 |
| Daycare equipment | 14,834.34 | - | - | - | - | - | - | - | - | 14,834.34 | - | - | - | 14,834.34 |
| Review of Official Plan - Urban Area | 1,252.87 | 1,252.87 | - | - | - | - | - | - | - | - | - | - | - | 1,252.87 |
| Secondary Plan | 81,847.27 | 81,847.27 | - | - | - | - | - | - | - | - | - | - | - | 81,847.27 |
| sub-total | 1,817,976.05 | 100,214.78 | 999,336.24 | 152,447.13 | 481,849.56 | 0.00 | 0.00 | 69,294.01 | 0.00 | 14,834.34 | 0.00 | 0.00 | 0.00 | 1,817,976.05 |
| Loans and Other | | | | | | | | | | | | | | |
| Complexe debt payment | 99,579.34 | - | - | - | - | - | - | 99,579.34 | - | - | - | - | - | 99,579.34 |
| Clarence-Rockland Arena | 165,525.91 | - | - | - | - | - | - | 165,525.91 | - | - | - | - | - | 165,525.91 |
| Caron debt payment | 134,197.05 | - | - | - | 134,197.05 | - | - | - | - | - | - | - | - | 134,197.05 |
| Library - Books | 18,651.60 | - | - | - | - | - | - | - | 18,651.60 | - | - | - | - | 18,651.60 |
| Total Capital Expenses | 2,235,929.95 | 100,214.78 | 999,336.24 | 152,447.13 | 616,046.61 | 0.00 | 0.00 | 334,399.26 | 18,651.60 | 14,834.34 | 0.00 | 0.00 | 0.00 | 2,235,929.95 |
| BALANCE DEC 31, 2018 | 3,988,432.33 | 17,859.15 | -813,888.37 | 175,316.68 | 1,265,202.08 | 2,885,438.79 | 418,494.08 | -502,370.59 | 51,137.21 | 344,159.27 | -26,758.65 | 85,287.95 | 88,554.73 | 3,988,432.33 |

CORPORATION OF THE CITY OF CLARENCE-ROCKLAND
STATEMENT OF TREASURER
Schedule C - DEVELOPMENT CHARGES 2018 - Residential

Per By-Law 2015-13

| | | | | | | | | | | | | | |
|--------------------------------|---------|-------|--------|-------|--------|--------|--------|--------|-------|-------|-------|-------|-------|
| RESIDENTIAL - city wide charge | 100.00% | 2.34% | 10.44% | 9.52% | 43.35% | 0.00% | 0.00% | 30.29% | 2.52% | 0.00% | 0.05% | 1.49% | 0.00% |
| RESIDENTIAL - waterworks | 100.00% | 2.10% | 9.36% | 8.53% | 38.85% | 0.00% | 10.38% | 27.15% | 2.26% | 0.00% | 0.04% | 1.33% | 0.00% |
| RESIDENTIAL - fully serviced | 100.00% | 1.32% | 5.88% | 5.36% | 24.41% | 37.16% | 6.53% | 17.05% | 1.42% | 0.0% | 0.03% | 0.84% | 0.00% |

| | Eligible % | TOTAL | General Government | Fire protection | P.W. Building / Equipment | P.W. Roads | P.W. Sewers | P.W. Waterworks | Recreation | Library | Daycare | By-Law | Transit | Engineering Studies | TOTAL |
|--------------------------------|------------|--------------|--------------------|-----------------|---------------------------|--------------|--------------|-----------------|-------------|-----------|------------|------------|-----------|---------------------|--------------|
| BALANCE DEC 31, 2017 | | 3,942,933.53 | 61,083.68 | 137,721.95 | 98,497.38 | 1,583,435.60 | 1,846,569.97 | 254,449.26 | -518,373.67 | 38,483.88 | 353,018.26 | -28,170.10 | 52,472.12 | 63,745.19 | 3,942,933.52 |
| LEVIES COLLECTED | | | | | | | | | | | | | | | |
| NEW BY-LAW: | | | | | | | | | | | | | | | |
| RESIDENTIAL - city wide charge | | 104,043.00 | 2,434.61 | 10,862.09 | 9,904.89 | 45,102.64 | 0.00 | 0.00 | 31,514.62 | 2,621.88 | 0.00 | 52.02 | 1,550.24 | 0.00 | 104,043.00 |
| RESIDENTIAL - waterworks | | 103,907.00 | 2,182.05 | 9,725.70 | 8,863.27 | 40,367.87 | 0.00 | 10,785.55 | 28,210.75 | 2,348.30 | 0.00 | 41.56 | 1,381.95 | 0.00 | 103,907.00 |
| RESIDENTIAL - fully serviced | | 1,808,686.60 | 23,874.66 | 106,350.77 | 96,945.60 | 441,500.40 | 672,107.94 | 118,107.23 | 308,381.07 | 25,683.35 | 0.00 | 542.61 | 15,192.98 | 0.00 | 1,808,686.61 |
| TOTAL | | 2,016,636.60 | 28,491.31 | 126,938.56 | 115,713.76 | 526,970.91 | 672,107.94 | 128,892.78 | 368,106.44 | 30,653.53 | 0.00 | 636.19 | 18,125.17 | 0.00 | 2,016,636.61 |
| INTEREST | | 66,740.00 | 1,033.93 | 2,331.15 | 1,667.21 | 26,802.00 | 31,255.94 | 4,306.93 | -8,774.24 | 651.40 | 5,975.36 | -476.82 | 888.17 | 1,078.98 | 66,740.00 |
| TOTAL RECEIVED | | 2,083,376.60 | 29,525.25 | 129,269.71 | 117,380.98 | 553,772.91 | 703,363.88 | 133,199.71 | 359,332.20 | 31,304.93 | 5,975.36 | 159.37 | 19,013.34 | 1,078.98 | 2,083,376.61 |

PROJECTS FINANCED

| | | | | | | | | | | | | | | | |
|--------------------------------------|------|--------------|------------|------------|------------|------------|------------|-----------|------------|-----------|-----------|------|------|------|--------------|
| Rockland Fire Station Expansion | 88% | 284,170.78 | 284,170.78 | | | | | | | | | | | | 284,170.78 |
| Bourget New Fire station | 88% | 595,245.11 | 595,245.11 | | | | | | | | | | | | 595,245.11 |
| Municipal garage expansion | 88% | 134,153.47 | | | | 134,153.47 | | | | | | | | | 134,153.47 |
| Caron Pond | 88% | 40,575.97 | | | | | 40,575.97 | | | | | | | | 40,575.97 |
| St-Jean Street (Sidewalk and lights) | 88% | 190,120.24 | | | | | 190,120.24 | | | | | | | | 190,120.24 |
| Morris Village Park | 100% | 48,138.57 | | | | | | | | | | | | | 48,138.57 |
| Lavigne Park | 100% | 21,155.44 | | | | | | | | | | | | | 21,155.44 |
| Development Charge Study | 88% | 15,060.88 | 15,060.88 | | | | | | | | | | | | 15,060.88 |
| Design Poupart Road | 88% | 70,400.00 | | | | | 70,400.00 | | | | | | | | 70,400.00 |
| St-Joseph Street | 88% | 8,544.10 | | | | | | 8,544.10 | | | | | | | 8,544.10 |
| Storm Sewer Master Plan | 88% | 82,220.44 | | | | | | 82,220.44 | | | | | | | 82,220.44 |
| Master Transportation Plan | 88% | 32,166.85 | | | | | | 32,166.85 | | | | | | | 32,166.85 |
| Daycare equipment | 100% | 14,834.34 | | | | | | | | | | | | | 14,834.34 |
| Review of Official Plan - Urban Area | 88% | 1,102.52 | 1,102.52 | | | | | | | | | | | | 1,102.52 |
| Secondary Plan | 88% | 72,025.60 | 72,025.60 | | | | | | | | | | | | 72,025.60 |
| Loans and Other | | | | | | | | | | | | | | | 0.00 |
| Complexe debt payment * | 100% | 99,579.34 | | | | | | | 99,579.34 | | | | | | 99,579.34 |
| Clarence-Rockland Arena * | 100% | 165,525.91 | | | | | | | 165,525.91 | | | | | | 165,525.91 |
| Caron debt payment | 88% | 118,093.40 | | | | | 118,093.40 | | | | | | | | 118,093.40 |
| Library - Books | 100% | 18,651.60 | | | | | | | 18,651.60 | | | | | | 18,651.60 |
| Total Capital Expenses | | 2,011,764.58 | 88,189.00 | 879,415.89 | 134,153.47 | 542,121.02 | 0.00 | 0.00 | 334,399.26 | 18,651.60 | 14,834.34 | 0.00 | 0.00 | 0.00 | 2,011,764.58 |

| | | | | | | | | | | | | | | |
|----------------------|--------------|----------|-------------|-----------|--------------|--------------|------------|-------------|-----------|------------|------------|-----------|-----------|--------------|
| Balance Dec 31, 2018 | 4,014,545.55 | 2,419.93 | -612,424.24 | 81,724.88 | 1,595,087.50 | 2,549,933.84 | 387,648.98 | -493,440.72 | 51,137.21 | 344,159.27 | -28,010.73 | 71,485.46 | 64,824.17 | 4,014,545.55 |
|----------------------|--------------|----------|-------------|-----------|--------------|--------------|------------|-------------|-----------|------------|------------|-----------|-----------|--------------|

CORPORATION OF THE CITY OF CLARENCE-ROCKLAND

STATEMENT OF TREASURER

Schedule D - DEVELOPMENT CHARGES 2018 - Non-Residential

Per By-Law 2015-13

| | | | | | | | | | | | | |
|--------------------------------------|---------|-------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|
| NON - RESIDENTIAL - city wide charge | 100.00% | 3.51% | 15.55% | 14.18% | 64.49% | 0.00% | 0.00% | 0.00% | 0.00% | 0.05% | 2.22% | 0.00% |
| NON - RESIDENTIAL - waterworks | 100.00% | 2.99% | 13.26% | 12.09% | 55.00% | 0.00% | 14.72% | 0.00% | 0.00% | 0.05% | 1.89% | 0.00% |
| NON - RESIDENTIAL - fully serviced | 100.00% | 1.63% | 7.22% | 6.59% | 29.95% | 45.54% | 8.02% | 0.00% | 0.00% | 0.02% | 1.03% | 0.00% |

| | Eligible % | TOTAL | General Government | Fire protection | P.W. Building / Equipment | P.W. Roads | P.W. Sewers | P.W. Waterworks | Recreation | Library | Daycare | By-Law | Transit | Engineering Studies | TOTAL |
|----------------------|------------|-----------|--------------------|-----------------|---------------------------|-------------|-------------|-----------------|------------|---------|---------|----------|-----------|---------------------|-----------|
| BALANCE DEC 31, 2017 | | 39,352.39 | 22,465.74 | -83,461.98 | 91,589.53 | -272,108.76 | 238,815.48 | 16,628.18 | -8,041.02 | 0.00 | 0.00 | 1,099.66 | 10,997.07 | 21,368.49 | 39,352.39 |

LEVIES COLLECTED

NEW BY-LAW:

| | | | | | | | | | | | | | | |
|--------------------------------------|-------------------|-----------------|------------------|------------------|------------------|------------------|------------------|----------------|-------------|--------------|-----------------|-----------------|-----------------|-------------------|
| NON - RESIDENTIAL - city wide charge | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| NON - RESIDENTIAL - waterworks | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| NON - RESIDENTIAL - fully serviced | \$154,349.76 | 2,515.90 | 11,144.05 | 10,171.65 | 46,227.75 | 70,290.88 | 12,378.85 | 0.00 | 0.00 | 30.87 | 1,589.80 | 0.00 | 0.00 | 154,349.76 |
| TOTAL | 154,349.76 | 2,515.90 | 11,144.05 | 10,171.65 | 46,227.75 | 70,290.88 | 12,378.85 | 0.00 | 0.00 | 30.87 | 1,589.80 | 0.00 | 0.00 | 154,349.76 |
| INTEREST | 4,350.00 | 2,483.36 | -9,225.86 | 10,124.28 | -30,078.81 | 26,398.58 | 1,838.07 | -888.85 | 0.00 | 0.00 | 121.56 | 1,215.61 | 2,362.07 | 4,350.00 |
| TOTAL RECEIVED | 158,699.76 | 4,999.26 | 1,918.19 | 20,295.93 | 16,148.94 | 96,689.46 | 14,216.92 | -888.85 | 0.00 | 0.00 | 152.43 | 2,805.42 | 2,362.07 | 158,699.76 |

PROJECTS FINANCED

| | | | | | | | | | | | | | | |
|--------------------------------------|-----|-----------|-----------|-----------|-----------|-----------|------|--|--|--|--|--|--|-----------|
| Rockland Fire Station Expansion | 12% | 38,750.56 | 38,750.56 | | | | | | | | | | | 38,750.56 |
| Bourget New Fire station | 12% | 81,169.79 | 81,169.79 | | | | | | | | | | | 81,169.79 |
| Municipal garage expansion | 12% | 18,293.66 | | 18,293.66 | | | | | | | | | | 18,293.66 |
| Caron Pond | 12% | 5,533.09 | | | 5,533.09 | | | | | | | | | 5,533.09 |
| St-Jean Street (Sidewalk and lights) | 12% | 25,925.49 | | | | 25,925.49 | | | | | | | | 25,925.49 |
| Morris Village Park | 0% | 0.00 | | | | | 0.00 | | | | | | | 0.00 |
| Lavigne Park | 0% | 0.00 | | | | | 0.00 | | | | | | | 0.00 |
| Development Charge Study | 12% | 2,053.76 | 2,053.76 | | | | | | | | | | | 2,053.76 |
| Design Poupart Road | 12% | 9,600.00 | | | 9,600.00 | | | | | | | | | 9,600.00 |
| St-Joseph Street | 12% | 1,165.11 | | | 1,165.11 | | | | | | | | | 1,165.11 |
| Storm Sewer Master Plan | 12% | 11,211.88 | | | 11,211.88 | | | | | | | | | 11,211.88 |
| Master Transportation Plan | 12% | 4,386.39 | | | 4,386.39 | | | | | | | | | 4,386.39 |
| Daycare equipment | 0% | 0.00 | | | | | | | | | | | | 0.00 |
| Review of Official Plan - Urban Area | 12% | 150.34 | 150.34 | | | | | | | | | | | 150.34 |
| Secondary Plan | 12% | 9,821.67 | 9,821.67 | | | | | | | | | | | 9,821.67 |

Loans and Other

| | | | | | | | | | | | | | | | |
|-----------------------------|-----|-------------------|------------------|--------------------|------------------|--------------------|-------------------|------------------|------------------|-------------|-------------|-----------------|------------------|------------------|-------------------|
| Complex debt payment | 0% | 0.00 | | | | 0.00 | | | | | | | | 0.00 | |
| Clarence-Rockland Arena | 0% | 0.00 | | | | 0.00 | | | | | | | | 0.00 | |
| Caron debt payment | 12% | 16,103.65 | | | 16,103.65 | | | | | | | | | 16,103.65 | |
| Library - Books | 0% | 0.00 | | | | | 0.00 | | | | | | | 0.00 | |
| Total Expenses | | 224,165.37 | 12,025.77 | 119,920.35 | 18,293.66 | 73,925.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 224,165.37 | |
| BALANCE DEC 31, 2018 | | -26,113.22 | 15,439.22 | -201,464.13 | 93,591.80 | -329,885.41 | 335,504.95 | 30,845.10 | -8,929.87 | 0.00 | 0.00 | 1,252.08 | 13,802.49 | 23,730.56 | -26,113.22 |



RAPPORT N° AMÉ-19-33-R

| | |
|---------------------|---|
| Date | 07/03/2019 |
| Soumis par | Claire Lemay |
| Objet | Modification au Règlement de Zonage – 733 rue Industrielle – Kimberle Herold pour RANN Enterprises Inc. |
| # du dossier | D-14-518 |

1) **NATURE / OBJECTIF :**

Le but de ce rapport est de présenter une demande de modification au Règlement de Zonage pour l’édifice située au 733 rue Industrielle à Rockland. La demande est pour ajouter une garderie à la liste des usages permis pour cette propriété.

2) **DIRECTIVE/POLITIQUE ANTÉCÉDENTE :**

S/O

3) **RECOMMANDATION:**

THAT the Committee of the Whole recommend that Municipal Council adopt a By-law to amend Zoning by-law 2016-10 in order to change the zoning category of the subject property from “General Industrial (MG) Zone” to “General Industrial – Exception 5 (MG-5) Zone” in order to permit a daycare as principal use, as recommended by the Planning Committee.

QUE le Comité plénier recommande au Conseil municipale d’adopter un règlement pour modifier le règlement de zonage 2016-10 afin de changer la catégorie de zonage du terrain visé de « Zone d’industrie générale (MG) » à « Zone d’industrie générale – exception 5 (MG-5) » afin de permettre une garderie comme usage principal, tel que recommander par le Comité d’aménagement.

4) **HISTORIQUE :**

Une demande complète de modification au Règlement de zonage 2016-10 fut soumise à la Cité de Clarence-Rockland le 21 janvier 2019 pour la propriété située au 729, 731, et 733 rue Industrielle. Le demandeur a l’intention d’ouvrir une garderie dans un édifice existant (le 733 rue Industrielle) dans le parc industriel de Rockland. La garderie proposée accomoderait des nourrissons, des bambins, des enfants d’âge préscolaire, ainsi que des enfants de l’âge scolaire avant et après l’école.

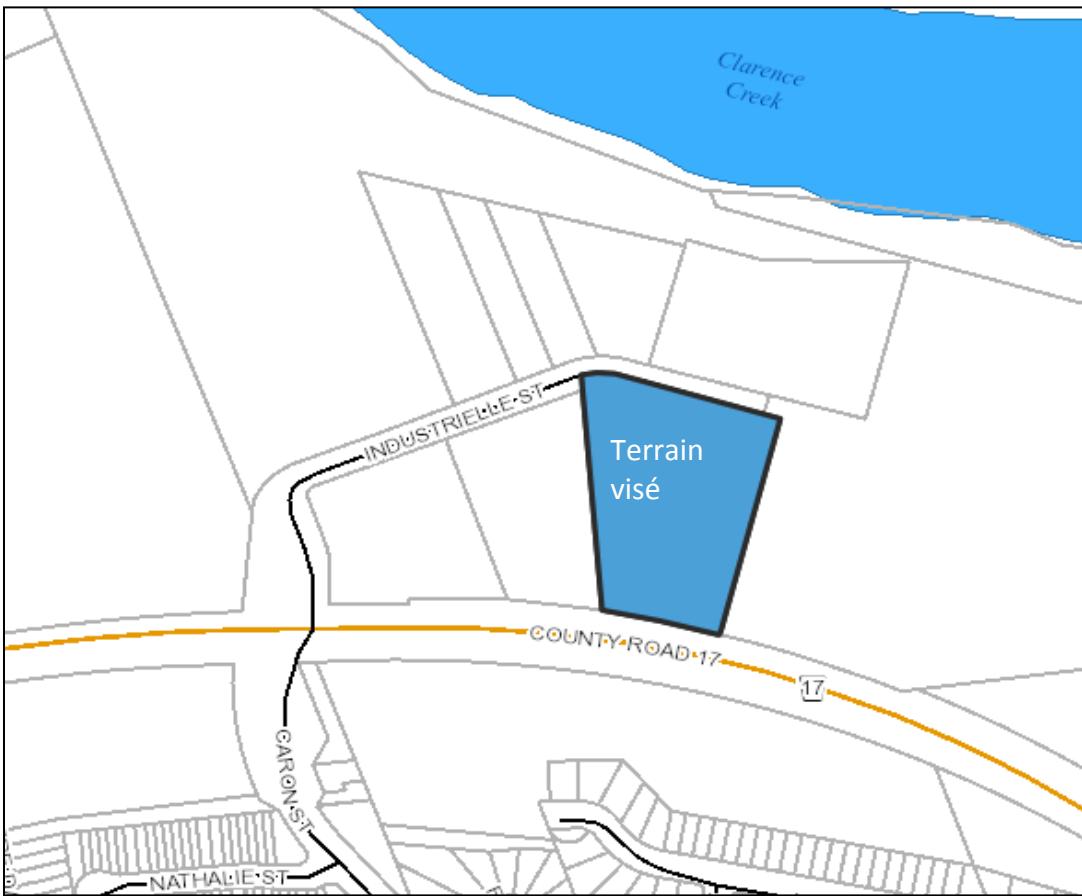


Figure 1 : Emplacement de la propriété sujette à la demande



Figure 2 : Bâtiment sujet à la demande (recommandation du Comité d'aménagement)

5) DISCUSSION :
DECLARATION DE PRINCIPES PROVINCIALE

Le terrain visé est situé dans une zone de peuplement. L'article 1.1.1 de la Déclaration de principes provinciale stipule que :

« Pour assurer l'existence de collectivités saines et sûres, où il fait bon vivre, il faut [...] permettre un éventail et une diversité appropriés d'utilisations à des fins résidentielles [...], institutionnelles (p. ex., lieux de culte, cimetières, foyers de soins de longue durée), de loisirs, d'espaces verts et de plein air et autres pour répondre aux besoins à long terme [...] ».

L'article 1.2.6 de la Déclaration de principes provinciale stipule que :

« Les *grandes installations* et les *utilisations sensibles du sol* doivent être conçues de façon appropriée, dotées de zones tampons ou séparées les unes des autres de manière à éviter ou à atténuer les *conséquences préjudiciables* des odeurs, du bruit et d'autres contaminants, à réduire au minimum les risques pour la santé et la sécurité publiques et à garantir la viabilité à long terme des *grandes installations*. »

Des « *grandes installations* » sont définies comme étant des « Installations qui doivent, dans certains cas, être séparées des *utilisations sensibles du sol*, notamment [...], les installations de traitement des eaux usées [...], les industries [...] » etc.

Les « *utilisations sensibles du sol* » sont définies comme étant des :

« bâtiments, aires d'agrément ou espaces extérieurs où des activités habituelles ou normales se déroulant à des moments raisonnablement prévisibles subiraient une ou plusieurs *conséquences préjudiciables* en raison du rejet de polluants provenant d'une *installation importante* située à proximité. Les *utilisations sensibles du sol* peuvent faire partie de l'environnement naturel ou bâti. Les résidences, les garderies et les établissements scolaires ou de soins de santé en sont des exemples. »

Il y a plusieurs usages industriels ainsi que la station d'épuration des eaux usées de Clarence-Rockland sur les terrains adjacents au terrain visé.

PLAN OFFICIEL DES COMTÉS UNIS DE PRESCOTT-RUSSELL

L'article 2.2.9 – Politiques de développement industriel du Plan officiel des Comtés unis de Prescott et Russell permet des usages industriels dans l'aire urbaine. De plus, la politique numéro 6 stipule que :

« Les conseils locaux doivent s'efforcer de maintenir le caractère et l'ampleur du développement industriel et s'assurer un contrôle approprié. La révision du développement du site et le développement des règlements de zonage doivent aborder ceci :

- a) Permettre une diversité d'usages industriels;
- b) Identifier les zones industrielles dans des secteurs sélectionnés des municipalités qui sont bien à l'écart des secteurs résidentiels et centre-ville ou qui peuvent être

développé dans une manière qui ne provoquera pas des conflits conformément aux Lignes directrices sur la compatibilité entre installations industrielles et utilisations sensibles du sol du Ministère de l'Environnement et changement climatique;

- c) S'assurer la protection des éléments de patrimoine naturel. »

L'établissement d'une garderie dans le parc industriel pourrait empêcher des commerces futurs de s'établir sur le terrain visé ou sur des terrains avoisinants à cause des conflits potentiels avec l'utilisation sensible (la garderie). Par exemple, d'autres commerces qui seraient considérés comme des usages industriels de catégorie I qui sont autrement permis dans le parc industriel à Rockland, ne pourraient pas s'installer sur le terrain visé ou les terrains avoisinants. Ces usages potentiels incluent la production de cannabis, l'entreposage, et la fabrication. Il n'y a pas présentement d'autre endroit dans les environs de Rockland où ces usages sont permis.

PLAN OFFICIEL DE L'AIRE URBAINE DE LA CITÉ DE CLARENCE-ROCKLAND

L'article 5.3 du Plan officiel de l'aire urbaine stipule que : « Certains usages commerciaux dans le parc d'affaires seraient souhaitables, pourvu qu'ils soient mineurs et connexes à l'usage principal du parc d'affaires. » La garderie proposée n'est pas connexe à un usage principal du parc d'affaires et n'est pas mineure.

L'article 5.3.1 du Plan officiel de l'aire urbaine décrit les usages permis dans le secteur Parc d'affaires.

« Les usages permis dans la zone désignée parc d'affaires comprendront toutes les formes d'usages liées à l'industrie légère qui sont compatibles avec les usages dans les zones avoisinantes, qui ne créent pas de nuisance attribuable au bruit, aux odeurs, aux vibrations, à la poussière ou à la fumée, y compris les établissements d'entreposage et de vente en gros, les manufactures, les installations de traitement, de montage et d'emballage, les installations de recherche, les ateliers d'imprimerie, les bureaux commerciaux ou professionnels, les installations récréatives intérieures et tous les usages liés au commerce autoroutier permis dans la zone désignée de commerce de services. »

L'article 4.14 du Plan officiel de l'aire urbaine stipule que :

« Les impacts du bruit et des odeurs devraient être considérés en rapport à tout nouvel usage sensible des terrains adjacents à des routes, des installations de traitement d'eaux usées, des industries ou autres sources fixes ou linéaires, où le bruit et les odeurs peuvent être générés. »

Une étude de bruit et/ou odeurs peut être exigée afin d'identifier les effets potentiels et de suggérer des mesures d'atténuation.

RÈGLEMENT DE ZONAGE 2016-10 DE LA CITÉ DE CLARENCE-ROCKLAND

Le terrain visé est situé dans la « Zone d'industrie générale (MG) ». Une garderie est permise, sujet aux restrictions suivantes :

- La garderie est accessoire à une utilisation permise
- La *surface de plancher nette* maximum doit être la moindre d'une surface de plancher nette maximum correspondant à 15 % de la surface de plancher nette de l'*utilisation* principale ou 200 m²; et,
- L'*utilisation* doit être confinée à l'intérieur des mêmes locaux que l'*utilisation permise* associée.

Des usages industriels légers et des usages de véhicule motorisés sont permis dans la zone d'industrie générale. Les usages de véhicules motorisés tel que des ateliers de carrosserie ou ateliers de réparations de véhicules motorisés ne sont pas permis à côté d'une zone résidentielle, afin de réduire le potentiel de conflit entre les usages. Aucune restriction existe présentement dans le zonage pour réduire des conflits entre les usages de véhicules motorisées et les autres utilisations de sol sensibles comme des garderies. Approuver une garderie sur le même terrain que des ateliers de carrosserie et de réparation de véhicules motorisés n'est pas recommandé comme étant une bonne pratique de l'aménagement du territoire.

L'article 4.42 - Distances de séparation du règlement de zonage 2016-10 stipule que :

« a) Nonobstant toute disposition contraire du présent Règlement, les nouvelles utilisations sensibles comme les logements, les garderies, les maisons de retraite, etc. seront interdites dans les emplacements ci-après :

- [...]
- À moins de 20 m de toute utilisation industrielle de catégorie I;
- À moins de 70 m de toute utilisation industrielle de catégorie II;
- À moins de 300 m de toute utilisation industrielle de catégorie III;

[...]

c) Nonobstant l'alinéa a) ci-dessus, les distances de séparation entre les utilisations industrielles ou les utilisations de granulat minéral et les utilisations sensibles de terrain (et vice versa) peuvent être réduites par un changement de zonage ou une dérogation mineure. Toute demande visant à réduire la distance de séparation doit être soutenue par des études appropriées (sur le bruit, les odeurs, les vibrations, etc.), et des mesures d'atténuation doivent démontrer qu'il n'y aura aucun impact négatif sur l'utilisation des terrains sensibles ou les utilisations à

des fins d'exploitation industrielle ou d'exploitation de granulat minéral. »

Ces distances de séparation sont mesurées de la ligne de propriété de l'utilisation du sol sensible à la ligne de propriété de l'utilisation industrielle.

Une utilisation industrielle légère de catégorie I est définie comme suit :

« un lieu d'activités sur lequel une usine ou un bâtiment indépendant produit, fabrique, assemble ou entrepose, à petite échelle, un produit contenu dans un emballage présentant une faible probabilité d'émissions fugitives, (bruits, odeurs, poussière, vibrations, etc.). Ces industries opèrent durant la journée seulement, exécutent peu fréquemment le déplacement de produits ou de camions lourds, et ne disposent pas d'entreposage extérieur. À titre d'exemples dans cette catégorie d'industrie, on retrouve la fabrication et la réparation de produits électroniques, les industries de haute technologie, la réparation et la restauration de meubles, l'embouteillage de boissons, les services d'emballage, les services d'artisanat, l'assemblage à petite échelle et la fourniture de pièces motorisées. Une utilisation industrielle légère ne nécessite pas de permis de prélèvement d'eau (PPE). »

Les usages suivants, qui sont tous permis dans la Zone d'industrie générale (MG) dans laquelle se situe le terrain visé, pourraient être classifiés comme des usages industriels de catégorie I :

- *Production alimentaire*
- *Atelier de fabrication sur commande*
- *Atelier de réparations*
- *Entreposage*
- *Entreposage à l'extérieur*
- *Fabrication*
- *Impression et imprimerie*
- *Installation de nettoyeur à sec*
- *Installation de production de cannabis*
- *Installation de stockage en vrac*
- *Installation d'un entrepreneur*
- *Traitements à l'extérieur*
- *Vente en gros et distribution*

Sur le terrain visé, il y a trois bâtiments existants, dont celui au 733 rue Industrielle qui est présentement utilisé par un commerce de golf virtuel, un atelier de réparation et l'unité vacante d'où la garderie serait située si autorisée. Le 729 rue Industrielle est utilisée pour un atelier de réparation de véhicules motorisés, un atelier de carrosserie pour véhicules motorisés, et un centre de conditionnement physique. L'édifice au 731 rue Industrielle était utilisé par ATG Industries (usage de fabrication). Les unités à louer dans ces trois édifices pourraient accommoder des usages industriels de

catégorie I dans le futur, d'après les politiques du règlement de zonage et du Plan officiel actuellement en vigueur.

Si l'amendement proposé est approuvé pour permettre une garderie sur le terrain visé, les unités au 729, 731, et 733 rue Industrielle ne pourront pas être utilisées pour des nouveaux usages industriels de catégorie I.

À l'ouest du terrain visé, au 701 rue Industrielle, l'édifice est occupé par Pack All Manufacturing. Les usages actuels sur le terrain incluent la fabrication et l'entreposage. Ce commerce est classifié comme usage industriel léger de catégorie I. La distance de séparation minimale requise par le règlement de zonage entre cet usage et une garderie ou autre usage sensible proposés est de 20m. Le terrain situé au 701 rue Industrielle partage une ligne de propriété avec le terrain visé; la distance minimale de séparation n'est pas respectée. Aucun nouvel usage industriel léger de catégorie I ne pourra s'installer au 701 rue Industrielle si l'amendement proposé est approuvé.

Au nord de la rue Industrielle, la Cité de Clarence-Rockland utilise une parcelle de terrain pour l'entreposage de neige. Une autre parcelle au nord de la rue Industrielle mais plus à l'ouest, est le site de la station d'épuration des eaux usées de Clarence-Rockland. La station d'épuration crée des odeurs déplaisantes. La ligne directrice D-2 du Ministère de l'Environnement, de la protection de la nature et des parcs de l'Ontario recommande une distance minimale de séparation de 150 mètres entre un réseau de traitement des eaux usées et des utilisations de sol fragile (tel qu'une garderie). La distance actuelle de 170 mètres (mesuré de la ligne de propriété du terrain visé au bâtiment de la station de traitement des eaux usées) n'est peut-être pas suffisante pour éviter que les enfants de la garderie proposée, lors de leur temps de jeu extérieur, ne sentent pas les odeurs de la station d'épuration des eaux usées. Une étude de bruit et odeur pourrait déterminer si la distance actuelle entre les bâtiments est suffisante et identifier des mesures d'atténuation, si nécessaires. De plus, tout futur agrandissement de la station de traitement des eaux usées pourrait être affecté à cause de la distance minimale de séparation. La distance entre les deux lignes de propriété est seulement 90 mètres.

Également, au nord de la rue Industrielle, plus à l'ouest, au 710 et au 720 rue Industrielle, l'usage est de l'entreposage, qui pourrait être classifié comme un usage industriel léger de catégorie I. Au 730 rue Industrielle, l'édifice est occupé par Pilon Fasteners; les usages actuels sur le terrain incluent la fabrication et l'entreposage. Vers l'est, le 760 rue Industrielle est appartenue et utilisé par ATG Industries. Ces deux commerces sont classifiés comme usages industriels légers de catégorie I. La distance de séparation minimale requise par le règlement de zonage entre ces usages et une garderie ou autre usage sensible proposé est de 20m. La distance entre la ligne de propriété du terrain visé et la ligne de propriété du 760 rue Industrielle et à la ligne de propriété du 730 rue Industrielle est 26 mètres.

La distance minimale de séparation est respectée.

Le terrain à l'est du terrain visé est utilisé par l'académie de hockey CIH. Cet usage n'a pas de conflit potentiel avec la garderie proposée.

Si la Cité de Clarence-Rockland décide dans le futur de détacher d'autres terrains dans le parc industriel et si l'amendement proposé est approuvé, ces terrains ne pourront peut-être pas être utilisés pour des usages industriels légers de catégorie I à cause du conflit potentiel avec la garderie.

Aucune étude n'a été soumise pour démontrer que les usages industriels situés sur le terrain visé ou sur les terrains adjacents n'auront pas d'impact négatif sur la garderie proposée et vice versa.

Il y a suffisamment de stationnements sur le terrain visé pour accommoder les usages existants et la garderie proposée. Le nombre d'espaces de stationnement requis est calculé pour tout le terrain au complet, et non pas pour chaque unité ou pour chaque bâtiment.

Un plan préliminaire pour l'aire de jeu extérieur et pour l'aménagement intérieur de la garderie a été soumis et est inclus avec ce rapport. Des révisions au plan proposé seront nécessaires afin de satisfaire des commentaires et inquiétudes du Département d'infrastructures et aménagement du territoire par rapport à la sécurité des enfants et le stationnement. Une révision aux dessins et la signature d'un amendement à l'Entente de plan d'implantation, ainsi qu'un permis de construction pour le changement d'usage, seront nécessaire afin de finaliser l'approbation municipale de cet usage proposé. L'approbation du Ministère de l'Éducation est également nécessaire.

CONCLUSION

En conclusion, le Département d'infrastructures et aménagement du territoire ne recommande pas l'approbation de la modification au Règlement de zonage proposée. Permettre une garderie dans le bâtiment du 733 rue Industrielle pourrait avoir l'effet d'interdire des usages industriels légers sur le terrain visé et les terrains adjacents du parc industriel. De plus, les impacts potentiels des usages industriels légers existants et futurs sur le terrain visé et le terrain adjacent ainsi que les impacts potentiels de la station d'épuration des eaux usées sur la garderie proposée n'ont pas été identifiés. La demande n'est pas conforme au Plan officiel des Comtés unis en raison qu'elle aurait l'effet d'interdire des futurs usages industriels dans la seule partie de Rockland où les usages industriels sont permis d'après le Plan officiel de l'aire urbaine et le Règlement de zonage, contrairement aux politiques de l'article 2.2.9. L'amendement proposé n'est pas conforme au Plan officiel de l'aire urbaine en raison que l'usage commercial proposé n'est pas mineur ni connexe à un usage principal dans le parc d'affaires.

6) CONSULTATION :

Un avis public a été envoyé aux propriétaires des terrains à 120 mètres de la propriété visée et un avis a été érigé sur le terrain le 25 janvier, 2019. La réunion du Comité d'aménagement du 6 mars 2019 a servi pour recevoir les commentaires du public.

Lors de la réunion du Comité d'aménagement, les membres du Comité ont discuté des mérites de l'utilisation proposée et des enjeux potentiels. Il fut remarqué qu'une future utilisation industrielle aura besoin de faire une demande de modification au règlement de zonage pour pouvoir opérer sur le terrain visé et les terrains adjacents, à cause de la distance de séparation entre une utilisation industrielle et la garderie, même si les utilisations industrielles sont des utilisations permises dans la Zone d'industrie générale.

Les membres du Comité ainsi que le demandeur ont présenté des points reliés aux emplois que la garderie apportera à Rockland et la nécessité pour des places dans des garderies à Rockland. L'emplacement proposée pour la garderie fut comparé à d'autres emplacements possibles, dans les secteurs commerciaux de Rockland où il y a des problèmes de sécurité pour les enfants et une manque d'espace vert pour l'aire de jeu extérieure. Le point fut soulevé qu'il y a déjà d'autres commerces situé au 729 et 733 rue Industrielle qui accueillent des jeunes enfants pour des activités (un gym de crossfit et le golf virtuel).

Il fut suggéré que la modification au règlement de zonage proposée soit modifiée pour changer le zonage du bâtiment au 733 rue Industrielle uniquement, et non pas pour toute la propriété au complet.

Suite à la direction du Comité d'aménagement, le Département d'infrastructures et aménagement du territoire a préparé un Règlement pour ajouter une garderie comme usage principale au 733 rue Industrielle ainsi que d'exempter la garderie des distances de séparation aux utilisations industrielles adjacentes. Ceci aurait l'effet de permettre la garderie à l'emplacement proposé, ainsi que d'interdire les usages industriels sur le terrain sujet à la demande et sur les terrains adjacents.

7) RECOMMANDATION DU COMITÉ D'AMÉNAGEMENT :

THAT the Municipal Council authorize the amendment to the zoning by-law submitted by Mrs. Kimberle Herold for RANN Enterprises Inc. uniquely for the unit at 733 Industrielle Street in Rockland.

QUE le Conseil municipale autorise la demande de modification au règlement de zonage soumis par Mme Kimberle Herold pour RANN Enterprises Inc uniquement pour l'unité au 733 rue Industrielle à Rockland.

8) IMPACT FINANCIER (monétaire/matériaux/etc.):

Il n'y a pas d'impact financier direct associé avec le refus de l'amendement

au Règlement de zonage. Si l'amendement proposé est approuvé et un appel est déposé, un urbaniste externe et un conseiller juridique externe seraient retenus.

9) IMPLICATIONS LÉGALES :

Conformément avec le projet de loi 139, si l'amendement au règlement de zonage proposé est adopté, un appel au Tribunal d'appel de l'aménagement local peut seulement être déposé basé sur un manque de conformité avec la Déclaration de principes provinciale et/ou le Plan officiel. Par ce que le personnel recommande que la demande soit refusée, si un appel est déposé contre le règlement de zonage, la Greffière et la Directrice générale chercheraient à retenir un urbaniste externe pour fournir un affidavit appuyant le refus pour la révision initiale de l'item au Tribunal. Un conseiller juridique externe serait aussi retenu afin de représenter la Cité auprès du Tribunal.

Si le règlement de zonage est refusé, des raisons doivent être données. Pour qu'un appel contre un refus d'une demande de modification au Règlement de zonage puisse réussir, l'appelante doit premièrement démontrer que le règlement de zonage existant n'est pas conforme à la Déclaration de principes provinciale ou au Plan officiel. La préparation des documents nécessaires pour le Tribunal d'appel de l'aménagement local et les soumissions au Tribunal pourraient être faites par le personnel.

10) GESTION DU RISQUE (RISK MANAGEMENT) :

S/O

11) IMPLICATIONS STRATÉGIQUES :

Si l'amendement proposé est approuvé pour permettre une garderie au 733 rue Industrielle, des nouveaux usages industriels légers seront interdits dans les autres unités au 729, 731, et 733 rue Industrielle sur le même terrain que la garderie, ainsi qu'au 701 rue Industrielle, et sur le terrain vacant situé à l'est du terrain visé, appartenant à la municipalité, qui est actuellement utilisé comme terrain de soccer. Un commerce désirant de s'installer avec un usage industriel léger sur l'un de ces terrains dans le parc industriel aurait besoin de faire une demande de modification au règlement de zonage afin d'éliminer la distance de séparation entre l'usage proposé et la garderie. Une étude de bruit, odeur, vibration, etc. pourrait être nécessaire afin d'appuyer la demande de modification au règlement de zonage.

12) DOCUMENTS D'APPUI:

Règlement 2019-XX

Lettre de Kimberle Herold

Lettre du Ministère de l'éducation

Lettre de recommandation de la Centre d'entrepreneurship de Prescott et Russell

RÈGLEMENT DE ZONAGE N° 2019-XX

Amendant le Règlement de zonage n° 2016-10

Corporation de la Cité de Clarence-Rockland

733 rue Industrielle
rédigé par

Cité de Clarence-Rockland
1560, rue Laurier
Rockland (Ontario)
K4K 1P7
(613) 446-6022

ZONING BY-LAW NO. 2019-XX

Amending Zoning By-Law No. 2016-10

The Corporation of the City of Clarence-Rockland

733 Industrielle Street

prepared by

City of Clarence-Rockland
1560 Laurier Street
Rockland, Ontario
K4K 1P7
(613) 446-6022

LA CORPORATION DE LA CITÉ DE CLARENCE-ROCKLAND

RÈGLEMENT N° 2019-XX

RÈGLEMENT AMENDANT LE RÈGLEMENT DE ZONAGE N° 2016-10;

ATTENDU QUE le Règlement de zonage n° 2016-10 réglemente l'utilisation des terrains, la construction et l'utilisation des bâtiments et structures sur le territoire de la Cité de Clarence-Rockland; et

ATTENDU QUE le Conseil de la Corporation de la Cité de Clarence-Rockland considère qu'il est opportun d'amender le Règlement de zonage n° 2016-10, tel qu'il suit;

PAR LA PRÉSENTE, le Conseil de la Corporation de la Cité de Clarence-Rockland donne force de loi à ce qui suit:

Article 1: La propriété décrite comme étant une partie du lot 23, concession 1 (O.S.), soit le 733 rue Industrielle, et identifiée à la cédule « A » ci-jointe, et faisant partie du présent règlement, est le terrain concerné par ce règlement.

Article 2: La cédule « B » du Règlement de zonage n° 2016-10, est par la présente amendée en modifiant de « *Zone d'industrie générale (MG)* » à « *Zone d'industrie générale - Exception 5 (MG-5)* », tel qu'identifiée à la cédule « A » ci-jointe, et faisant partie intégrante du présent règlement.

Article 3: L'article 10.1.3 (e) du Règlement de zonage n. 2016-10, est par la présente ajoutée et lit comme suit :

« (b) MG-5, 733 rue Industrielle

Nonobstant toute disposition contraire en vertu du présent Règlement, les terrains zonés MG-5 doivent être utilisés conformément aux dispositions ci-après :

(i) Utilisations additionnelles permises :

- garderie

(ii) Une garderie n'est pas sujette aux dispositions de l'article 4.42 du présent règlement. »

Article 4: Le présent règlement entrera en vigueur à la date de son adoption par le Conseil sous réserve de l'approbation du Tribunal ou suite à la date limite pour le dépôt des avis d'opposition, selon le cas.

FAIT ET ADOPTÉ EN RÉUNION PUBLIQUE, CE 19^{ÈME} JOUR DE MARS 2019.

Guy Desjardins, maire

Monique Ouellet, greffière

THE CORPORATION OF THE CITY OF CLARENCE-ROCKLAND

BY-LAW NO. 2019-XX

BEING A BY-LAW TO AMEND ZONING BY-LAW NO. 2016-10;

WHEREAS Zoning By-Law no. 2016-10 regulates the use of land, and the use and erection of buildings and structures in the City of Clarence-Rockland; and

WHEREAS the Council of the Corporation of the City of Clarence-Rockland considers appropriate to amend Zoning By-Law No. 2016-10, as described;

NOW THEREFORE, the Council of the Corporation of the City of Clarence-Rockland enacts as follows:

Section 1: The property described as part of Lot 23, Concession 1 (O.S.), 733 Industrielle Street, identified on Schedule "A" attached to and forming part of this by-law shall be the lot affected by this by-law.

Section 2: Schedule "B" of Zoning By-Law No. 2016-10 is hereby amended by changing the "*General Industrial (MG) Zone*" to "*General Industrial – Exception 1 (MG-5) Zone*" on Schedule "A" of the map attached hereto and fully integrated as part of this by-law.

Section 3: Section 10.1.3 (e) of the Zoning By-law No. 2016-10 is hereby added and reads as follows:

"(b) MG-5, 733 Industrielle Street

Notwithstanding the provisions of this By-law to the contrary, the lands zoned MG-5 shall be used in accordance with the following provisions:

(i) Additional permitted uses:

- daycare

(ii) A daycare is not subject to the provisions of section 4.42 of this by-law.

Section 4: This by-law shall become effective on the date of passing hereof, subject to the approval of the Tribunal or following the last date for filing objections as the case may be.

DATED AND PASSED IN OPEN COUNCIL, THIS 19TH DAY OF MARCH, 2019.

Guy Desjardins, Mayor

Monique Ouellet, Clerk

NOTE EXPLICATIVE

But et effet du Règlement

Le but du présent règlement consiste à modifier le Règlement de zonage n° 2016-10, afin de changer la catégorie de zonage de « *Zone d'industrie générale (MG)* » à « *Zone d'industrie générale – exception 5 (MG-5)* » pour l'édifice située au 733 rue Industrielle à Rockland. L'amendement aura l'effet de permettre une garderie comme usage principale, ainsi que d'éliminer la zone tampon entre la garderie et les usages industriels existants.

Pour tous renseignements supplémentaires relativement à cette modification au Règlement de zonage n° 2016-10, veuillez communiquer avec Mme Claire Lemay, urbaniste municipale du Service d'infrastructure et aménagement du territoire à l'Hôtel de ville situé au 1560, rue Laurier ou par téléphone au numéro (613) 446-6022, poste 2267.

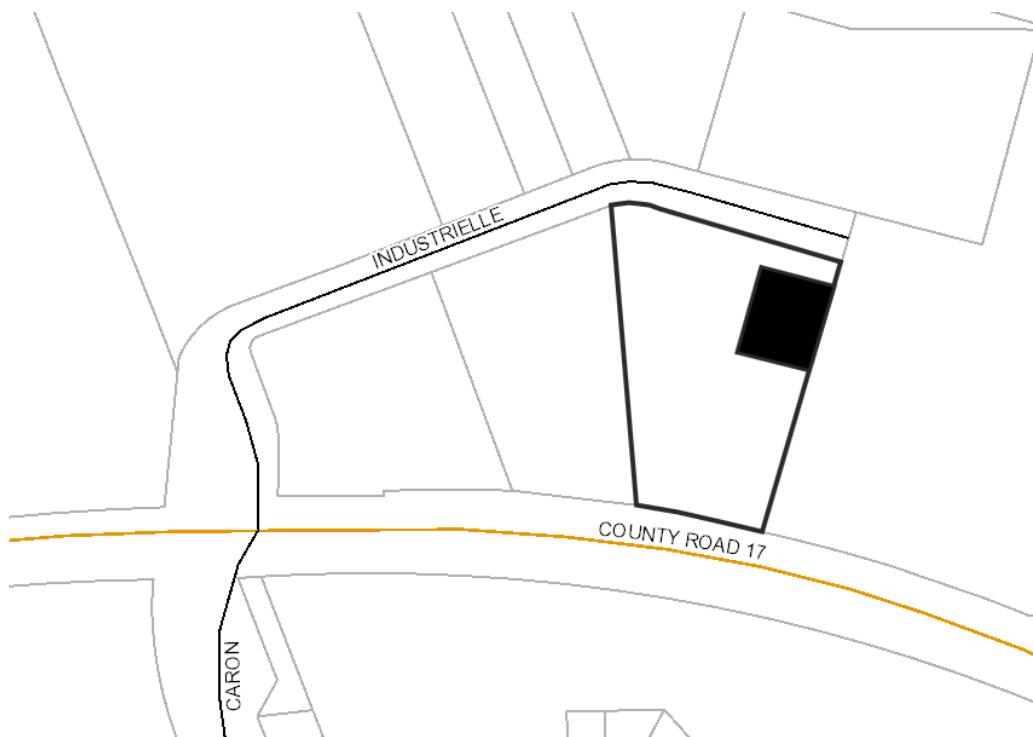
EXPLANATORY NOTE

Purpose and Effects of this By-Law

The purpose of the by-law is to amend Zoning By-Law No. 2016-10 in order to change the zoning category from "General Industrial (MG) Zone" to "General Industrial - Exception 5 (MG-5) Zone" for the building located at 733 Industrielle Street in Rockland. The amendment has the effect of permitting a daycare as a principal use on the property as well as eliminating the buffer distance between the daycare and existing industrial uses.

For further information concerning the amendment to Zoning By-Law No. 2016-10, you may contact Mrs. Claire Lemay, Municipal Planner for the Infrastructure and Planning Department, at the Town Hall, 1560 Laurier Street or by telephone at (613) 446-6022, ext. 2267.

CÉDULE « A » / SCHEDULE “A”



De / From (MG) à / to (MG-5)

| | |
|--|--|
| <p> Terrains(s) touché(s) par ce règlement Area(s) affected by this by-law</p> <p>Changement de zonage /Zone change de/from MG à/to MG-5</p> <p>Certification d'authenticité Certificate of Authentication</p> <p>Ceci constitue le plan Cédule « A » du Règlement de zonage n° 2019-XX, adopté le 19 mars 2019.</p> <p>This is plan Schedule “A” to Zoning By-Law No. 2019-XX, passed the 19th day of March, 2019.</p> | <p>Plan Cédule «A» du règlement n° 2019-XX</p> <p>Schedule “A” to By-Law No. 2019-XX</p> <p>733 Industrielle Street</p> <p>733 rue Industrielle</p> <p>Cité de Clarence-Rockland City</p> <p>Préparé par/prepared by Cité de Clarence-Rockland City 1560, rue Laurier Street Rockland, Ontario K4K 1P7</p> <p>Pas à l'échelle/Not to scale</p> |
| <p>Guy Desjardins, Maire / Mayor</p> | <p>Monique Ouellet, Greffière / Clerk</p> |

*Kimberle Herold
903 Lise Crescent, Rockland
K4K1G8
Tél : 613-869-2029
E-mail : kherold12@gmail.com*

Rockland, le 10 mars 2019

A l'attention du Conseil, Service
d'Infrastructure et tout autre secteur
concerné au règlement de zonage du 733
Industrielle

*Adresse: 1560 Laurier St, Rockland, ON
K4K 1P, Ontario
Téléphone : (613) 446-6022*

Objet : Règlement au zonage au 733 rue industrielle à Rockland

À qui de droit,

La francophonie canadienne fait face à un état d'urgence concernant l'accès à des services en petite enfance francophones en situation minoritaire. Le Réseau de développement économique et d'employabilité (RDÉE Canada) en partenariat avec la Commission nationale des parents francophones (CNPF) et l'Association des collèges et universités de la francophonie canadienne (ACUFC) a créé une alliance stratégique afin d'intervenir en petite enfance pour les communautés francophones au Canada. Les trois organismes nationaux ont joint leurs forces, en misant sur la complémentarité de leurs mandats respectifs, afin d'explorer et de concrétiser des solutions novatrices dans le but d'améliorer l'accès à des services en français de qualité pour la petite enfance au sein des communautés francophones partout au Canada au sein des CLOSM.

Dans le cadre de la Stratégie nationale en petite enfance pour les communautés de langues officielles en situation minoritaire (CLOSM), cette initiative propose des solutions concrètes pour surmonter les défis reliés à l'accès des services de qualité dans le milieu de la petite enfance au Canada.

Notre désir est de vous rendre attentif à ce projet, crucial pour nous comme pour ceux qui sollicitent de l'aide. Beaucoup de tension dans les jeunes familles en ce qui attire à un retour impossible au travail à cause de la pénurie de service en petite enfance dans notre région. Nous ne sommes pas sans savoir que la liste d'attente pour un service de garde à Rockland est d'une durée de 2 ans minimum et 3 ans maximum.

De ce fait, nous avons répondu à l'appel d'offre du Réseau de développement économique et d'employabilité dans le but d'obtenir les subventions possibles pour la réalisation de ce projet.

En ce qui attire au parc industriel de Rockland, il a été fondé avec de bonnes intentions ; industriel léger et commercial. La plus grande majorité a été réaménagée pour une école de hockey, un terrain de football et le solde a été transformé en logement. Plusieurs nouveaux projets en vigueur parmi lesquels une école secondaire ou primaire qui viendra s'installer très prochainement à côté du 733 industrielle. Et pourquoi pas une garderie ? Une garderie qui ajoutera la diversité, la vie à ce beau parc.

Dans le règlement de zonage de mai 2016

(www.clarence-rockland.com/images/zbl05.pdf), partie 10, page 226, 227, "Garderie existe déjà.

Donc, c'est déjà acceptable. Nous pouvons toute même opérer une garderie avec les 200 mètres carrés, mais tout ce que nous voulons c'est rendre l'espace plus attrayant en ayant plus d'espace afin d'un aménagement qui répondra mieux aux normes ministérielles et aux bien-être de nos jeunes enfants dans la communauté. Oui c'est un parc "parc industriel et commercial". Mais qu'en est-il des autres garderies qui offrent leurs services dans des parcs industriels à Orleans, Ottawa et autres. Si on fait des recherches sur Google Taylor Creek à Orléans. On peut compter jusqu'à 3 garderies. C'est pourtant de véritable parc industriel dans des lieux très fréquenté avec de vrai trafique. Sans pour autant aller plus loin ici à Rockland nous avons Tiny Hopper qui se trouve dans la rue la plus animée avec un stationnement rapide pour prendre une pizza. La garderie accompagne les enfants sur Laurier. Qu'adviendra si un conducteur oublie d'arrêter pour les feux rouges d'un autobus scolaire.

Au 733 industriel, l'unité contient beaucoup de fenêtres adaptées, c'est beaucoup plus calme que d'autres endroits. Nous serons à l'abri des camions parce nous serons éloignés de leur parcours. C'est à côté du vieux terrain de football et à côté de l'arène. Les petits enfants pourront s'amuser et participer à des activités dans un environnement plus sûr, mieux que d'autres endroits. Pour l'instant c'est la place la plus pratique et commode pour un service de garde tant pour les citoyens de Clarence-Rockland, Clarence-Creek, Wendover et environ. L'emplacement est parfait pour les parents avec un accès facile sur la 174.

Notre but est d'appuyé directement dans le développement de nouvelles places en service de garde pour assurer un continuum de départ misant fortement sur la qualité des services en petite enfance avant l'entrée scolaire de l'enfant.

Nous voulons avoir un impact concret sur le maintien et l'augmentation du nombre de places en service de garde au pays.

Les cibles qu'ont visent sont les suivants :

- ✓ Augmenter, maintenir, et développer de nouvelles places en garderie pour les enfants de 0 à 13 ans
- ✓ Accroître notre connaissance de l'état des lieux en petite enfance
- ✓ Nous doter d'une stratégie de développement
- ✓ Développer un plan de viabilité à long terme
- ✓ Assurer un service de qualité
- ✓ Appuyer le secteur de la petite enfance
- ✓ Faire partie d'un plan, d'une stratégie ou d'un projet de plus grande envergure
- ✓ Répondre à un besoin ou à un problème identifié
- ✓ Être une valeur ajoutée au secteur de la petite enfance
- ✓ Contribuer au développement économique
- ✓ Créer de nouveaux emplois

Nous vous prions d'accepter le changement au zonage à l'édifice 733 rue industrielle comme il a été indiqué dans notre demande car nous n'avons jamais demander de changer le zonage du 729 et 731 rue industrielle. Ceci pour permettre la création d'un

nouveau service de garde agréé de qualité, nous pensons que Clarence-Rockland doit saisir cette opportunité pour créer de nouveaux emplois et aider le long délai nécessaire à trouver un service de garde.

On vous remercie.

Au nom de la compagnie ;

Kimberle Herold

Signature

La Municipalité de Clarence-Rockland

Objet: Lettre de recommandation
Kimberle Herold

Monsieur, Madame,

La présente a pour but de souligner le travail effectué par madame Kimberle Herold en tant que cliente du Centre d'entrepreneurship de Prescott et Russell.

Madame Herold a su travailler efficacement et stratégiquement pour répondre à un besoin de la région de Clarence-Rockland. Elle est une personne dynamique, travaillante, organisée, ponctuelle et discrète. De plus, elle démontre un souci du travail afin de produire des documents qui correspondent aux exigences du ministère.

Je crois sincèrement que Madame Herold saura accomplir les tâches et fournir le travail demandé et, pour l'ensemble des raisons évoquées, avec l'appui des services de garde des Comtés unis de Prescott et Russell ainsi que le travail effectué avec le Centre d'entrepreneurship de Prescott et Russell, je ne peux que vous la recommander.

Les services de garde à l'enfance jouent maintenant un rôle de premier plan dans le fonctionnement de nos sociétés. L'analyse de la localisation des garderies et de leur clientèle par rapport aux milieux sociaux de la région de Clarence-Rockland permet d'aborder la question des variations dans l'accessibilité aux services de garde. Les grands traits de l'espace socio-résidentiel de Clarence-Rockland sont d'abord définis à l'aide d'une écologie factorielle. En général, les garderies ont tendance à se localiser dans les zones centrales alors que les enfants d'âge préscolaire habitent très majoritairement dans les banlieus éloignées. Cette contradiction apparente fait l'objet d'une analyse plus poussée qui montre que le lieu de travail des parents influence grandement le rapport entre la répartition de l'offre de places en garderie et la répartition de la demande, ce qui pourrait avoir des conséquences intéressantes pour les quartiers urbains centraux.

Rockland est une communauté en banlieue d'Ottawa des plus importantes dans la région de Prescott et Russell. Avec une des plus grandes concentrations de la population (Recensement 2016 = 12,302) et d'un revenu médian des plus élevés de la région (42,721\$), le besoin d'une garderie en région est d'une importance cruciale. Suffit qu'il y a plusieurs jeunes familles avec des enfants d'où les parents travaillent en ville/ont la navette, le besoin d'une garderie en région serait complémentaire (Groupes d'âge et d'âge moyen de la population de 0 à 14 ans est de 2,220). Enfin, des relations significatives sont établies entre la localisation des garderies et leur degré de mixité sociale.

N'hésitez pas à communiquer avec moi pour de plus amples renseignements. Veuillez, recevoir, Madame, Monsieur, mes salutations distinguées.



Benoit Brunette, agent de projet
Centre d'entrepreneurship de Prescott et Russell
59 rue Court, L'Orignal, ON K0B 1K0
613-675-4661 poste 8106

politique d'urgence

Inbox

 Brisebois, Stephanie (EDU)

Thu, Mar 7, 1:26 PM (2 days ago)

to me

Brisebois, Stephanie (EDU) <Stephanie.Brisebois@ontario.ca>

to: Kimberle Herold <kherold12@gmail.com>

date: Mar 7, 2019, 1:26 PM

subject: politique d'urgence

mailed-by: ontario.ca

security:Standard encryption (TLS) [Learn more](#)

Bonjour

La première étape d'une application est de faire approuver les plans afin que vous puissiez commencer la construction. Ceci dit, nous ne pouvons pas approuver les plans sans avoir le OK pour le zonage, car vos plans démontrent plus de 200m², mais la lettre du zonage indique que vous ne pouvez pas avoir plus de 200m². L'application ne peut pas avancer sans savoir si tu auras accès à plus de 200 m². Alors, il est primordial d'avoir une réponse pour le zonage, car l'approbation des plans dépend de cette réponse. Si tu reçois le OK pour le zonage, les plans pourront être approuvés assez rapidement, car nous y avons travaillé entre temps.

J'ai joint la politique d'urgence du Minsitère, vous devez ajouter la page 13 (Phase 3 : Rétablissement (une fois la situation d'urgence terminée) à votre politique. Merci

Stephanie Brisebois

Program Advisor, East Region
Child Care Quality Assurance and Licensing Branch
Early Years and Child Care Division | Ministry of Education

Conseillère en programmes, Région Est
Direction de l'assurance de la qualité et de la délivrance des permis des services de garde d'enfants
Division de la petite enfance et de la garde d'enfants
Ministère de l'Éducation



| | |
|---------------------|--|
| Date | 19/03/2019 |
| Submitted by | Marie-Eve Bélanger |
| Subject | TIS and modification to a condition of Draft Approval of Brigil and Stage 5 Morris Village |
| File N° | D-12-121, D-12-122 |

REPORT N°

AMÉ-19-30-R

1) NATURE/GOAL :

The nature of this report is the present the Transportation Impact Study for the east-west collector and to change a condition in the Draft Plan Approval of Brigil and Morris Village Stage 5.

2) DIRECTIVE/PREVIOUS POLICY :

n/a

3) DEPARTMENT'S RECOMMENDATION :

ATTENDU QUE l'étude de transport pour le collecteur est-ouest a été complétée en décembre 2018, et

ATTENDU QU'UNE condition doit être modifiée dans la liste de conditions approuvées pour le lotissement du Village Morris Stage 5 et de Brigil.

QUE la condition 26 du lotissement de Brigil et la condition 29 du lotissement du village Morris stage 5 soit modifié afin de lire comme suit :

- "That Poupart Side Road, Bronze Avenue and St-Jean Street be designed and built to municipal standards with an urban cross-section approved by the City. The design should follow the recommendation of the detailed transportation impact study that was completed by Castleglenn Consultants (Dec 2018) with any subsequent revisions, if applicable. The design, the environmental studies, the EA, the construction work, the project management fees and any other studies or works required are to be paid by the Development Charges By-law and the municipal budget in place for the current year. The estimated cost of the design and works to be completed must be approved by the City before any undertaking."

WHEREAS the Transportation Impact Study for the east-west collector was completed in December 2018.

AND WHEREAS a condition must be modified under the Brigil and Morris Village Stage 5 draft approval.

THAT Condition 26 of the Brigil file and Condition 29 of the Morris Village Stage 5 file be modified to read as follows:

- That Poupart Side Road, Bronze Avenue and St-Jean Street be designed and built to municipal standards with an urban cross-section approved by the City. The design should follow the recommendation of the detailed transportation impact study that was completed by Castleglenn Consultants (Dec 2018) with any subsequent revisions, if applicable. The design, the environmental studies, the EA, the construction work, the project management fees and any other studies or works required are to be paid by the Development Charges By-law and the municipal budget in place for the current year. The estimated cost of the design and works to be completed must be approved by the City before any undertaking.

4) BACKGROUND :

On April 17th, 2018, Council approved a list of conditions for the Brigil Subdivision. On June 18th, 2018, two conditions were added following the LPAT appeal.

On April 4th, 2018, Council approved a list of conditions for Morris Village Stage 5. On May 7th, 2018, one condition was amended to change the date of expiry as per the Counties request.

5) DISCUSSION :

On December 21st, 2018, the City obtained a copy of the Transportation Impact Study that was completed for the Brigil and Morris Village Stage 5 projects. The study includes recommendations on the construction of the future east-west collector, which includes parts of Poupart Side Road and St-Jean Street. The Study also shows modifications or improvements to be completed to different existing intersections.

Following a meeting with the Developer's Engineer, Atrel Engineering, it was determined that we should be undertaking the design of St-Jean Street first. As such, the budget of 2019 was approved with an amount for the design of St-Jean Street from Poupart Side Road to Docteur Corbeil Boulevard.

The study that was undertaken for the east-west collector was necessary for the City and was paid under the 2018 budget. The draft

plan conditions that were approved for both project indicated that both developers needed to work together to hire an Engineer to complete this study and that the development charges would cover the cost. As such, the study was undertaken by the developers.

With the 2019 budget approved and the study completed, we deem that the developer's Engineer should be responsible to complete the design of St-Jean Street from Poupart Side Road to Docteur Corbeil Boulevard. The developers' engineering firm completed a preliminary design at the same time as the traffic study and thus it would be beneficial that the same firm continues the work that was started.

Condition 26 of Brigil's Draft Plan Approval and Condition 29 of Morris Village Stage 5 Draft Plan Approval indicates that the Owner is responsible to complete the design of Poupart Road and Street No.1 (in Morris Village). However, St-Jean Street was omitted from the condition and should be added.

As such, we recommend that both conditions be modified to read as follows:

- That Poupart Side Road, Bronze Avenue and St-Jean Street be designed and built to municipal standards with an urban cross-section approved by the City. The design should follow the recommendation of the detailed transportation impact study that was completed by Castleglenn Consultants (Dec 2018) with any subsequent revisions, if applicable. The design, the environmental studies, the EA, the construction work, the project management fees and any other studies or works required are to be paid by the Development Charges By-law and the municipal budget in place for the current year. The estimated cost of the design and works to be completed must be approved by the City before any undertaking.

Transportation Impact Study:

The Transportation Impact Study is included as Schedule A of this report. Based on this study, the east-west collector must be designed to accommodate a divided 4-lane starting from the west. Once Poupart reaches St-Jean Street, it will become an undivided 4-lane to the east to the new roundabout at the bottom the hill. At this point, St-Jean Street will split into two streets, one being Bronze Street in Morris Village and the other will stay St-Jean Street towards Laurier Street. Both of those two streets will be 2-lane. The study also recommends multiples roundabouts throughout the east-west collector. An excerpt from the Study is included as Schedule B and shows the modifications

to be completed. See Appendix E of the Transportation Impact Study for the preliminary design and road configuration.

6) CONSULTATION:

The City has consulted with both Developers; all parties are in agreement with the outcomes of the study, the timing of works and plans.

7) RECOMMENDATIONS OR COMMENTS FROM COMMITTEE/ OTHER DEPARTMENTS :

n/a

8) FINANCIAL IMPACT (expenses/material/etc.):

The budget was approved for \$400,000.00 for the design of St-Jean Street from Poupart Side Road to Docteur Corbeil Boulevard. It is mostly funded by the Development Charges.

9) LEGAL IMPLICATIONS :

n/a

10) RISK MANAGEMENT :

n/a

11) STRATEGIC IMPLICATIONS :

It is important to design the east-west collector at this stage since we will be in a better position to design the surrounding areas. The right-of-way easements will be easier to obtain prior to any subdivisions being built.

12) SUPPORTING DOCUMENTS:

Transportation Impact Study
Excerpt of TIS

TRANSPORTATION IMPACT STUDY

(DRAFTPLAN OF SUBDIVISION)

Submitted To:



CITY OF CLARENCE-ROCKLAND
Department of Infrastructure and Planning
1560 Laurier Street Rockland, Ontario K4K 1P7

And

SPACE BUILDERS

Spacebuilders Ottawa Ltd
345A Laurier Street, P.O. Box 849
Clarence-Rockland, Ontario, K4K 1L5

BRIGIL

Brigil Construction
98 Lois Street
Gatineau, Quebec, J8Y 3R7

Prepared by:



Atrel Engineering Ltd.
1-2884 Chamberland Street
Rockland, ON K4K 1M6
Tel: (613) 446-7423

And



Castleglenn Consultants Inc.
2460 Lancaster Road, Suite 200
Ottawa, ON K1B 4S5
Tel: (613) 731-4052

December 21, 2018

Transportation Impact Study

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Transportation Impact Study

APPENDICES

Appendix "A" SK1 – Location Map

Appendix "B" Traffic Impact Study prepared by CastleGlenn Consultants

Appendix "C" Typical Cross-Sections

- 180801-CS1 – Proposed undivided 23.0m R.O.W. (Poupart)
- 180801-CS2 - Proposed 30.0m divided R.O.W. (Poupart)
- 180801-CS3 - Proposed 30.0m undivided R.O.W. (St-Jean)
- 180801-CS4 - Proposed 26.0m undivided R.O.W. (Morris Village)
- 180801-CS5 - Proposed 26.0m undivided R.O.W. (St-Jean)

Appendix "D" Reference Plan – 180801-RP1

Appendix "E" Roundabout Schematic Plans

- 180801-RA1 (Poupart)
- 180801-RA2 (Poupart/Brigil)
- 180801-RA3 (Poupart/Brigil/St-Jean)
- 180801-RA4 (St-Jean/Morris)
- 180801-RA5 (St-Jean/Dr. Corbeil)

Appendix "F" Land Acquisition Preliminary Plans

- 180801-LA1 (Poupart)
- 180801-LA2 (Poupart)
- 180801-LA3 (Poupart/St-Jean)
- 180801-LA4 (St-Jean)
- 180801-LA5 (St-Jean)
- 180801-LA6 (St-Jean)

Appendix "G" Road Schematic Plans

- 180801-RD1 (Poupart)
- 180801-RD2 (Poupart)
- 180801-RD3 (Poupart/St-Jean)
- 180801-RD4 (St-Jean)
- 180801-RD5 (St-Jean)
- 180801-RD6 (St-Jean)

Appendix "H" St-Jean Hill Plans

- 180801-HILL - St-Jean Preliminary Hill Plan and Profile
- 180801-DS1 - St-Jean Residential Preliminary Driveway Slopes
- 180801-DS2 - St-Jean Commercial Preliminary Driveway Slopes

Appendix "I" Hydro Station Sketches

- 180801-HS1 - Hydro Station Street View
- 180801-HS2 - Hydro Station Top View

1.0 INTRODUCTION

1.1 Background

The following Traffic Impact Study has been prepared by Atrel Engineering Ltd for the City of Clarence-Rockland in response to the Draft Plan conditions provided to Brigil and Spacebuilders. A location map illustrating the Traffic Study Area is presented in Appendix "A" of this report (refer to SK1 "Location Map"). The recommendations are based on the results obtained from CastleGlenn Consultants, provided in Appendix "B", the legal plan prepared by Arpentage Dutrisac Surveying Inc. (ADSI) and the schematic design prepared by Atrel Engineering Ltd (AEL).

1.2 Study Objectives

As mentioned, this study is presented as a City request as part of the draft conditions for multiple development in the Rockland area. The requirements are detailed below:

The Owner shall submit a Transportation Impact Study certified by a qualified Professional Engineer with expertise in undertaking such studies which measures and analyzes traffic impacts, transit impacts and implications for traffic at the existing and proposed following intersections:

- a. County Road 21 (St-Jean Street) and Laurier Street; (**Point A**)
- b. County Road 21 (St-Jean Street) and Patricia Street; (**Point B**)
- c. County Road 21 (St-Jean Street) and Docteur Corbeil Boulevard; (**Point C**)
- d. Docteur Corbeil Boulevard and Caron Street (**Point D**)
- e. David Street and Caron Street (**Point E**)
- f. Street No.1 and Caron Street (**Point F**)
- g. County Road 21 (St-Jean Street) and Street No. 1 of the proposed Stage 5 Subdivision; (**Point G**)
- h. County Road 21 (St-Jean Street) and Poupart Road and Street No. 2 of the proposed Brigil/Poupart Subdivision; (**Point H**)
- i. Poupart Road and Brigil/Poupart Subdivision West entrance (**Point I**)
- j. Poupart Side Road with Poupart Side Road at the 90 degree turn (**Point J**)
- k. Poupart Side Road and Richelieu Street (**Point K**)
- l. Laurier Street bend (**Point L**)
- m. Richelieu Street and the entrance to Walmart and commercial uses to the north (**Point M**)
- n. Poupart Side Road and Carmen Bergeron (**Point N**)
- o. County Road 17 and Carmen Bergeron Street (**Point O**)

The consultant shall provide traffic counts at all above mentioned locations. Furthermore, the consultant shall provide the prescribed rights-of-ways for Poupart Road and St-Jean Street as part of this study as well as provide turning lanes and through lanes information.

Further, the Transportation Impact Study will consider the road link capacity and configuration for all roadways from Laurier Street to County Road 17 as per the intersections listed above and shall consider the development potential located east of the Spacebuilders Stage 5 Subdivision. The Transportation Impact Study shall consider a roundabout at the intersection of St-Jean Street and

Street No. 1 of the proposed Stage 5 Subdivision as well as at the intersection of County Road 21 and Dr. Corbeil Boulevard. The study shall be reviewed and approved by the Director of Infrastructure and Planning of the City of Clarence-Rockland.

Additionally, the study will identify the following:

- a. the schematic design of the critical intersections (**Points C, D, G, H, I and K**) along Poupart Road and St-Jean Street
- b. the legal boundary extent from points **L to B** along Poupart Road and St-Jean Street
- c. recommendations for hill rehabilitation and necessary land acquisition along the St-Jean Street slope (from points **H to G**)
- d. whether the roads should be divided or not
- e. whether a sidewalk, bikepath or multi-use path is required
- f. the lane width, length, storage, turning, acceleration and deceleration lanes
- g. the proposed posted speed limit and any traffic calming features
- h. if the intersections are warranted
- i. the maximum hill slope of St-Jean Street. A preliminary grading and profile will be provided from points **H to G**.
- j. the traffic schemes from existing to build out conditions including a 5 to 10 year and a 10 to 20 year horizon.

1.3 Key Findings

As per the Traffic Impact Study, prepared by CastleGlenn Consultants, presented in Appendix “B” and the legal plan prepared by ADSI, the following observations/recommendations are made:

1.3.1 General

Road cross-sections were developed based on the forecast traffic volume, the posted speed limit, the traffic calming features and the non-auto mode requirements. Five (5) typical cross-sections (Appendix “C”) were developed to identify the various right-of-way width, roadway lanes and non-auto mode.

A reference plan has been prepared to identify the various locations of the cross-sections, the land acquisition plans, the roundabout schematic plans, the road schematic plans, the St-Jean hill preliminary plans and the hydro station sketches.

Based on the forecasted traffic volumes and analysis, Castleglenn Consultants have elected to use roundabouts between Richelieu Street and Patricia Street to control the traffic. Roundabout schematics of the various intersection are shown as drawings 180801-RA1 to 180801-RA5 in Appendix “E”.

Using the existing legal plan, the proposed road cross-section and the roundabout schematic, the land acquisition preliminary plans were prepared to identify various areas where the existing right-of-way width is insufficient to accommodate the proposed road infrastructures. Drawings 180801-LA1 to 180801-LA6 (Appendix “F”) show the preliminary extent of the require land acquisition. Prior to acquiring the land, a detailed road, roundabout and utility design will be

required and then, an Ontario Land Surveyor (OLS) will need to clearly identify the proposed right-of-way.

Based on the proposed cross-sections, the widening of the Poupart Road and St-Jean Street will require some land acquisition. Dutrisac Surveying Inc. has been retained by AEL to obtain the existing legal surveying plans of the Poupart Road and St-Jean Street.

Drawings 180801-RD1 to 180801-RD6 in Appendix “G” show the proposed road schematic plans for Poupart Road and St-Jean Street from Laurier to Patricia Street which correspond to the cross-sections.

One of the main constraints in re-building St-Jean Street is the longitudinal slope of the existing road from the St-Jean/Poupart intersection to the proposed roundabout at Street No.1 (Morris Village entrance). After careful analysis of the surrounding areas, preliminary drawings were prepared to harmonize the hill to the surrounding residential and commercial entrances. Drawings 180801-HILL, 180801-DS1 and 180801-DS2 show the preliminary design of the hill and its proposed modifications.

Furthermore, the property requirement (road widening and roundabout construction) in proximity to the hydro station will have to be discussed with hydro at an early stage.

Additionally, drawings 180801-HS1 and 180801-HS2 show that some utility poles are currently located within the proposed road area and subsequently will need to be relocated as per the typical cross-sections mentioned above. Coordination with the utility companies will be required in order to complete this work.

1.3.2 Richelieu Street, Carmen Bergeron Street and Future East to West Poupart Road Bypass (Study Points O, N, M, K and J)

As detailed in Castleglenn’s report, the majority of the future developments south of Rockland will travel along St-Jean Street and Poupart Road in the east and west direction to travel to and from the City of Ottawa. Castleglenn has analyzed Richelieu Street and Carmen Bergeron Street and found that at the 5 to 10 year timeframe, the segments’ capacities are maximized and the system requires a travel alternative.

The alternative is provided in the form of the City of Clarence-Rockland’s special study to extend the current Poupart Road to the west from the 90 degree bend in order to connect to County Road 17 further west (refer to Castleglenn’s report for details).

This alternative, however, does not fix the issue of County Road 17 itself which is currently near maximum capacity. Another traffic study has been prepared and recommended to upgrade County Road 17 in the medium term (\pm year 2032).

1.3.3 Poupart Road (from Laurier Street to 90 degree bend) (Study point L, K and J)

- The road is currently a two lane undivided asphalt road from Richelieu Street to Sta. 1+310.
- The road is currently a two lane rural undivided gravel road with surface treatment from Sta. 1+310 to the 90 degree bend.
- The existing right-of-way width is approximately 23m from Laurier Street to Sta. 1+425.

- The existing right-of-way width ranges from approximately 12m to 23m from Sta. 1+425 to the 90 degree bend.
- Please refer to cross-section 180801-CS1 in Appendix "C" for this segment's proposed roadway and servicing details.
- The proposed right-of-way width is proposed to be 23m.
- As shown on the cross-section, the built out roadway will be a two lane (4.25m per lane) undivided asphalt road with concrete barrier curbs.
- A multi-use pathway and sidewalk are proposed in the boulevard.
- As shown on drawing 180801-RD1, there are existing utility poles along the road which will need to be relocated to the new location as shown on the cross-section.

1.3.4 Poupart Road (from 90 degree bend to St-Jean Street) (Study Points J, I and H)

- The road is currently a two lane rural undivided gravel road with surface treatment.
- The existing right-of-way width ranges from approximately 10m to 23m.
- Please refer to cross-section 18010-CS2 in Appendix "C" for this segment's proposed roadway and servicing details.
- The proposed right-of-way width is proposed to be 30m.
- As shown on the cross-section, the built out roadway will be a four lane (3.75m per lane) divided asphalt road (5.0m island) with concrete barrier curbs.
- A multi-use pathway and sidewalk are proposed in the boulevard.
- As shown on drawings 180801-RD2 and 180801-RD3, there are existing utility poles along the road which will need to be relocated to the new location as shown on the cross-section.

1.3.5 St-Jean Street (from Poupart Road to Morris Site Entrance - Street No. 1) (Study Points H and G)

- The road is currently a two lane rural undivided asphalt road.
- The existing right-of-way width ranges from approximately 24m to 38m.
- The current maximum slope along the road is approximately 14.6%.
- Please refer cross-section 180801-CS3 in Appendix "C" for this segment's proposed roadway and servicing details.
- The proposed right-of-way width will be widened to a minimum of 30m depending on the side slopes.
- As shown on the cross-section, the built out roadway will be a four lane (3.75m per lane) undivided asphalt road with concrete barrier curbs.
- The maximum proposed slope will be 8%.
- A multi-use pathway and sidewalk are proposed in the boulevard.
- As shown on drawings 180801-RD3 and 180801-RD4, there are existing utility poles along the road which will need to be relocated to the new location as shown the cross-section.

1.3.6 Morris Village Street No. 1 (Study Points C and D)

- Please refer to cross-section 180801-CS4 in Appendix "C" for this segment's proposed roadway and servicing details.
- The proposed right-of-way width will be 26m.
- As shown on the cross-section, the built out roadway will be a two lane (5.5m per lane) undivided asphalt road with concrete mountable curbs.
- A multi-use pathway and sidewalk are proposed in the boulevard

1.3.7 St-Jean Street (from Morris Site Entrance – Street No. 1 to Patricia Street) (Study Points G and C)

- The road is currently a two lane rural undivided asphalt road.
- The existing right-of-way width ranges from approximately 10m to 15m.
- Please refer to cross-section 180801-CS5 in Appendix “C” for this segment’s proposed roadway and servicing details.
- The proposed right-of-way width will be a minimum of 26m depending on the side slopes.
- As shown on the cross-section, the built out roadway will be a two lane (4.25m per lane) undivided asphalt road with concrete barrier curbs.
- A multi-use pathway and sidewalk are proposed in the boulevard.
- As shown on drawings 180801-RD4 to 180801-RD6, there are utility poles along the road which will need to be relocated to the new locations as shown on the cross-sections.

1.3.8 Caron Street (Study Points D, E and F)

- The road is currently a two lane rural undivided asphalt road from Baseline Road to David Street.
- The road then becomes a three lane undivided with a shared turning lane from David Street to Laurier Street.
- Castleglenn has evaluated Caron Street for all development timeframes and has detailed their results within their report. A four (4) lane road with traffic lights are ultimately proposed for better traffic flow.

1.4 St-Jean Street Hill Rehabilitation (From Study Points H to G)

The existing St-Jean Street’s road gradient was found to be approximately 15%. As per the Ontario Ministry of Transportation, the maximum slope for an undivided four lane collector is found to be 8.0%. In order to achieve such a requirement, the St-Jean Street hill was redesigned and realigned in order to match the existing properties.

There are currently four (4) lots which need to be accounted for in the hill design; three residential lots at the top of the hill (1253, 1259 and 1273 St-Jean Street) as well as the existing commercial lot owned by Centennial Construction Rockland Ltd (1211 St- Jean Street).

The St-Jean hill was designed in order to accommodate those lots. Based on the preliminary design, the existing residential properties’ entrances will be matched and reinstated while the commercial entrances will be slightly modified to accommodate the hill’s design slope of 8% which results in increasing the St-Jean Street elevations several metres near the bottom of the hill (Refer to drawing 180801-HILL for profile alignment and 180801-DS1 and 180801-DS2 for recommended driveway realignment).

In order to properly accommodate the commercial land entrances, it is proposed to realign the St-Jean Street centreline to the north. The right-of-way from Sta. 3+400 to Sta. 3+900 will be between 30m and 45m wide.

The existing culvert at the bottom of the St-Jean hill, which conveys runoff from the existing Lafontaine Creek, does not currently convey the creek’s 100 year runoff. Instead the major storm event’s runoff crosses St-Jean Street overland. As St-Jean Street will be raised several metres, the culvert will probably be replaced and sized to convey the creek’s 100 year storm runoff. Various work permits from the conservation authority/Ministry of Natural

Resources/Ministry of Environment will be required in order to work within the floodplain limits.

1.5 Laurier/Poupart Intersection (Study Point L)

The existing intersection is currently curving toward the west to abruptly turn towards the east when driving to the north.

ADSI looked at the legal property to observe that there are no private properties to acquire in order to rebuild this road with a normal curve.

Essentially this road can be re-aligned whenever the City wishes to do so. Drawing 180801-LA1 shows the extent of the property lines.

Since the multi-use pathway (MUP) will be provided to the Poupart/Laurier intersection, it would be recommended to continue the MUP to Laporte Street if the right-of-way allows such installation. The legal boundary would need to be verified, especially at the Lafontaine Creek crossing to ensure it can be achieved.

1.6 Hydro Station/Utilities

The construction of a wider and urbanized road will trigger the movement of infrastructures. The above and underground utilities along the Poupart and St-Jean roads will have to be identified and a relocation plan will be worked out with all utility companies.

Drawings 180801-HS1 and 180801-HS2 show the existing hydro station at the corner of Poupart and St-Jean and its various pole lines. In order to acquire the appropriate land, discussions should take place with Hydro One and other utility companies at an early stage to ensure that land can be acquired in this area, otherwise a plan 'B' will be required.

2.0 SUMMARY AND RECOMMENDATION

Castleglenn has analyzed Rockland's transportation system for three timeframes; 5 to 10 year, 10 to 20 year and built out. Recommendations have been made for key intersections and roadway specifications for all three timeframes along the study area as mentioned in the City's draft conditions to the developers.

In addition, road and intersection configurations are shown on the attached drawings along with land acquisition drawings and St-Jean Street hill grading specifications. As mentioned, the St-Jean hill's proposed grading will require widening of the right-of-way as well as work within the Lafontaine Creek area. These works will require a geotechnical report, an environmental impact study as well as a hydraulic analysis of the creek itself in order to assess the impact of the proposed road profile on the new culvert.

In order to assess the required land acquisition, a detailed road and roundabout design should be undertaken including the input of the utility companies.

All of which is respectfully submitted:

Prepared by:

ATREL ENGINEERING LTD



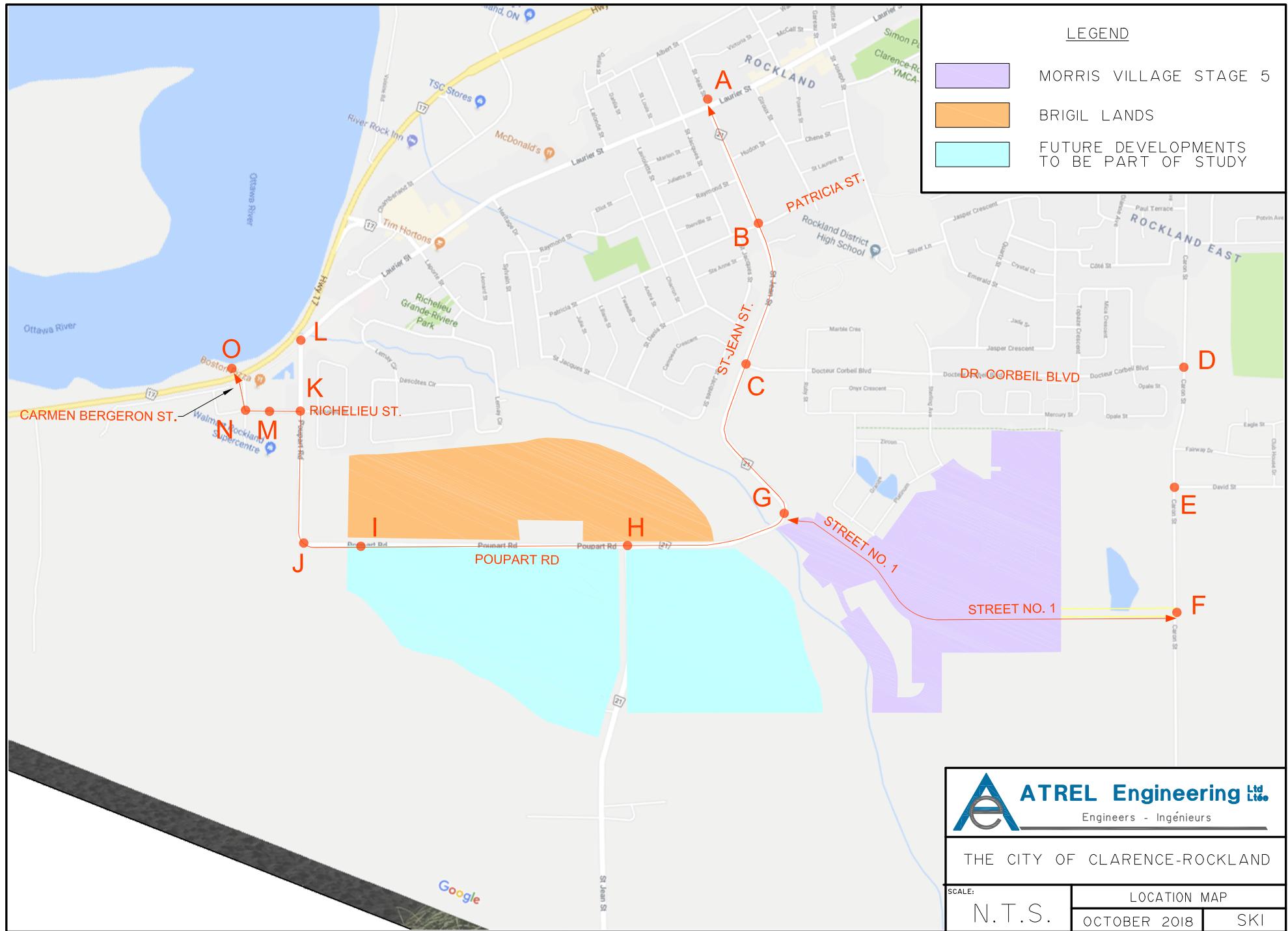
Jonathan Gendron, P.Eng.
Project Designer



Jean Décoeur, P.Eng.
Project Engineer

APPENDIX "A"

SK1 – Location Map



APPENDIX "B"

Traffic Impact Study prepared by CastleGlenn Consultants

TRANSPORTATION IMPACT STUDY

Draft Plan of Subdivision

Presented to: Atrel Engineering

Mr. Jean Décoeur
Project Manager
1-2884 Chamberland St.
Rockland, Ontario K4K 1M6

Prepared by: Castleglenn Consultants Inc.

2460 Lancaster Road
Ottawa, ON K1J 8K5

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1 INTRODUCTION

Castleglenn Consultants Inc. was retained in August, 2018 to undertake a Transportation Impact Study (TIS) that would:

- provide an overview of the existing conditions within the study area;
- address the traffic and transportation issues associated with the plan of subdivision located in the south-west end of the City of Clarence-Rockland; and
- provide input to the design component within the study area, inclusive of intersection type and configuration, auxiliary lane requirements, cross-section configuration (divided vs undivided), posted speed, traffic calming measures, non-auto mode requirements, right-of-way requirements and the St-Jean Street hill slope.

The plan of subdivision would involve the construction of over 9,000 units over approximately 430 hectares of land. The residential units are anticipated to consist of approximately 4,000 single family detached homes, 2,700 townhomes and 2,400 apartment units. A 1.03 hectares commercial development is also proposed.

2 EXISTING CONDITIONS

The study area is defined by Carmen-Bergeron Street to the west, County Road (CR) 17 and Laurier St to the north, Caron Street to the east and Poupart Road to the south. A site visit was undertaken on September 18th, 2018 to verify current roadway geometrics (roadway lane configuration, land uses, etc.) and undertake observations of the existing conditions within the vicinity of the proposed site.

The majority of the study area is undeveloped rural and treed areas, with some existing country residential dwellings located along Poupart Road. Within the north-east section of the study area, residential development has been built around Dr. Corbeil Boulevard. West of the proposed development plans is an existing commercial area with big box stores.

2.1 EXISTING ROADWAYS

The roadways within the study area are described as follows:

- **Carmen Bergeron Street:** This north-south corridor represents the first main access into the City from the west. The corridor connects CR 17 with a commercial development, by way of a 4-lane undivided cross-section. On-street parking is not permitted and one sidewalk is located on the east side. The speed limit is 50 km/hr.
- **Caron Street:** This north-south corridor was recently (within the last 10 years) reconstructed and intersects with CR 17. The corridor has a 3-lane cross-section, with a single lane in each direction and a middle lane with back-to-back left turns (between

CR 17 and David Street). On-street parking is not permitted and one sidewalk is located on the west side and a multi-use pathway on the east side. The posted speed limit is 50 km/hr.

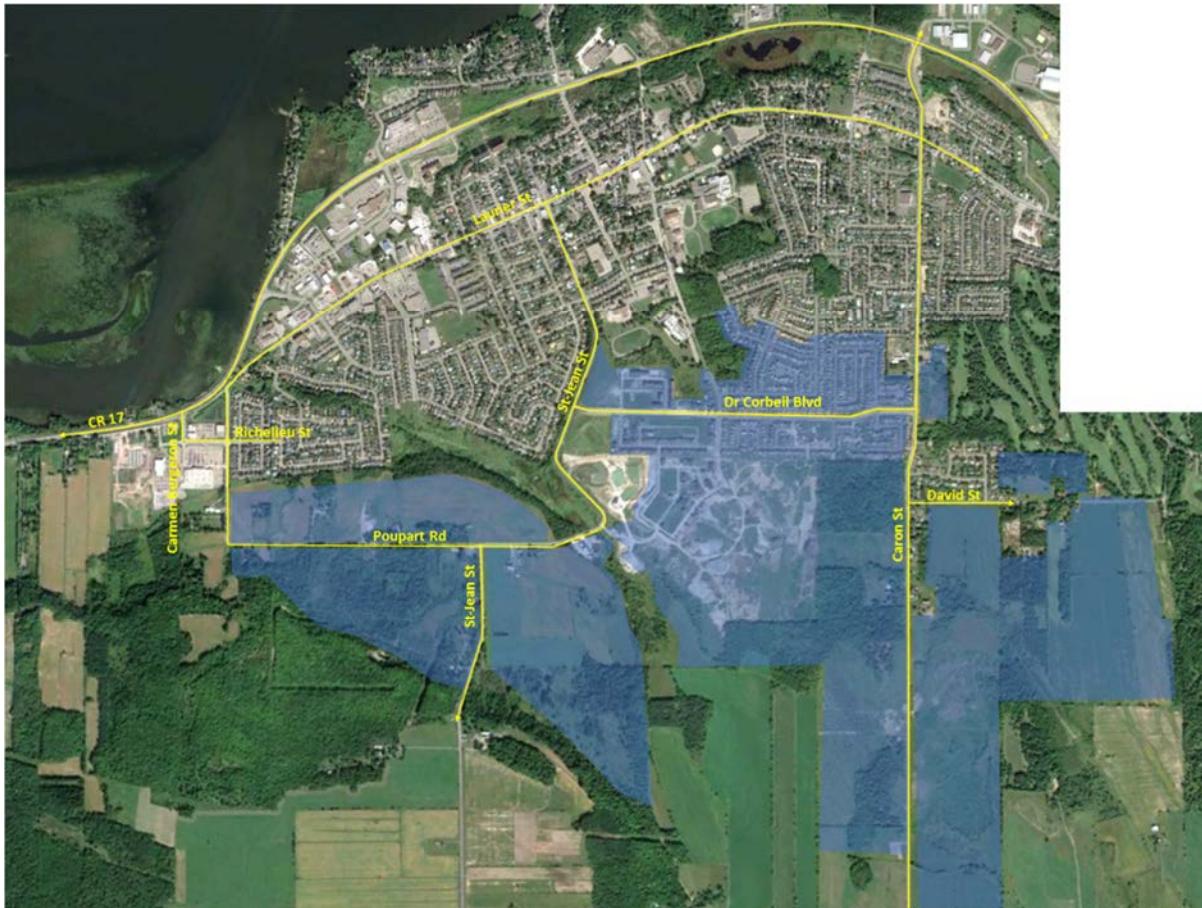


Exhibit 2-1: Study Area (Development area shown in blue)

- **County Road 17 (CR 17):** This east-west corridor connects the City of Clarence-Rockland to Ottawa on the west and Hawkesbury on the east. Within the City, the corridor cross-section is 2-lanes (one-lane in each direction) along the majority of its length. On-street parking is not permitted and no sidewalks are provided. The posted speed limit is 70 km/hr.
- **David Street:** This east-west corridor is a local, rural, 2-lane roadway. There are no sidewalks. The speed limit is 50 km/hr.
- **Dr. Corbeil Boulevard:** This east-west corridor connects St-Jean Street to Caron Street and was constructed within the last 10-years as a local 2-lane roadway. The roadway has on-street parking permitted on the north side and sidewalks on either the south side or along both sides along its length. The corridor accommodates bike lanes and has a speed limit of 50 km/hr.
- **Laurier Street:** This east-west corridor represents the City's "main street". The roadway has a 2-lane cross-section along the majority of its length and on-street

parking is permitted along many segments of the roadway. Sidewalks are provided on the north side or on both sides throughout its length. The posted speed limit is 50 km/hr.

- **Patricia Street:** This east-west corridor is a local, 2-lane roadway. Parking is permitted on both sides and a sidewalk is provided on the south side. The speed limit is 50 km/hr.
- **Poupart Road:** This east-west corridor connects the commercial development to the west, to the residential area around St-Jean Street. The corridor has a 2-lane cross-section and a paved surface treatment chip seal. There are no sidewalks along the majority of the length, with the exception of a sidewalk along the west side of the north-south section of roadway (between Laurier and the Walmart access). The speed limit is 50 km/hr.
- **Richelieu Street:** This east-west corridor has a 3-lane cross-section within the study area (between Carmen Bergeron St and Poupart Rd), where the center lane provides back-to-back left-turn auxiliary lanes. The section is intersected by Smart Centres commercial area and Walmart accesses. On-street parking is not permitted. Sidewalks are provided along both sides of the roadway. The speed limit is 50 km/hr.
- **St-Jean Street:** This north-south corridor connects Laurier Street to Poupart Rd (and continues further south as County Road 21). The corridor has a 2-lane cross-section. The roadway has designated on-street parking permitted on the west side (from Laurier Street to Raymond St) and a sidewalk located along the east side (from Laurier Street to Dr. Corbeil Blvd). The speed limit is 50 km/hr.

2.2 EXISTING PEDESTRIAN FACILITIES

Sidewalks currently exist along:

- St-Jean St, from Laurier Street to Dr. Corbeil Boulevard;
- Poupart Road in the vicinity of Richelieu Street and the commercial plaza;
- Dr. Corbeil Boulevard; and
- Caron Street, from CR 17 to David Street on the west side of the road.

Multi-use pathway (MUP) currently exist in the east-west direction south of Dr. Corbeil Boulevard from Caron Street to St-Jean Street.

2.3 EXISTING CYCLING FACILITIES

In general, there are no dedicated cycling lanes within the study area, with the exception that on-street cycling lanes are provided along Dr. Corbeil Boulevard. Very few cyclists were observed during the traffic count periods.

2.4 EXISTING TRANSIT PROVISIONS

Clarence-Rockland Transit (CR Transit) operates a commuter route in the morning and afternoon peak hours, providing service to Ottawa in the morning and return in the afternoon. Service is not provided on statutory holidays. There are two main routes:

- **#530A – Morris Village:** This route, going westbound in the morning, travels from CR 17, along Laurier Street, down Caron Street, along Dr. Corbeil Boulevard, down St-Jean Street and back onto Laurier Street and connects with CR 17. Ten (10) stops are provided along the route. The reverse route takes place in the afternoon; and
- **#530 – Laurier:** This route, going westbound in the morning, travels from CR 17, goes along the entire length of Laurier Street, and connects back to CR 17. Eight (8) stops are provided along the route. The reverse route takes place in the afternoon.

A total of 8 westbound trips are provided in the morning and 7 eastbound in the afternoon (a single westbound trip also takes place in the early afternoon as the first bus travels to Ottawa).

2.5 EXISTING TRAFFIC VOLUMES

Traffic counts were undertaken at the existing study area intersections during the week of September 10th, 2018, which accounted for school traffic. The traffic counts were undertaken during the morning (6:30am-to-9:00am) and afternoon (3:00pm-to-6:00pm) peak hours.

A review of Exhibit 2.1 indicates that the demand in the morning is greater in the westbound direction (vehicles traveling towards Ottawa) and the reverse trend is observed in the afternoon (where commuters return home).

3 TRAFFIC ANALYSIS

This TIS evaluated three (3) design horizon years: short-term (5-to-10 years), medium-term (10-to-20 years) and ultimate build-out. The forecast traffic volumes are based on existing (2018) traffic data and future developments within the study area. The following sections provide details on the forecast traffic volumes and analysis.

3.1 FUTURE DEVELOPMENT

Exhibit 3.1 illustrates the future developments that were accounted for in the forecasted traffic volumes. The future developments were segmented into three phases that included short-term, medium-term and ultimate build-out.

- In the short-term, over 2,000 units are anticipated to be constructed;
- In the medium-term, an additional 3,100 are anticipated to come on board; and
- At full build-out, an additional 3,900 units are anticipated, resulting in over 9,100 total units.

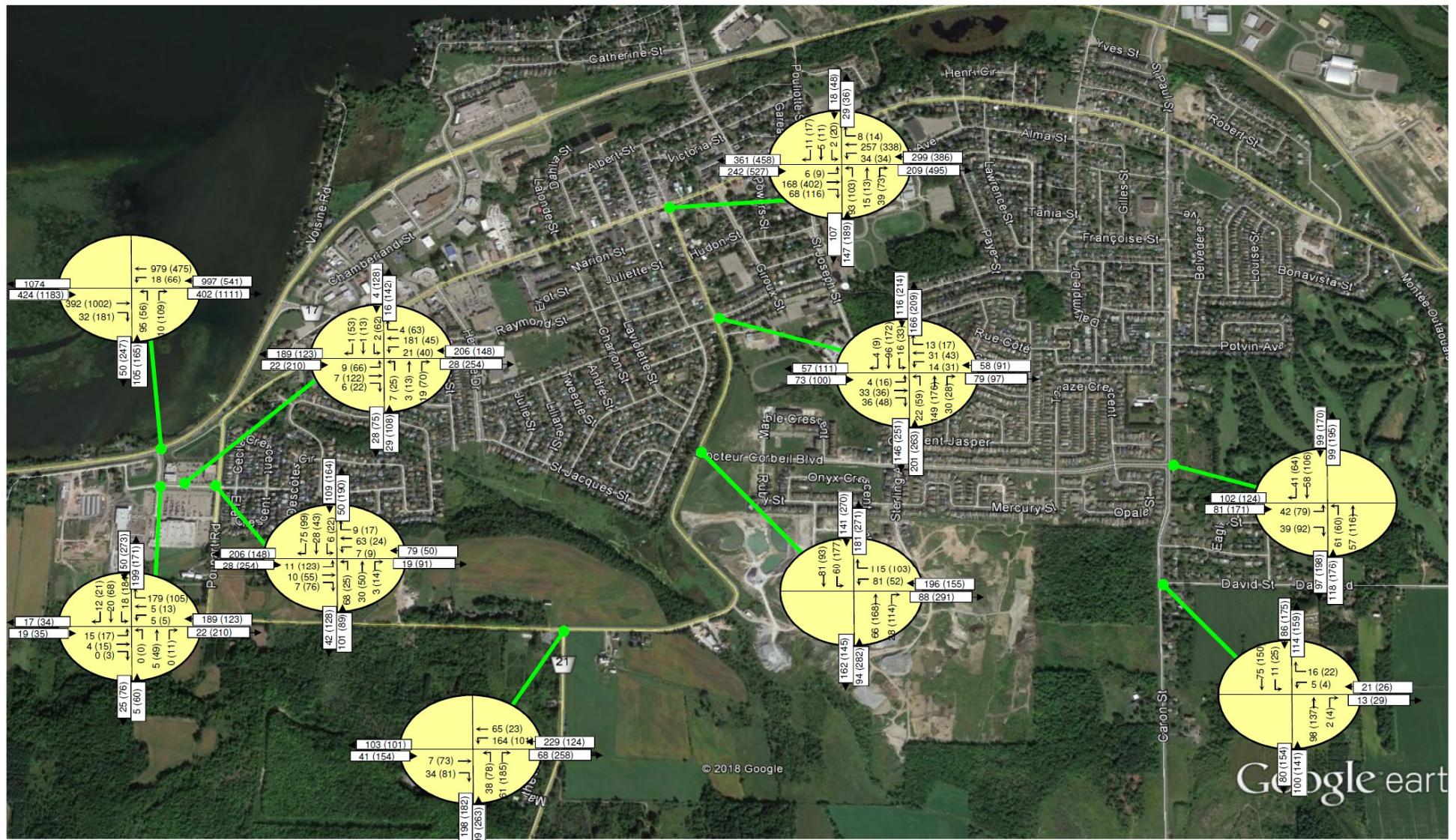


Exhibit 2.1: Existing (2018) Traffic Volumes

Format: Morning peak hour (afternoon peak hour)

3.2 TRIP GENERATION

The trip generation associated with the study area developments were estimated using the ITE Trip Generation Manual. The morning and afternoon peak hour rates were used to estimate the site traffic volumes. It has become a common and accepted practice to determine the volume of “person” trips to be generated by a given development. The purpose of this is to quantify the expected demands for the primary modes of transportation. In order to convert ITE rates to person trips, the rates obtained from the ITE Trip Generation Manual were adjusted by a factor of 1.3 passengers-per-vehicle to account for an inherent transit modal share and auto occupancy.

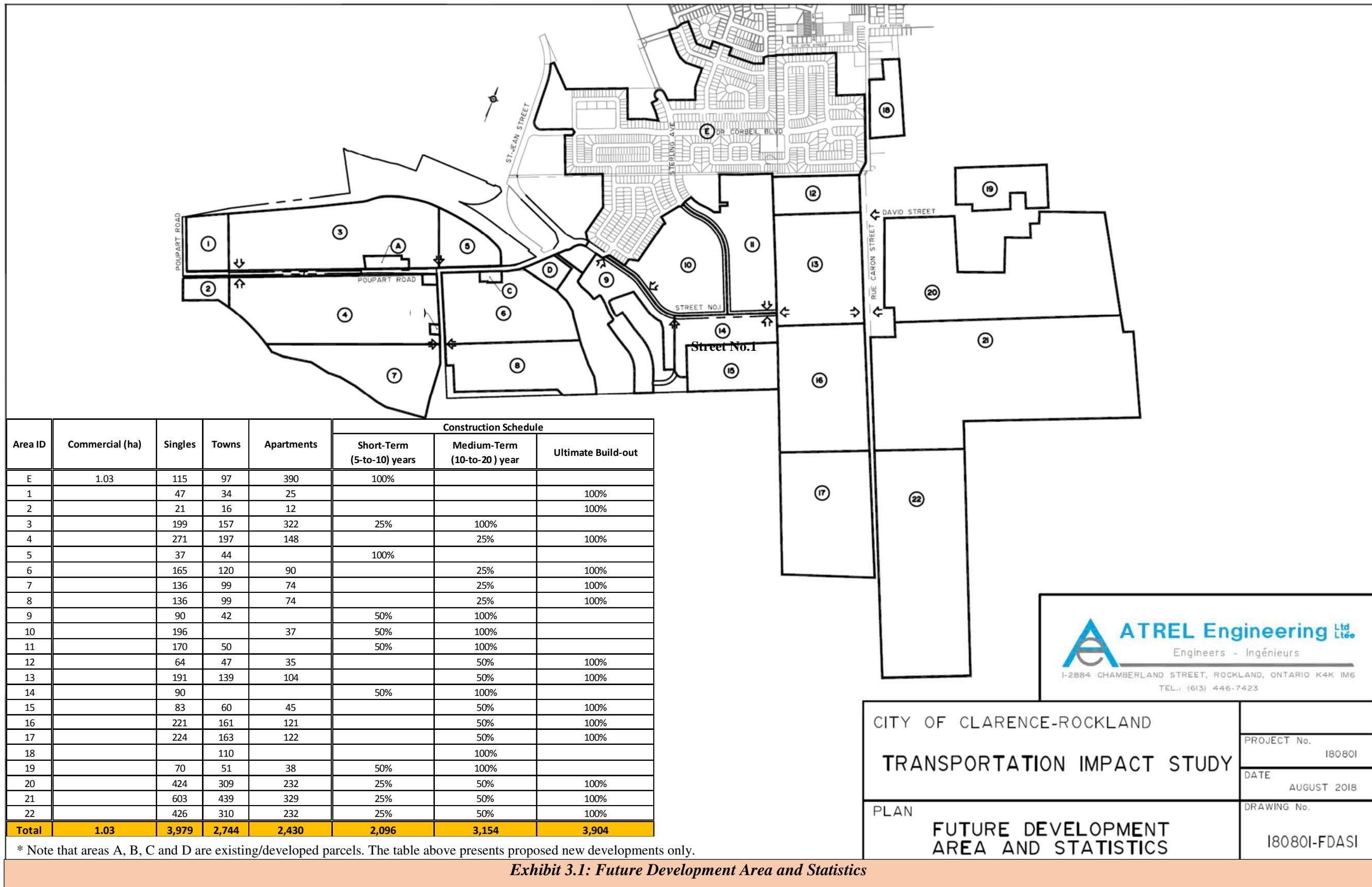
Table 3.1: ITE Trip Rates

| ITE Trip Rates | | | Modified Person Trips Rate | | | x 1.3 | | | |
|---------------------------|-----------|------|----------------------------|-----|---------------------------|-----------|------|-------|-----|
| Rate per unit | Pk Period | Rate | Split | | Rate per unit | Pk Period | Rate | Split | |
| | | | IN | OUT | | | | IN | OUT |
| Single Family Homes - 210 | AM | 0.75 | 25% | 75% | Single Family Homes - 210 | AM | 0.98 | 25% | 75% |
| | PM | 1.01 | 63% | 37% | | PM | 1.31 | 63% | 37% |
| Townhomes - 230 | AM | 0.44 | 17% | 83% | Townhomes - 230 | AM | 0.57 | 17% | 83% |
| | PM | 0.52 | 67% | 33% | | PM | 0.68 | 67% | 33% |
| Apartment - 220 | AM | 0.51 | 20% | 80% | Apartment - 220 | AM | 0.66 | 20% | 80% |
| | PM | 0.62 | 65% | 35% | | PM | 0.81 | 65% | 35% |

The person trips were then assigned to the primary modal shares (i.e. auto, passenger, transit and non-auto). Based on limited existing transit service and active mode facilities in the immediate study area, it was assumed that the auto driver modal share will be 85% and the remaining 15% will encompass passenger, transit, and non-auto modes.

Table 3.1: Build-Out Total Development – Person Trips by Modal Share

| Travel Mode | Mode Share | AM | | | PM | | |
|-------------------------------------|------------|--------------|--------------|--------------|--------------|--------------|--------------|
| | | In | Out | Total | In | Out | Total |
| Auto Driver | 85% | 1,481 | 4,473 | 5,954 | 4,936 | 3,019 | 7,955 |
| Passenger | 5% | 78 | 257 | 335 | 242 | 187 | 428 |
| Transit (Non-Auto) | 10% | | 509 | 509 | 581 | | 581 |
| Total Person Trips | 100% | 1,559 | 5,239 | 6,798 | 5,759 | 3,206 | 8,965 |
| Total Development Auto Trips | | 1,481 | 4,473 | 5,954 | 4,936 | 3,019 | 7,955 |



ATREL Engineering Ltd
Engineers - Ingénieurs
I-2884 CHAMBERLAND STREET, ROCKLAND, ONTARIO K4K 1M6
TEL.: (613) 446-7423

| | |
|---|-----------------------------|
| CITY OF CLARENCE-ROCKLAND | |
| TRANSPORTATION IMPACT STUDY | PROJECT No. I8080I |
| PLAN | DATE AUGUST 2018 |
| FUTURE DEVELOPMENT AREA AND STATISTICS | DRAWING No. I8080I-FDASI |

The total site traffic volumes generated by the proposed development have been estimated to be approximately 6,000 vehicle trips during the morning peak hour and 8,000 vehicle trips during the afternoon peak hour.

A small commercial development is also proposed within the study area located at the southwest corner of St-Jean Street / Street No.1 (area between “D” and “9” on Exhibit 3.1). The commercial development site trips are anticipated to be internal and pass-by trips from the community. Therefore, the traffic impacts of the commercial development are not anticipated to be significant.

3.3 TRIP DISTRIBUTION AND ASSIGNMENT

The traffic distribution assumptions were derived from the “*Place of work and commuting to work*” information obtained from Statistics Canada in the 2016 Census. The statistics indicate that the majority (~65%) of working residents commute to a different census subdivision. However, given the nature of the development (residential) and the lack of employment development in Rockland, the following traffic distribution assumptions were applied:

- 65% destined to/from west of the City of Rockland;
- 15% destined to/from south of the City of Rockland;
- 13% destined to/from east of the City of Rockland; and
- 7% remain within the City of Rockland.

3.4 FORECAST TRAFFIC VOLUMES

The forecast short-term, medium-term and ultimate traffic volumes were produced for the study area. Appendix “B” illustrates the site and forecast traffic volumes for the study area intersections.

3.5 INTERSECTION CAPACITY ANALYSIS

Intersection capacity analysis was undertaken for the existing and forecast traffic volumes for the study area intersections. Synchro 10™ was used to analyze stop control and traffic-controlled intersections. Roundabouts were analyzed using Sidra intersection analysis. For analysis purposes, it was assumed that a volume-to-capacity (v/c) ratio of greater than 0.92 was considered unsatisfactory.

3.5.1 Existing Traffic Analysis

Table 3.1 depicts a summary of the intersection capacity analysis results for the study area intersections (See Appendix A for detailed traffic analysis sheets). Existing signal timing was used for the intersection of CR 17 and Carmen Bergeron Street.

Table 3.1: Existing (2018) Intersection Capacity Analysis Results

| Intersection | Control Type | Morning Peak Hour | | Afternoon Peak Hour | |
|--------------------------------------|------------------------|-------------------|------------------------------|---------------------|------------------------------|
| | | Overall LOS | Critical Movement (LOS, V/C) | Overall LOS | Critical Movement (LOS, V/C) |
| CR 17 / Carmen Bergeron ¹ | Traffic Signal | C | WB-TH (C, 0.92) | E | EB-TH (F, 1.22) |
| CR 17 / Carmen Bergeron ² | Traffic Signal | C | WB-TH (C, 0.62) | C | EB-TH (D, 0.96) |
| Carmen Bergeron / Richelieu | All-Way Stop Control | A | WB-T/RT (A, 0.22) | A | WB-T/RT (A, 0.16) |
| Richelieu / Commercial Access | 2-Way Stop Control | B | NB (A, 0.04) | B | SB (B, 0.26) |
| Poupart / Richelieu | All-Way Stop Control | A | NB (A, 0.14) | A | SB (A, 0.22) |
| Poupart / St-Jean | All-Way Stop Control | A | WB (A, 0.30) | A | NB (A, 0.34) |
| St-Jean / Dr. Corbeil | Minor-leg Stop Control | B | WB (B, 0.26) | B | WB (B, 0.27) |
| St-Jean / Patricia | All-Way Stop Control | A | NB (A, 0.04) | A | NB (B, 0.38) |
| St-Jean / Laurier | Traffic Signal | B | WB (B, 0.37) | B | EB-TH (B, 0.65) |
| Caron / Dr. Corbeil | Minor-leg Stop Control | B | EB (B, 0.11) | B | EB (B, 0.26) |
| Caron / David | All-Way Stop Control | A | NB (A, 0.13) | A | NB (A, 0.18) |

1- Existing signal timing from County of Prescott-Russell

2- Optimized signal timing

The results indicate that all the intersections operate at satisfactory level of service except the intersection of CR 17 / Carmen Bergeron Street. The intersection operates at an overall level of service (LOS) “E” during the afternoon peak hour of travel demand. The critical movement was determined to be the eastbound (EB) movement with LOS “F” and v/c ratio of 1.22. With optimized signal timing (i.e. providing more time to the dominant movement), the EB-TH movement can be improved to LOS “D” with v/c ratio of 0.96 during the afternoon peak hour of travel demand.

3.5.2 Forecast Short-term (5-to-10 years) Traffic Analysis

By the short-term horizon year, it was assumed that:

- Roundabouts would be constructed at St-Jean Street / Dr. Corbeil Boulevard and St-Jean Street / Street No.1 Access into Morris Village development;
- Stop-Control configuration along Poupart west of the St-Jean Street slope hill;

- Stop-Control configuration along Caron Street; and
- 2-lane cross-sections along St-Jean Street, Poupart Road and Caron Street.

Table 3.2 below provides a summary of the short-term analysis results (See Appendix “D” for detailed analysis sheets).

Table 3.2: Short-Term Traffic Analysis

| <i>Intersection</i> | <i>Control Type</i> | <i>Morning Peak Hour</i> | | <i>Afternoon Peak Hour</i> | |
|-------------------------------|------------------------|--------------------------|-------------------------------------|----------------------------|-------------------------------------|
| | | <i>Overall LOS</i> | <i>Critical Movement (LOS, V/C)</i> | <i>Overall LOS</i> | <i>Critical Movement (LOS, V/C)</i> |
| CR 17 / Carmen Bergeron | Traffic Signal | F | WB-TH (F, 1.20) NB-LT (F, 1.00) | F | EB-TH (F, 1.38) |
| Carmen Bergeron / Richelieu | All-Way Stop Control | B | WB-T/R (A, 0.48) | B | SB-T/L (B, 0.49) |
| Richelieu / Commercial Access | 2-Way Stop Control | B | NB (A, 0.05) | C | SB (C, 0.44) |
| Poupart / Richelieu | All-Way Stop Control | B | NB (A, 0.46) | B | EB-T/R (B, 0.57) |
| Poupart / St-Jean | All-Way Stop Control | B | WB (A, 0.57) | B | NB (B, 0.54) |
| St-Jean / Dr. Corbeil | Roundabout | A | EB (A, 0.39) | A | SB (A, 0.48) |
| St-Jean / Patricia | All-Way Stop Control | B | NB (A, 0.52) | B | SB (B, 0.61) |
| St-Jean / Laurier | Traffic Signal | B | WB-TH (B, 0.39) NB-LT (C, 0.56) | B | EB-TH (B, 0.68) |
| Caron / Dr. Corbeil | Minor-leg Stop Control | C | EB (B, 0.33) | E | EB (E, 0.74) |
| Caron / David | All-Way Stop Control | B | NB (A, 0.55) | C | SB (C, 0.70) |
| St-Jean/Street No. 1 Access | Roundabout | A | SB (A, 0.28) | A | NB (A, 0.43) |
| Street No.1 / Sterling | Minor-leg Stop Control | A | SB (A, 0.005) | A | SB (A, 0.02) |
| Caron / Street No.1 | All-Way Stop Control | B | NB (B, 0.52) | C | SB (D, 0.79) |
| Poupart / Site Access | Minor-leg Stop Control | B | SB (B, 0.06) | B | SB (B, 0.04) |

All of the study area intersections operate at satisfactory level of service during the peak hours of travel demand, except for CR 17 / Carmen Bergeron Street. The intersection warrants more capacity in the east-west direction (over 1,500 vph in the peak direction). The CR 17 is at capacity today and warrants to be widened given the level of development that is anticipated to occur.

3.5.3 Forecast Medium-term (10-to-20 years) Traffic Analysis

By the medium-term horizon year, it was assumed that:

- Single roundabouts would be constructed along Poupart Road;

- Poupart Road would require to be extended further west to connect with CR 17¹; and
- Traffic signals would be required along Caron Street;
- 2-lane cross-sections along St-Jean Street, Poupart Road and Caron Street²; and 4-lanes along CR 17.

Table 3.3 below provides a summary of the medium-term analysis results.

Table 3.3: Medium-Term Traffic Analysis

| Intersection | Control Type | Morning Peak Hour | | Afternoon Peak Hour | |
|-------------------------------|------------------------|--------------------------|-------------------------------------|----------------------------|--|
| | | Overall LOS | Critical Movement (LOS, V/C) | Overall LOS | Critical Movement (LOS, V/C) |
| CR 17 / Carmen Bergeron | Traffic Signal | B | WB-TH (C, 0.91) | C | EB-TH (D, 1.00) |
| Carmen Bergeron / Richelieu | All-Way Stop Control | A | WB-T/R (A, 0.27) | A | SB-L/T (A, 0.18) |
| Richelieu / Commercial Access | 2-Way Stop Control | B | SB (B, 0.03) | C | SB (C, 0.40) |
| Poupart / Richelieu | All-Way Stop Control | A | NB (A, 0.30) | B | EB-LT (B, 0.34) |
| Poupart / St-Jean | Roundabout | C | WB (C, 0.94) | E | EB (F, 1.14) NB (F, 1.14) |
| St-Jean / Dr. Corbeil | Roundabout | A | WB (A, 0.44) | A | SB (A, 0.61) |
| St-Jean / Patricia | All-Way Stop Control | B | NB (C, 0.66) | C | SB (D, 0.80) |
| St-Jean / Laurier | Traffic Signal | B | NB-LT (C, 0.69) | B | WB (C, 0.76) |
| Caron / Dr. Corbeil | Traffic Signal | B | EB (C, 0.58) NB (B, 0.68) | C | EB (E, 0.85) SB (C, 0.95) |
| Caron / David | Traffic Signal | A | WB (B, 0.44) NB (A, 0.69) | A | SB (A, 0.80) |
| St-Jean/Street No. 1 Access | Roundabout | A | NB (A, 0.29) | A | SB (A, 0.86) |
| Street No.1 / Sterling | Minor-leg Stop Control | B | WB (B, 0.13) | C | SB (C, 0.23) |
| Caron / Street No.1 | Traffic Signal | B | SB (E, 0.59) | B | SB (C, 0.78) |
| Poupart Rd Extension | Roundabout | A | WB (A, 0.91) | C | EB (F, 1.03) |
| Poupart / Site Access | Roundabout | A | WB (A, 0.83) | C | EB (F, 1.04) |

All of the study area intersections operate at satisfactory level of service during the peak hours of travel demand, except for:

- **CR 17 / Carmen Bergeron Street:** The intersection still experiences slight congestion in the peak direction despite assuming a 4-lane CR 17. The EB movement results in a v/c ratio greater than 0.90 during the afternoon peak hour of travel demand.
 - **Poupart Road west of St-Jean Street:** The proposed single roundabouts from St-Jean Street to Poupart Road extension to CR 17 are anticipated to reach capacity (EB direction results in v/c ratio greater than 1.00) during the afternoon peak hour. The corridor should be monitored as development progresses to confirm if/when a 4-lane facility is required during the medium-term horizon year.
- Since the forecast assumes that a 2-lane Poupart and single roundabouts fail within

¹ Official Plan City of Clarence-Rockland - Schedule “B” – Road Network and Community Linkages

² Caron Street has an existing third lane along its length.

the medium-term horizon, consideration should be given to construct this corridor as a 4-lane cross-section with double roundabouts from the onset. Staging Poupart Road and the roundabouts from single-to-double within a short time period (potentially under 10-years) would result in throw-away infrastructure and is not recommended.

3.5.4 Forecast Ultimate Build-Out Traffic Analysis

By the full build-out year, it was assumed that:

- Poupart Road west of the Morris Village roundabout (as St-Jean/Poupart transition from north-south to east-west) would require a 4-lane cross-section to accommodate development growth; and
- Caron Street would require a 4-lane cross-section to accommodate development along Caron Street.

Table 3.4 below provides a summary of the build-out analysis.

Table 3.4: Build-Out Traffic Analysis

| Intersection | Control Type | Morning Peak Hour | | Afternoon Peak Hour | |
|-------------------------------|------------------------|-------------------|------------------------------|---------------------|---------------------------------------|
| | | Overall LOS | Critical Movement (LOS, V/C) | Overall LOS | Critical Movement (LOS, V/C) |
| CR 17 / Carmen Bergeron | Traffic Signal | D | WB-TH (C, 1.04) | F | EB-TH (F, 1.25) |
| Carmen Bergeron / Richelieu | All-Way Stop Control | A | WB-T/R (A, 0.29) | A | SB-L/T (A, 0.19) |
| Richelieu / Commercial Access | 2-Way Stop Control | B | SB (B, 0.04) | D | SB (C, 0.54) |
| Poupart / Richelieu | All-Way Stop Control | A | NB (A, 0.41) | B | EB-LT (B, 0.54) |
| Poupart / St-Jean | Roundabout | B | WB (C, 0.82) SB (E, 0.98) | C | EB (C, .96) NB-RT (F, 1.01) |
| St-Jean / Dr. Corbeil | Roundabout | A | WB (B, 0.51) | A | SB (A, 0.75) |
| St-Jean / Patricia | All-Way Stop Control | C | NB (D, 0.84) | E | SB (F, 1.03) |
| St-Jean / Laurier | Traffic Signal | B | NB-LT (C, 0.79) | C | WB (C, 0.86) |
| Caron / Dr. Corbeil | Traffic Signal | B | EB (C, 0.59) NB (B, 0.68) | C | EB (D, 0.80) SB (C, 0.91) |
| Caron / David | Traffic Signal | A | WB (C, 0.47) NB (B, 0.68) | A | SB (A, 0.80) |
| St-Jean/Street No. 1 Access | Roundabout | B | EB-LT (B, 0.76) | A | SB (A, 0.77) |
| Street No.1 / Sterling | Minor-leg Stop Control | C | SB (C, 0.35) | C | SB (F, 0.91) |
| Caron / Street No.1 | Traffic Signal | C | WB (E, 0.75) | C | SB (C, 0.83) |
| Poupart Rd Extension | Roundabout | A | WB (A, 0.77) | B | EB (C, 0.94) |
| Poupart / Site Access | Roundabout | B | WB (A, 0.77) SB (C, 0.83) | A | EB (A, 0.88) NB (C, 0.77) |

All of the study area intersections operate at satisfactory level of service during the peak hours of travel demand, except for:

- **CR 17 / Carmen Bergeron Street:** The intersection would continue to experience congestion in the peak direction despite assuming a 4-lane CR 17. The EB movement results in a v/c ratio greater than 0.90 during the afternoon peak hour of travel demand.

- ***St-Jean Street / Patricia Street:*** The intersection would experience failure level of service in the southbound direction during the afternoon peak hour. The intersection should be monitored as development progresses within the area to determine if traffic signals are warranted at this intersection.
- ***Poupart Road west of St-Jean Street:*** The proposed roundabouts from St-Jean Street to Poupart Road extension to CR 17 are anticipated to improve in terms of level of service with the additional capacity along Poupart Road. Albeit a few roundabouts would still experience slightly high v/c ratio at the build-out stage during the afternoon peak hour of travel demand.

4 INFRASTRUCTURE REQUIREMENTS

This section provides the infrastructure requirements for the study area for each phase of the development. The section is segmented into two part: study area corridors and intersections.

4.1 STUDY AREA CORRIDORS

Exhibit 4.1 illustrates the infrastructure envisioned to be required for each phase of the development. The exhibit provides link volumes at each location along the study area corridors. In summary:

- ***Poupart Road*** (west of Street No.1/St-Jean roundabout) is envisioned to be a 4-lane facility. The corridor reaches capacity by the medium-term horizon year. Should development progress as envisioned in this study, widening should be considered by or beyond the medium-term horizon year.
- ***St-Jean Street*** north of the Street No.1 roundabout is envisioned to remain a 2-lane corridor.
- ***Caron Street*** is envisioned to remain a 2-lane facility and would (at the time of the full build-out) require to be widened to 4-lanes to accommodate the growth on either side of the corridor. It is appreciated that some sections of Caron Street might not have sufficient right-of-way (ROW) to be able to be widened. This should be evaluated in details to determine if sufficient ROW exists to widen ultimately to 4-lanes.

4.2 STUDY AREA INTERSECTIONS

As development progresses within the study area, roundabouts are envisioned along Poupart Road and traffic signals along Caron Street for the study area intersections.

Traffic signals were selected along Caron Street as a preferred intersection control given the dominant direction alternates between the northbound (during the morning) and southbound (during the afternoon) direction. Traffic signals would provide the ability to control and provide more green time to the dominant movement during the peak direction.

Table 4.1 provides a summary of the intersection type and configuration for each phase of the development.

Table 4.1: Proposed Improvements

| Intersections | Short-Term Improvements | Medium-Term Improvements | Ultimate Build-Out Improvements |
|---------------------------------------|---|--|---|
| Caron / Dr. Corbeil | All-Way Stop Control | Traffic Signals ¹ • NB-LT = 40 m | Traffic Signals NB-LT = 40 m Storage |
| Caron / David St | 2-Way Stop Control | Traffic Signals ¹ • NB-LT = 30 m | Traffic Signals SB-LT = 30 m Storage |
| Caron / Street No.1 | All-Way Stop Control | Traffic Signals ¹ • NB-LT = 120 m • SB-LT = 120m • SB-RT = 120m • EB-LT = 35 • EB-RT = 125m • WB-LT = 30m • WB-RT = 120m | Traffic Signals • NB-LT = 120 m • SB-LT = 120m • SB-RT = 120m • EB-LT = 35 • EB-RT = 125m • WB-LT = 30m • WB-RT = 120m |
| St-Jean / Dr. Corbeil | Single lane roundabout | Single lane roundabout | Single lane roundabout |
| St-Jean / Street No.1 | Single lane roundabout with auxiliary lanes | Single lane roundabout with auxiliary lanes ² | Single lane roundabout with auxiliary lanes |
| St-Jean / Poupart | All-Way Stop Control | Single (or Double ³) lane roundabout | 2-lane roundabout with auxiliary lanes ² |
| Poupart / Site Access | 2-Way Stop Control | Single (or Double ³) lane roundabout ³ | 2-lane roundabout |
| Poupart / Poupart Rd Extension | N/A | Single (or Double ³) lane roundabout ³ | 2-lane roundabout |

- 1- The storage lengths were calculated assuming a cycle length of 120 sec, vehicle length of 7m and a safety factor of 1.5.
- 2- See Appendix “C” for conceptual level lay-out along with auxiliary lane.
- 3- The roundabouts can be constructed as 4-lanes during the medium term. The intersections should be monitored closely at this time to confirm a 4-lane Poupart facility is required. Consideration should be given to construct double roundabouts and a 4-lane Poupart Rd from the outset.

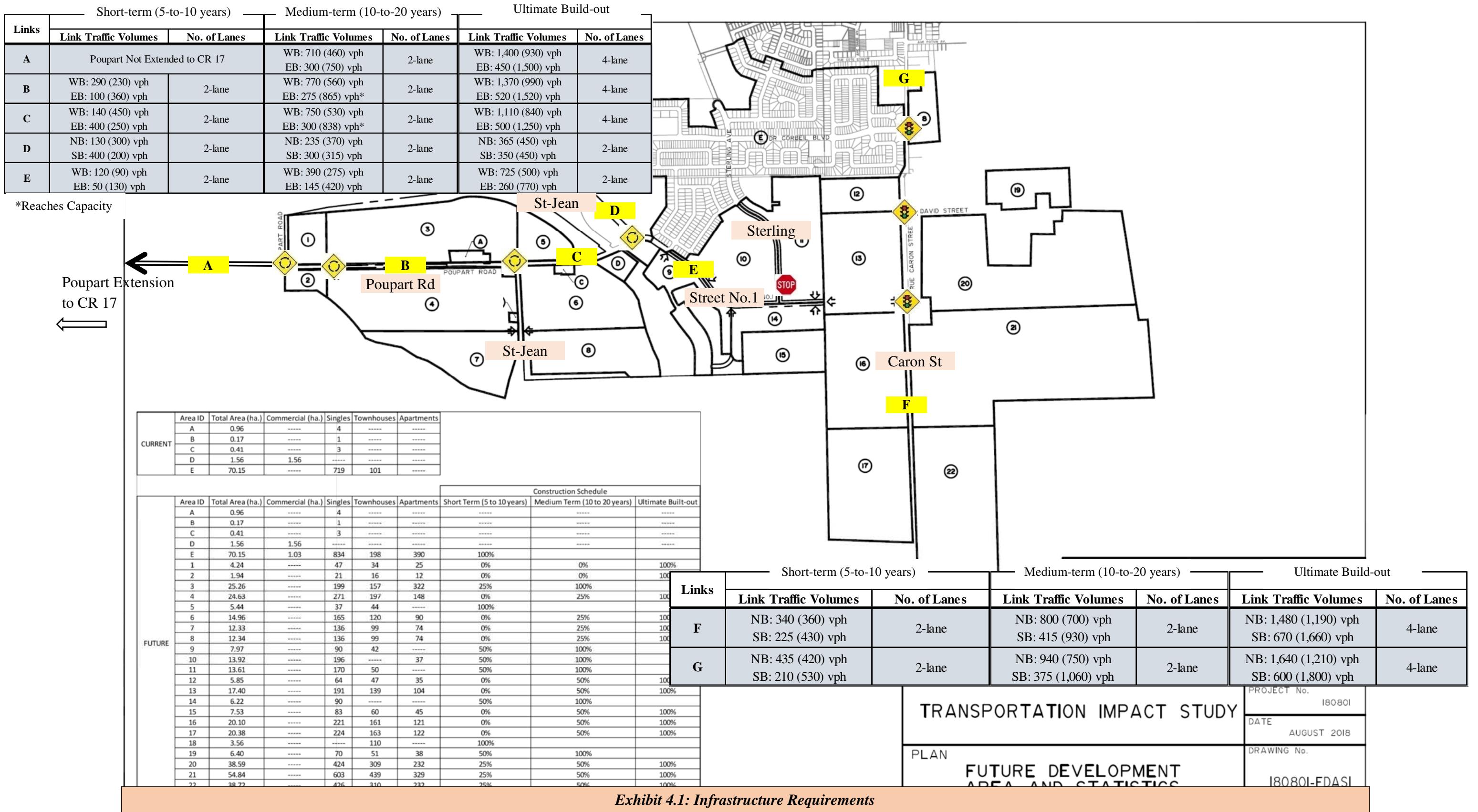


Exhibit 4.1: Infrastructure Requirements

5 DESIGN INPUT

This section provides input to the design component of the traffic study such as cross-section requirements, posted speeds, traffic calming measures, etc.

5.1 CROSS-SECTION CONFIGURATION (DIVIDED VS UNDIVIDED)

Poupart Road, from the proposed St-Jean Street (CR 21) roundabout to the proposed extension to CR 17 is anticipated to be a 4-lane facility. Whether the cross-section configuration be divided or undivided depends on many factors, which include access management, speed, traffic volumes, but the main factor is safety.

Raised medians are used to restrict turning movements and access points, and consequently decrease collision rates. Table 4.5.3 within the “*Geometric Design Guide for Canadian Roads*” (Transportation Association of Canada, June 2017) indicates that divided roads reduce the potential of collisions (i.e. head-on and side sweep collisions) by up to ~60% (based upon traffic volumes). As such, a divided cross-section along Poupart Road is recommended from the proposed St-Jean Street roundabout (west of the hill) to the proposed extension to CR 17.

It should be noted that although east of the St-Jean Street roundabout to the Street No. 1 roundabout is recommended to be a divided cross-section, a divided configuration cannot be accommodated due to the hill slope requirements along this segment of St-Jean Street (see Section 5.7 of this report).

5.2 POSTED SPEED

A posted speed limit of 50 km/hr is recommended along all roads within the study area (with the exception of CR 17 which has an existing posted speed of 70 km/hr).

Due to mainly residential land uses surrounding the corridors and the use of roundabouts along Poupart Road and St-Jean Street, it is recommended that a posted speed of 50 km/hr be maintained along this corridor. (A higher posted speed would result in vehicles speeding up/slowing down between each roundabout, which is considered undesirable and defeats the purpose of using roundabouts as traffic calming tools, see Section 5.3.)

5.3 TRAFFIC CALMING

Traffic calming measures are often implemented as a reactionary tool where high speed traffic, cut-through traffic or other local issues are identified in established areas.

As a precautionary traffic calming tool, roundabouts have been proposed along many intersections within the study area. Roundabouts naturally slow vehicular traffic and encourage drivers to be more aware by increasing cognitive load approaching intersections. Roundabouts are posted at 30 km/hr and, by their design, all vehicles approaching intersections slow down (as opposed to traffic signals where vehicles are often seen speeding up to ensure they cross on the green).

Other traffic calming features that can be considered at the design stage, specifically for local roads, include narrow lanes, horizontal deflections and accommodating on-street parking.

5.4 NON-AUTO MODE REQUIREMENTS

Along St-Jean Street, Poupart Road and Street No. 1, the design is to include a multi-use pathway and/or sidewalk to provide for a safe area for pedestrians and cyclists. The multi-use pathway (MUP) is proposed to be 2.5m wide and would accommodate cyclists and other forms of active transportation (skateboards, rollerblades, etc.); the pathway will connect to the existing path along the hydro corridor within the residential development. The sidewalk is proposed to be 2m wide. Both the multi-use pathway and sidewalk are recommended to be hard-surfaces (pavement for MUP and concrete for sidewalks) and cleared of snow in winter months.

5.5 RIGHT-OF-WAY REQUIREMENTS

Right-of-way widths were identified as 26m for two-lane roadways (with the exception of Poupart Road in the vicinity of the Walmart access which is currently 23m) and 30m for four-lane cross-sections (See proposed cross-sections presented by Atrel). Additional property would be needed at intersections to accommodate auxiliary lanes (particularly where roundabouts are provided, see Section 4.2).

- **Caron Street:** This corridor was recently constructed to a 3-lane cross-section. It is recommended that in the ultimate stage, this roadway be widened to 4-lanes. Traffic signals are proposed along the intersections at Dr Corbeil Boulevard, David Street and Street No. 1, however it would be prudent to protect right-of-way to accommodate roundabouts along this corridor, should they be preferred in the future.
- **Poupart Road:** A 4-lane divided cross-section is proposed within the 30 m right-of-way with 15m pavement width (3.75m per lane) and 5m median. Additional right-of-way is required at the roundabout locations. Poupart Road at Walmart narrows to ROW of 23m with pavement width of 8.5m.
- **St-Jean Street:** A 4-lane undivided cross-section is proposed within the 30 m right-of-way to Street No.1 (3.75m lane width). A 2-lane cross-section is envisioned north of Street No.1 roundabout with ROW of 26m and pavement width of 8.5m.

- **Street No.1:** This road is envisioned to accommodate 2 travel lanes with ROW of 26m. The pavement width is proposed to be 11m to accommodate on-street parking.

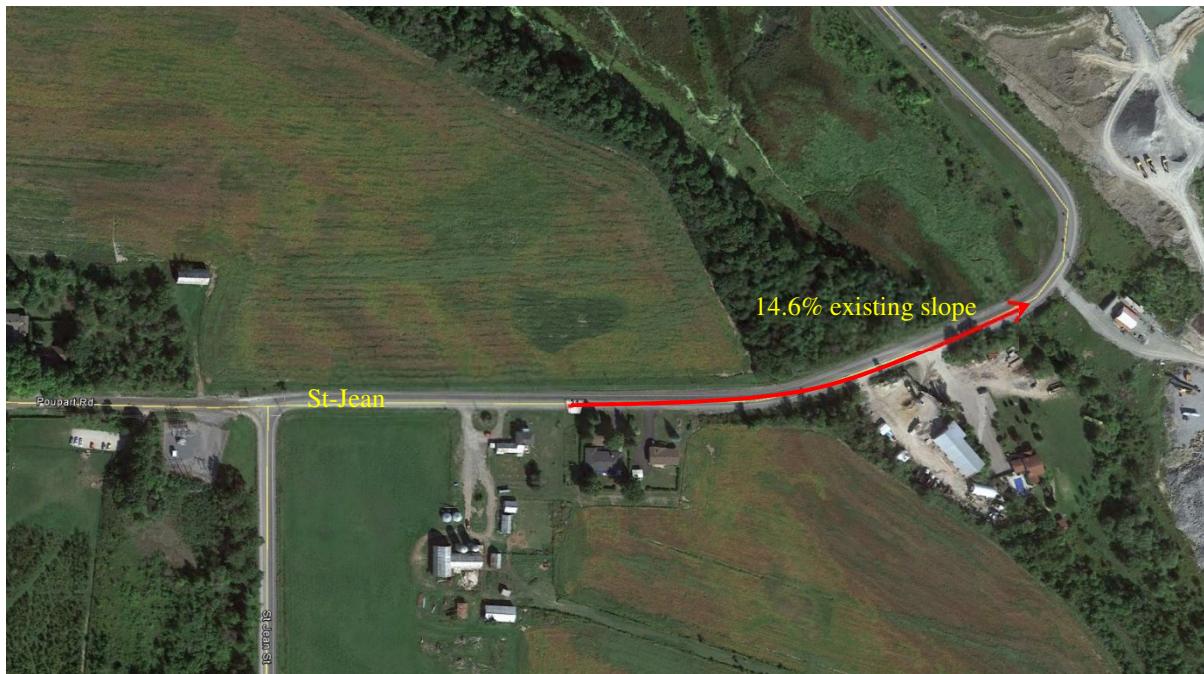
5.6 ROUNDABOUT CONFIGURATIONS

The following provides details regarding roundabout configuration and sizing:

- For all roundabouts, the roundabout circle diameter depends on the design vehicle that would traverse the roundabout. Typically for a single lane roundabout that would accommodate a WB-15 truck has an inscribed circle that ranges from 32-to-46m³. In the case of the St-Jean Street and Dr. Corbeil roundabout, a 32-to-36m inscribed circle for a single lane would suffice. This translates to a 6m circular lane width and 20m inner circle that includes a 3-to-4m apron for trucks.
- A 2-lane roundabout, that would typically accommodate a WB-15 or WB-20 truck, has an inscribed circle that ranges from 46-to-67m. A 46-to-50m inscribed circle for a 2-lane roundabout within this study area should suffice. This translates to 9.5-to-10m circular lane width and a 30m inner circle that includes a 3-to-4m apron for trucks.
Please note that the dimensions of the roundabout should be tested to accommodate the design vehicle that is envisioned to use the roundabout.

5.7 ST-JEAN STREET HILL SLOPE

St-Jean Street hill is located after the bend along St-Jean Street shown in the exhibit below with an existing slope of 14.6%. St-Jean Street is generally posted at 50km/hr. speed with an advisory speed of 30 km/hr in the vicinity of the hill because of the back-to-back curves on either side along St-Jean Street.



³ National Cooperative Highway Research Program (NCHRP) Report 672, Exhibit 6-9

It was assumed that the St-Jean Street hill will be classified (as development progresses) as an Urban Collector Undivided (UCU) roadway. Based on this classification and referencing Table 3.3.1 of the “*Geometric Design Guide for Canadian Roads*” (Transportation Association of Canada, June 2017), the maximum acceptable gradient for UCU (50km/hr) is 8% for rolling topography. This would flatten the slope by almost half of the existing slope.

5.8 POUPART RD & LAURIER ST CURVE

Poupart Rd and Laurier St are currently connected by back-to-back curves, where the main curve appears to have a radius of approximately 18m (which does not meet current design standards⁴). Two-way traffic volumes along this segment of roadway are currently 159 vehicles-per-hour in the morning and 354 vph in the afternoon. Traffic volume growth from the proposed developments are anticipated to be low (growth along this section of Poupart Rd/Laurier St is going to be more representative of background growth within the City itself), by the ultimate stage, forecast traffic volumes along this segment are anticipated to be 225 vph in the morning and 435 vph in the afternoon.

The existing curve should be reviewed and considerations should be given to increase the radius in this location if/when safety concerns arise.

6 ALTERNATE FUTURE ROUTES

The following section explores, at a high-level, potential alternative road options for the City of Clarence-Rockland.

6.1 EAST-WEST CORRIDOR

Given the growth that is anticipated to occur within the City of Clarence-Rockland in the next 20 years (and beyond), it is recommended that other road options be explored to provide an alternative entry/exit point to the City. The majority of traffic today use CR 17 to head to/from the City of Ottawa, which funnels all the traffic in and out of the City. Despite widening the CR 17 corridor, it reaches capacity in the next 20-to-30 years as development progresses. A potential alternative option is evaluating a second east-west corridor south of the study area (i.e. connecting Baseline Road to Innes Road – Exhibit 6.1). This would provide additional capacity and alleviate traffic along CR 17, Poupart Road and divert traffic south of the study area. A detailed network-wide assessment is recommended to be undertaken to determine the level of impact on traffic diversion.

⁴ “*Geometric Design Guide for Canadian Roads*”, (Transportation Association of Canada, June 2017). Table 3.2.8 states that, at a minimum, a 30m radius curve should be provided for a roadway with a design speed of 30km/hr.



6.2 NORTH-SOUTH CORRIDOR

It is anticipated that Caron Street would ultimately require to be 4-lanes to accommodate growth on either side of the corridor. The challenge with 4-lanning Caron Street is the potential ROW constraint along some segments of the road, especially north of David Street. Another option is to evaluate an alternative north-south corridor connecting the City of Clarence-Rockland to Baseline Road. Consideration should be given to having this roadway be somewhere between St-Jean St (CR 21) and Caron Street, or between Caron Street and Landry Street. This could alleviate the pressure from Caron Street and eliminate the need to 4-lane the corridor. Again, this option should be evaluated in more details as part of a network-wide study to quantify the benefits, a north-south corridor on its own, without an extended east-west connection (i.e. Baseline to Innes, as described above), would not likely provide much benefit.

7 FINDINGS AND RECOMMENDATIONS

The traffic study yields the following findings:

1. The total site traffic volumes generated by the proposed development has been estimated be approximately 6,000 vehicle trips during the morning peak hour and 8,000 vehicle trips during the afternoon peak hour.
2. By the short-term horizon year, it was assumed that:
 - a. Roundabouts are recommended to be constructed at St-Jean Street / Dr. Corbeil Boulevard and St-Jean Street / Street No.1 access into the Morris Village development (as development is anticipated to progress from the east to west);
 - b. Stop-Control configuration along Poupart west of the St-Jean Street slope hill;
 - c. Stop-Control configuration along Caron Street; and
 - d. A 2-lane St-Jean Street, Poupart Road and Caron Street.
3. By the medium-term horizon year, it was assumed that:
 - a. Single roundabouts and a 2-lane Poupart Road would be constructed. It should be acknowledged that a 2-lane Poupart Road does reach capacity by this horizon year if development progresses at the rate assumed within this report. The intersections should be monitored to confirm if a 4-lane Poupart facility and double roundabouts are preferred. Consideration should be given to construct double roundabouts and a 4-lane Poupart Rd from the outset to avoid staging costs and throw-away infrastructure;
 - b. Poupart Road would require to be extended further west to connect with CR 17;
 - c. Traffic signals would be required along Caron Street; and
 - d. 2-lane cross-sections along St-Jean Street and Caron Street and 4-lanes along CR 17.
4. By the full build-out year, it was assumed that:
 - a. Poupart Road west of the Morris Village roundabout would require a 4-lane cross-section to accommodate development growth; and
 - b. Caron Street would require a 4-lane cross-section to accommodate development along Caron Street. A detailed evaluation is recommended to ensure Caron Street has sufficient ROW to accommodate a 4-lane roadway.
5. A divided cross-section along Poupart Road is recommended from the proposed St-Jean Street roundabout (west of the hill) to the proposed extension to CR 17.
6. A posted speed limit of 50 km/hr is recommended along St-Jean Street, Poupart Road and Street No.1.
7. The maximum acceptable proposed gradient for St-Jean Street hill [UCU (50km/hr.)] is recommended to be 8% for rolling topography. This would flatten the slope by almost half of the existing slope.

8. The Poupart Road and Laurier Street curve should be monitored; considerations should be given to increase the radius in this location if/when safety concerns arise.
9. Roundabouts have been proposed along many intersections within the study area. Roundabouts naturally slow vehicular traffic and encourage drivers to be more aware. Roundabouts are posted at 30 km/hr and by their design act as a traffic calming measures. Other traffic calming features that can be considered at the design stage, specifically for local roads, include narrow lanes, horizontal deflections and accommodating on-street parking.
10. The design is to include a paved multi-use pathway and/or concrete sidewalk located within the boulevard to provide for a safe area for pedestrians and cyclists along St-Jean Street, Poupart Road and Street No. 1.

It is recommended that the City of Clarence-Rockland proceed to process the application of subdivision from a transportation perspective. Given the size of the development and long-term planning horizon years, the City of Clarence-Rockland is encouraged to undertake subsequent transportation impact studies as the development progresses to substantiate the medium and long-term assumptions (beyond five years) in this traffic study.

Yours Truly,

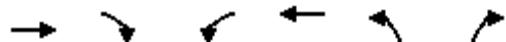
Arman Matti

Arman Matti, P. Eng.
Sr. Transportation Engineer
 December 2018

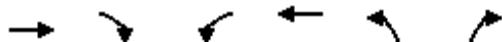


Appendix A

Existing Traffic Analysis



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 392 | 32 | 18 | 979 | 95 | 10 |
| Future Volume (vph) | 392 | 32 | 18 | 979 | 95 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 1810 | 1524 | 1703 | 1881 | 1770 | 1346 |
| Flt Permitted | | | 0.394 | | 0.950 | |
| Satd. Flow (perm) | 1810 | 1524 | 706 | 1881 | 1770 | 1346 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 35 | | | 11 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 5% | 6% | 6% | 1% | 2% | 20% |
| Adj. Flow (vph) | 426 | 35 | 20 | 1064 | 103 | 11 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 426 | 35 | 20 | 1064 | 103 | 11 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|-------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 56.0 | 56.0 | 21.0 | 77.0 | 26.0 | 26.0 |
| Total Split (%) | 54.4% | 54.4% | 20.4% | 74.8% | 25.2% | 25.2% |
| Maximum Green (s) | 49.8 | 49.8 | 14.8 | 70.8 | 20.8 | 20.8 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 48.4 | 48.4 | 52.6 | 52.6 | 21.4 | 21.4 |
| Actuated g/C Ratio | 0.56 | 0.56 | 0.61 | 0.61 | 0.25 | 0.25 |
| v/c Ratio | 0.42 | 0.04 | 0.04 | 0.92 | 0.23 | 0.03 |
| Control Delay | 12.6 | 3.6 | 5.6 | 27.8 | 32.1 | 17.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 12.6 | 3.6 | 5.6 | 27.8 | 32.1 | 17.1 |
| LOS | B | A | A | C | C | B |
| Approach Delay | 11.9 | | | 27.3 | 30.7 | |
| Approach LOS | B | | | C | C | |

Intersection Summary

Area Type: Other

Cycle Length: 103

Actuated Cycle Length: 85.7

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.92

Intersection Signal Delay: 23.3

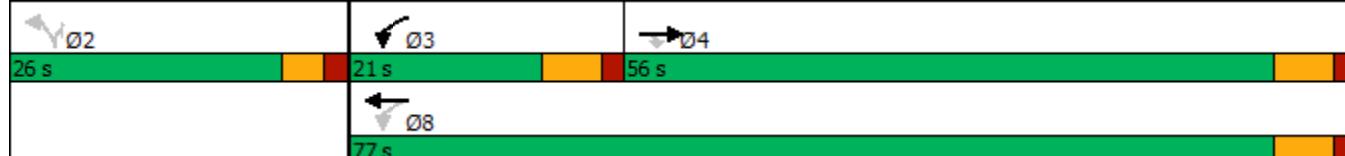
Intersection LOS: C

Intersection Capacity Utilization 66.3%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



Lanes, Volumes, Timings
17: St-Jean & Laurier

Existing Analysis AM
10/21/2018

| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 6 | 168 | 68 | 34 | 257 | 8 | 93 | 15 | 39 | 2 | 5 | 11 |
| Future Volume (vph) | 6 | 168 | 68 | 34 | 257 | 8 | 93 | 15 | 39 | 2 | 5 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.996 | | | 0.891 | | | 0.894 | |
| Flt Protected | | 0.998 | | | 0.994 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1843 | 1568 | 0 | 1875 | 0 | 1719 | 1479 | 0 | 1805 | 1604 | 0 |
| Flt Permitted | | 0.985 | | | 0.959 | | 0.746 | | | 0.719 | | |
| Satd. Flow (perm) | 0 | 1819 | 1568 | 0 | 1809 | 0 | 1350 | 1479 | 0 | 1366 | 1604 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 127 | | | 3 | | | 42 | | | 12 | |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 549.0 | | | 622.7 | | | 441.7 | | | 187.4 | |
| Travel Time (s) | | 39.5 | | | 44.8 | | | 31.8 | | | 13.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 3% | 3% | 3% | 0% | 0% | 5% | 13% | 15% | 0% | 20% | 0% |
| Adj. Flow (vph) | 7 | 183 | 74 | 37 | 279 | 9 | 101 | 16 | 42 | 2 | 5 | 12 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 190 | 74 | 0 | 325 | 0 | 101 | 58 | 0 | 2 | 17 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.1 | 23.1 | 23.1 | 10.1 | 23.1 | | 23.1 | 23.1 | | 23.1 | 23.1 | |
| Total Split (s) | 24.0 | 24.0 | 24.0 | 10.1 | 34.1 | | 25.9 | 25.9 | | 25.9 | 25.9 | |
| Total Split (%) | 40.0% | 40.0% | 40.0% | 16.8% | 56.8% | | 43.2% | 43.2% | | 43.2% | 43.2% | |
| Maximum Green (s) | 19.0 | 19.0 | 19.0 | 5.1 | 29.1 | | 20.9 | 20.9 | | 20.9 | 20.9 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 19.0 | 19.0 | | 29.1 | | 20.9 | 20.9 | | 20.9 | 20.9 | |
| Actuated g/C Ratio | | 0.32 | 0.32 | | 0.48 | | 0.35 | 0.35 | | 0.35 | 0.35 | |

Baseline

Synchro 10 Report

Page 1



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|------|------|-----|------|-----|------|------|-----|------|------|-----|-----|
| v/c Ratio | 0.33 | 0.13 | | 0.37 | | 0.21 | 0.11 | | 0.00 | 0.03 | | |
| Control Delay | 17.7 | 1.6 | | 11.1 | | 15.4 | 7.1 | | 13.0 | 8.8 | | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | 17.7 | 1.6 | | 11.1 | | 15.4 | 7.1 | | 13.0 | 8.8 | | |
| LOS | B | A | | B | | B | A | | B | A | | |
| Approach Delay | 13.2 | | | 11.1 | | | 12.4 | | | 9.3 | | |
| Approach LOS | B | | | B | | | B | | | A | | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.37

Intersection Signal Delay: 12.0

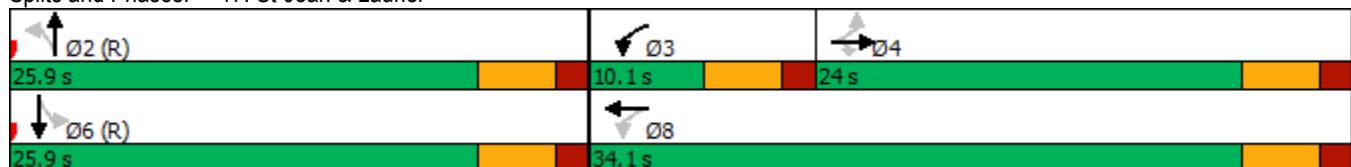
Intersection LOS: B

Intersection Capacity Utilization 49.4%

ICU Level of Service A

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



Intersection

Intersection Delay, s/veh 8.6
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 149 | 30 | 16 | 96 | 4 |
| Future Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 149 | 30 | 16 | 96 | 4 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 6 | 0 | 14 | 6 | 0 | 5 | 3 | 10 | 0 | 1 | 25 |
| Mvmt Flow | 4 | 36 | 39 | 15 | 34 | 14 | 24 | 162 | 33 | 17 | 104 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | | 1 | | | 1 | | | 1 | |
| HCM Control Delay | 8 | | | 8.4 | | | 9 | | | 8.3 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 11% | 5% | 24% | 14% |
| Vol Thru, % | 74% | 45% | 53% | 83% |
| Vol Right, % | 15% | 49% | 22% | 3% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 201 | 73 | 58 | 116 |
| LT Vol | 22 | 4 | 14 | 16 |
| Through Vol | 149 | 33 | 31 | 96 |
| RT Vol | 30 | 36 | 13 | 4 |
| Lane Flow Rate | 218 | 79 | 63 | 126 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.267 | 0.099 | 0.086 | 0.157 |
| Departure Headway (Hd) | 4.396 | 4.477 | 4.93 | 4.484 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 817 | 800 | 727 | 801 |
| Service Time | 2.419 | 2.506 | 2.96 | 2.51 |
| HCM Lane V/C Ratio | 0.267 | 0.099 | 0.087 | 0.157 |
| HCM Control Delay | 9 | 8 | 8.4 | 8.3 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 1.1 | 0.3 | 0.3 | 0.6 |

Intersection

Intersection Delay, s/veh 8

Intersection LOS A

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|----------|-----|-----|-----|-----|-----|-----|
|----------|-----|-----|-----|-----|-----|-----|

| | | | | | | |
|---------------------|---|--|--|--|--|--|
| Lane Configurations |  | | | | | |
|---------------------|---|--|--|--|--|--|

| | | | | | | |
|--------------------|---|----|----|---|----|----|
| Traffic Vol, veh/h | 5 | 16 | 98 | 2 | 11 | 75 |
|--------------------|---|----|----|---|----|----|

| | | | | | | |
|-------------------|---|----|----|---|----|----|
| Future Vol, veh/h | 5 | 16 | 98 | 2 | 11 | 75 |
|-------------------|---|----|----|---|----|----|

| | | | | | | |
|------------------|------|------|------|------|------|------|
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
|------------------|------|------|------|------|------|------|

| | | | | | | |
|-------------------|----|----|---|---|----|----|
| Heavy Vehicles, % | 40 | 13 | 9 | 0 | 18 | 13 |
|-------------------|----|----|---|---|----|----|

| | | | | | | |
|-----------|---|----|-----|---|----|----|
| Mvmt Flow | 5 | 17 | 107 | 2 | 12 | 82 |
|-----------|---|----|-----|---|----|----|

| | | | | | | |
|-----------------|---|---|---|---|---|---|
| Number of Lanes | 1 | 0 | 1 | 0 | 1 | 1 |
|-----------------|---|---|---|---|---|---|

| Approach | WB | NB | SB |
|----------|----|----|----|
|----------|----|----|----|

| | | | |
|-------------------|--|----|----|
| Opposing Approach | | SB | NB |
|-------------------|--|----|----|

| | | | |
|----------------|---|---|---|
| Opposing Lanes | 0 | 2 | 1 |
|----------------|---|---|---|

| | | | |
|---------------------------|----|--|----|
| Conflicting Approach Left | NB | | WB |
|---------------------------|----|--|----|

| | | | |
|------------------------|---|---|---|
| Conflicting Lanes Left | 1 | 0 | 1 |
|------------------------|---|---|---|

| | | | |
|----------------------------|----|--|----|
| Conflicting Approach Right | SB | | WB |
|----------------------------|----|--|----|

| | | | |
|-------------------------|---|---|---|
| Conflicting Lanes Right | 2 | 1 | 0 |
|-------------------------|---|---|---|

| | | | |
|-------------------|-----|-----|-----|
| HCM Control Delay | 7.8 | 7.9 | 8.1 |
|-------------------|-----|-----|-----|

| | | | |
|---------|---|---|---|
| HCM LOS | A | A | A |
|---------|---|---|---|

| Lane | NBLn1 | WBLn1 | SBLn1 | SBLn2 |
|------|-------|-------|-------|-------|
|------|-------|-------|-------|-------|

| | | | | |
|-------------|----|-----|------|----|
| Vol Left, % | 0% | 24% | 100% | 0% |
|-------------|----|-----|------|----|

| | | | | |
|-------------|-----|----|----|------|
| Vol Thru, % | 98% | 0% | 0% | 100% |
|-------------|-----|----|----|------|

| | | | | |
|--------------|----|-----|----|----|
| Vol Right, % | 2% | 76% | 0% | 0% |
|--------------|----|-----|----|----|

| | | | | |
|--------------|------|------|------|------|
| Sign Control | Stop | Stop | Stop | Stop |
|--------------|------|------|------|------|

| | | | | |
|---------------------|-----|----|----|----|
| Traffic Vol by Lane | 100 | 21 | 11 | 75 |
|---------------------|-----|----|----|----|

| | | | | |
|--------|---|---|----|---|
| LT Vol | 0 | 5 | 11 | 0 |
|--------|---|---|----|---|

| | | | | |
|-------------|----|---|---|----|
| Through Vol | 98 | 0 | 0 | 75 |
|-------------|----|---|---|----|

| | | | | |
|--------|---|----|---|---|
| RT Vol | 2 | 16 | 0 | 0 |
|--------|---|----|---|---|

| | | | | |
|----------------|-----|----|----|----|
| Lane Flow Rate | 109 | 23 | 12 | 82 |
|----------------|-----|----|----|----|

| | | | | |
|--------------|---|---|---|---|
| Geometry Grp | 5 | 2 | 7 | 7 |
|--------------|---|---|---|---|

| | | | | |
|--------------------|-------|-------|-------|-------|
| Degree of Util (X) | 0.128 | 0.029 | 0.018 | 0.109 |
|--------------------|-------|-------|-------|-------|

| | | | | |
|------------------------|-------|-------|-----|-------|
| Departure Headway (Hd) | 4.249 | 4.649 | 5.4 | 4.815 |
|------------------------|-------|-------|-----|-------|

| | | | | |
|------------------|-----|-----|-----|-----|
| Convergence, Y/N | Yes | Yes | Yes | Yes |
|------------------|-----|-----|-----|-----|

| | | | | |
|-----|-----|-----|-----|-----|
| Cap | 838 | 775 | 662 | 743 |
|-----|-----|-----|-----|-----|

| | | | | |
|--------------|-------|-------|-------|------|
| Service Time | 2.303 | 2.649 | 3.136 | 2.55 |
|--------------|-------|-------|-------|------|

| | | | | |
|--------------------|------|------|-------|------|
| HCM Lane V/C Ratio | 0.13 | 0.03 | 0.018 | 0.11 |
|--------------------|------|------|-------|------|

| | | | | |
|-------------------|-----|-----|-----|-----|
| HCM Control Delay | 7.9 | 7.8 | 8.2 | 8.1 |
|-------------------|-----|-----|-----|-----|

| | | | | |
|--------------|---|---|---|---|
| HCM Lane LOS | A | A | A | A |
|--------------|---|---|---|---|

| | | | | |
|-----------------|-----|-----|-----|-----|
| HCM 95th-tile Q | 0.4 | 0.1 | 0.1 | 0.4 |
|-----------------|-----|-----|-----|-----|

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|-------|-------|------|
| Int Delay, s/veh | 6 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | W | B | | | A | |
| Traffic Vol, veh/h | 81 | 115 | 66 | 28 | 60 | 81 |
| Future Vol, veh/h | 81 | 115 | 66 | 28 | 60 | 81 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 4 | 2 | 7 | 2 | 2 |
| Mvmt Flow | 88 | 125 | 72 | 30 | 65 | 88 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 305 | 87 | 0 | 0 | 102 | 0 |
| Stage 1 | 87 | - | - | - | - | - |
| Stage 2 | 218 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.24 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.336 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 691 | 966 | - | - | 1490 | - |
| Stage 1 | 941 | - | - | - | - | - |
| Stage 2 | 823 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 659 | 966 | - | - | 1490 | - |
| Mov Cap-2 Maneuver | 659 | - | - | - | - | - |
| Stage 1 | 898 | - | - | - | - | - |
| Stage 2 | 823 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay, s | 11 | 0 | 3.2 | | | |
| HCM LOS | B | | | | | |
| Minor Lane/Major Mvmt | NBT | NBR | WBLn1 | SBL | SBT | |
| Capacity (veh/h) | - | - | 810 | 1490 | - | |
| HCM Lane V/C Ratio | - | - | 0.263 | 0.044 | - | |
| HCM Control Delay (s) | - | - | 11 | 7.5 | 0 | |
| HCM Lane LOS | - | - | B | A | A | |
| HCM 95th %tile Q(veh) | - | - | 1.1 | 0.1 | - | |

Intersection

Intersection Delay, s/veh 8.7
Intersection LOS A

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|------|------|------|------|------|------|
| Lane Configurations | ↔ | | ↑ | ↔ | | |
| Traffic Vol, veh/h | 7 | 34 | 164 | 65 | 38 | 61 |
| Future Vol, veh/h | 7 | 34 | 164 | 65 | 38 | 61 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 43 | 0 | 1 | 0 | 0 | 5 |
| Mvmt Flow | 8 | 37 | 178 | 71 | 41 | 66 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB | WB | | NB | | |
| Opposing Approach | WB | | EB | | | |
| Opposing Lanes | 1 | | 1 | | 0 | |
| Conflicting Approach Left | | | NB | | EB | |
| Conflicting Lanes Left | 0 | | 1 | | 1 | |
| Conflicting Approach Right | NB | | | WB | | |
| Conflicting Lanes Right | 1 | | 0 | | 1 | |
| HCM Control Delay | 7.9 | | 9.2 | | 7.9 | |
| HCM LOS | A | | A | | A | |

| Lane | NBLn1 | EBLn1 | WBLn1 |
|------------------------|-------|-------|-------|
| Vol Left, % | 38% | 0% | 72% |
| Vol Thru, % | 0% | 17% | 28% |
| Vol Right, % | 62% | 83% | 0% |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 99 | 41 | 229 |
| LT Vol | 38 | 0 | 164 |
| Through Vol | 0 | 7 | 65 |
| RT Vol | 61 | 34 | 0 |
| Lane Flow Rate | 108 | 45 | 249 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.128 | 0.057 | 0.296 |
| Departure Headway (Hd) | 4.282 | 4.639 | 4.285 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 843 | 775 | 829 |
| Service Time | 2.283 | 2.65 | 2.364 |
| HCM Lane V/C Ratio | 0.128 | 0.058 | 0.3 |
| HCM Control Delay | 7.9 | 7.9 | 9.2 |
| HCM Lane LOS | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.2 | 1.2 |

Intersection

Intersection Delay, s/veh 7.9

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↓ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 11 | 10 | 7 | 7 | 63 | 9 | 68 | 30 | 3 | 6 | 28 | 75 |
| Future Vol, veh/h | 11 | 10 | 7 | 7 | 63 | 9 | 68 | 30 | 3 | 6 | 28 | 75 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 22 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 33 | 0 | 4 | 0 |
| Mvmt Flow | 12 | 11 | 8 | 8 | 68 | 10 | 74 | 33 | 3 | 7 | 30 | 82 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 8.1 | | | 8 | | | 8.2 | | | 7.5 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 67% | 100% | 0% | 9% | 6% |
| Vol Thru, % | 30% | 0% | 59% | 80% | 26% |
| Vol Right, % | 3% | 0% | 41% | 11% | 69% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 101 | 11 | 17 | 79 | 109 |
| LT Vol | 68 | 11 | 0 | 7 | 6 |
| Through Vol | 30 | 0 | 10 | 63 | 28 |
| RT Vol | 3 | 0 | 7 | 9 | 75 |
| Lane Flow Rate | 110 | 12 | 18 | 86 | 118 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.136 | 0.02 | 0.025 | 0.107 | 0.128 |
| Departure Headway (Hd) | 4.444 | 5.948 | 4.779 | 4.484 | 3.897 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 809 | 604 | 751 | 801 | 923 |
| Service Time | 2.457 | 3.666 | 2.497 | 2.501 | 1.91 |
| HCM Lane V/C Ratio | 0.136 | 0.02 | 0.024 | 0.107 | 0.128 |
| HCM Control Delay | 8.2 | 8.8 | 7.6 | 8 | 7.5 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.5 | 0.1 | 0.1 | 0.4 | 0.4 |

Intersection

Intersection Delay, s/veh 7.9

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | 0 | 5 | 5 | 179 | 0 | 5 | 0 | 18 | 20 | 12 |
| Traffic Vol, veh/h | 15 | 4 | 0 | 5 | 5 | 179 | 0 | 5 | 0 | 18 | 20 | 12 |
| Future Vol, veh/h | 15 | 4 | 0 | 5 | 5 | 179 | 0 | 5 | 0 | 18 | 20 | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 |
| Mvmt Flow | 16 | 4 | 0 | 5 | 5 | 195 | 0 | 5 | 0 | 20 | 22 | 13 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 2 | | | 2 | | | 2 | | | 2 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 2 | | | 2 | | | 2 | | | 2 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 2 | | | 2 | | | 2 | | | 2 | | |
| HCM Control Delay | 8 | | | 7.8 | | | 6.9 | | | 8.1 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 47% | 0% |
| Vol Thru, % | 100% | 100% | 0% | 100% | 0% | 3% | 53% | 0% |
| Vol Right, % | 0% | 0% | 0% | 0% | 0% | 97% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 3 | 3 | 15 | 4 | 5 | 184 | 38 | 12 |
| LT Vol | 0 | 0 | 15 | 0 | 5 | 0 | 18 | 0 |
| Through Vol | 3 | 3 | 0 | 4 | 0 | 5 | 20 | 0 |
| RT Vol | 0 | 0 | 0 | 0 | 0 | 179 | 0 | 12 |
| Lane Flow Rate | 3 | 3 | 16 | 4 | 5 | 200 | 41 | 13 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.004 | 0.003 | 0.024 | 0.006 | 0.008 | 0.218 | 0.061 | 0.016 |
| Departure Headway (Hd) | 5.041 | 3.335 | 5.206 | 4.705 | 5.112 | 3.93 | 5.331 | 4.289 |
| Convergence, Y/N | Yes |
| Cap | 714 | 1079 | 680 | 751 | 695 | 904 | 676 | 839 |
| Service Time | 2.743 | 1.036 | 2.995 | 2.494 | 2.879 | 1.696 | 3.032 | 1.99 |
| HCM Lane V/C Ratio | 0.004 | 0.003 | 0.024 | 0.005 | 0.007 | 0.221 | 0.061 | 0.015 |
| HCM Control Delay | 7.8 | 6 | 8.1 | 7.5 | 7.9 | 7.8 | 8.4 | 7.1 |
| HCM Lane LOS | A | A | A | A | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.1 | 0 | 0 | 0.8 | 0.2 | 0 |

| Intersection | | | | | | |
|--------------------------|--------|--------|-------|--------|------|------|
| Int Delay, s/veh | 4.4 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 42 | 39 | 61 | 57 | 58 | 41 |
| Future Vol, veh/h | 42 | 39 | 61 | 57 | 58 | 41 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 400 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 13 | 13 | 9 | 0 | 10 |
| Mvmt Flow | 46 | 42 | 66 | 62 | 63 | 45 |
| Major/Minor | Minor2 | Major1 | | Major2 | | |
| Conflicting Flow All | 280 | 86 | 108 | 0 | - | 0 |
| Stage 1 | 86 | - | - | - | - | - |
| Stage 2 | 194 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.33 | 4.23 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.417 | 2.317 | - | - | - |
| Pot Cap-1 Maneuver | 710 | 943 | 1417 | - | - | - |
| Stage 1 | 937 | - | - | - | - | - |
| Stage 2 | 839 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 677 | 943 | 1417 | - | - | - |
| Mov Cap-2 Maneuver | 677 | - | - | - | - | - |
| Stage 1 | 893 | - | - | - | - | - |
| Stage 2 | 839 | - | - | - | - | - |
| Approach | EB | NB | | SB | | |
| HCM Control Delay, s | 10.2 | 4 | | 0 | | |
| HCM LOS | B | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR | |
| Capacity (veh/h) | 1417 | - | 783 | - | - | |
| HCM Lane V/C Ratio | 0.047 | - | 0.112 | - | - | |
| HCM Control Delay (s) | 7.7 | - | 10.2 | - | - | |
| HCM Lane LOS | A | - | B | - | - | |
| HCM 95th %tile Q(veh) | 0.1 | - | 0.4 | - | - | |

| Intersection | | | | | | | | | | | | | | | | | | | |
|--------------------------|-------|--------|------|------|--------|------|------|--------|-------|------|------|------|--|--|--|--|--|--|--|
| Int Delay, s/veh | 2 | | | | | | | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | | | | | |
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | | | | | | | |
| Traffic Vol, veh/h | 9 | 7 | 6 | 21 | 181 | 4 | 7 | 3 | 19 | 2 | 1 | 1 | | | | | | | |
| Future Vol, veh/h | 9 | 7 | 6 | 21 | 181 | 4 | 7 | 3 | 19 | 2 | 1 | 1 | | | | | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | | | | | | | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | | | | | | | |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - | | | | | | | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | | | | | | | |
| Heavy Vehicles, % | 22 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Mvmt Flow | 10 | 8 | 7 | 23 | 197 | 4 | 8 | 3 | 21 | 2 | 1 | 1 | | | | | | | |
| Major/Minor | | | | | | | | | | | | | | | | | | | |
| Major1 | | Major2 | | | Minor1 | | | Minor2 | | | | | | | | | | | |
| Conflicting Flow All | 201 | 0 | 0 | 15 | 0 | 0 | 278 | 279 | 12 | 289 | 280 | 199 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 32 | 32 | - | 245 | 245 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 246 | 247 | - | 44 | 35 | - | | | | | | | |
| Critical Hdwy | 4.32 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | | | | | | | |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | | | | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | | | | | |
| Follow-up Hdwy | 2.398 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 | | | | | | | |
| Pot Cap-1 Maneuver | 1260 | - | - | 1616 | - | - | 678 | 632 | 1074 | 667 | 632 | 847 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 990 | 872 | - | 763 | 707 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 762 | 706 | - | 975 | 870 | - | | | | | | | |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - | | | | | | | |
| Mov Cap-1 Maneuver | 1260 | - | - | 1616 | - | - | 665 | 618 | 1074 | 640 | 618 | 847 | | | | | | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 665 | 618 | - | 640 | 618 | - | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 982 | 865 | - | 757 | 697 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 749 | 696 | - | 945 | 863 | - | | | | | | | |
| Approach | | | | | | | | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | | | | | | | | |
| HCM Control Delay, s | 3.2 | | 0.7 | | | 9.3 | | | 10.4 | | | | | | | | | | |
| HCM LOS | A | | | | | | B | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | | | | | | | | | | | | | | | | | | |
| Capacity (veh/h) | 877 | 1260 | - | - | 1616 | - | - | - | 675 | | | | | | | | | | |
| HCM Lane V/C Ratio | 0.036 | 0.008 | - | - | 0.014 | - | - | - | 0.006 | | | | | | | | | | |
| HCM Control Delay (s) | 9.3 | 7.9 | - | - | 7.3 | - | - | - | 10.4 | | | | | | | | | | |
| HCM Lane LOS | A | A | - | - | A | - | - | - | B | | | | | | | | | | |
| HCM 95th %tile Q(veh) | 0.1 | 0 | - | - | 0 | - | - | - | 0 | | | | | | | | | | |

| | → | ↓ | ↖ | ← | ↗ | ↑ |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 1002 | 181 | 66 | 475 | 56 | 109 |
| Future Volume (vph) | 1002 | 181 | 66 | 475 | 56 | 109 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 1845 | 1599 | 1752 | 1863 | 1805 | 1615 |
| Flt Permitted | | | 0.071 | | 0.950 | |
| Satd. Flow (perm) | 1845 | 1599 | 131 | 1863 | 1805 | 1615 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 111 | | | 118 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 3% | 1% | 3% | 2% | 0% | 0% |
| Adj. Flow (vph) | 1089 | 197 | 72 | 516 | 61 | 118 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 1089 | 197 | 72 | 516 | 61 | 118 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|-------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 26.2 | 26.2 |
| Total Split (s) | 56.0 | 56.0 | 26.0 | 82.0 | 36.0 | 36.0 |
| Total Split (%) | 47.5% | 47.5% | 22.0% | 69.5% | 30.5% | 30.5% |
| Maximum Green (s) | 49.8 | 49.8 | 19.8 | 75.8 | 30.8 | 30.8 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 50.0 | 50.0 | 60.8 | 60.8 | 30.9 | 30.9 |
| Actuated g/C Ratio | 0.48 | 0.48 | 0.59 | 0.59 | 0.30 | 0.30 |
| v/c Ratio | 1.22 | 0.24 | 0.38 | 0.47 | 0.11 | 0.21 |
| Control Delay | 135.9 | 8.3 | 14.9 | 13.6 | 28.6 | 6.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 135.9 | 8.3 | 14.9 | 13.6 | 28.6 | 6.4 |
| LOS | F | A | B | B | C | A |
| Approach Delay | 116.4 | | | 13.7 | 13.9 | |
| Approach LOS | F | | | B | B | |

Intersection Summary

Area Type: Other

Cycle Length: 118

Actuated Cycle Length: 103.1

Natural Cycle: 100

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 1.22

Intersection Signal Delay: 78.0

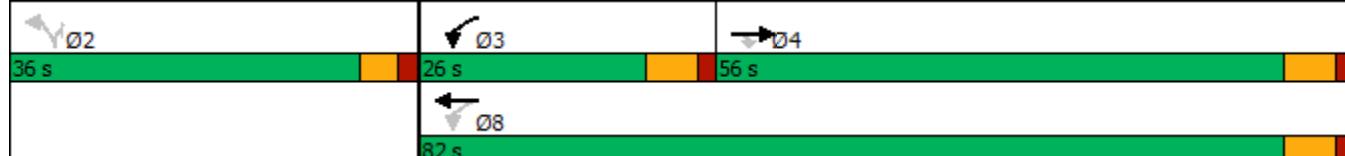
Intersection LOS: E

Intersection Capacity Utilization 69.0%

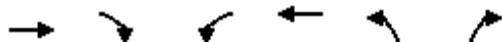
ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | → | ↓ | ↖ | ← | ↗ | ↑ |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 1002 | 181 | 66 | 475 | 56 | 109 |
| Future Volume (vph) | 1002 | 181 | 66 | 475 | 56 | 109 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | 70.0 | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 1845 | 1599 | 1752 | 1863 | 1805 | 1615 |
| Flt Permitted | | | 0.054 | | 0.950 | |
| Satd. Flow (perm) | 1845 | 1599 | 100 | 1863 | 1805 | 1615 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 171 | | | 118 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 3% | 1% | 3% | 2% | 0% | 0% |
| Adj. Flow (vph) | 1089 | 197 | 72 | 516 | 61 | 118 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 1089 | 197 | 72 | 516 | 61 | 118 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 26.2 | 26.2 |
| Total Split (s) | 80.0 | 80.0 | 11.2 | 91.2 | 26.8 | 26.8 |
| Total Split (%) | 67.8% | 67.8% | 9.5% | 77.3% | 22.7% | 22.7% |
| Maximum Green (s) | 73.8 | 73.8 | 5.0 | 85.0 | 21.6 | 21.6 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 67.8 | 67.8 | 76.2 | 76.2 | 22.1 | 22.1 |
| Actuated g/C Ratio | 0.62 | 0.62 | 0.69 | 0.69 | 0.20 | 0.20 |
| v/c Ratio | 0.96 | 0.19 | 0.49 | 0.40 | 0.17 | 0.28 |
| Control Delay | 39.3 | 2.4 | 21.1 | 7.8 | 42.2 | 9.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 39.3 | 2.4 | 21.1 | 7.8 | 42.2 | 9.4 |
| LOS | D | A | C | A | D | A |
| Approach Delay | 33.7 | | | 9.4 | 20.6 | |
| Approach LOS | C | | | A | C | |

Intersection Summary

Area Type: Other

Cycle Length: 118

Actuated Cycle Length: 110

Natural Cycle: 100

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.96

Intersection Signal Delay: 25.6

Intersection LOS: C

Intersection Capacity Utilization 69.0%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 9 | 402 | 116 | 34 | 338 | 14 | 103 | 13 | 73 | 20 | 11 | 17 |
| Future Volume (vph) | 9 | 402 | 116 | 34 | 338 | 14 | 103 | 13 | 73 | 20 | 11 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.995 | | | 0.873 | | | 0.910 | |
| Flt Protected | | 0.999 | | | 0.996 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1898 | 1568 | 0 | 1878 | 0 | 1752 | 1659 | 0 | 1805 | 1729 | 0 |
| Flt Permitted | | 0.988 | | | 0.928 | | 0.738 | | | 0.697 | | |
| Satd. Flow (perm) | 0 | 1877 | 1568 | 0 | 1750 | 0 | 1361 | 1659 | 0 | 1324 | 1729 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 127 | | | 5 | | | 79 | | | 18 | |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 549.0 | | | 622.7 | | | 441.7 | | | 187.4 | |
| Travel Time (s) | | 39.5 | | | 44.8 | | | 31.8 | | | 13.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 3% | 0% | 0% | 7% | 3% | 0% | 0% | 0% | 0% | 0% |
| Adj. Flow (vph) | 10 | 437 | 126 | 37 | 367 | 15 | 112 | 14 | 79 | 22 | 12 | 18 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 447 | 126 | 0 | 419 | 0 | 112 | 93 | 0 | 22 | 30 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 27.0 | 27.0 | 27.0 | 10.0 | 37.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (%) | 45.0% | 45.0% | 45.0% | 16.7% | 61.7% | | 38.3% | 38.3% | | 38.3% | 38.3% | |
| Maximum Green (s) | 22.0 | 22.0 | 22.0 | 5.0 | 32.0 | | 18.0 | 18.0 | | 18.0 | 18.0 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 22.0 | 22.0 | | 32.0 | | 18.0 | 18.0 | | 18.0 | 18.0 | |
| Actuated g/C Ratio | | 0.37 | 0.37 | | 0.53 | | 0.30 | 0.30 | | 0.30 | 0.30 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|------|------|-----|------|------|-----|------|------|------|------|------|-----|
| v/c Ratio | 0.65 | 0.19 | | 0.44 | | | 0.27 | 0.17 | | 0.06 | 0.06 | |
| Control Delay | 21.2 | | 3.8 | | 10.2 | | 18.3 | 6.5 | | 15.6 | 9.9 | |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 21.2 | | 3.8 | | 10.2 | | 18.3 | 6.5 | | 15.6 | 9.9 | |
| LOS | C | | A | | B | | B | A | | B | A | |
| Approach Delay | | 17.3 | | | 10.2 | | | | 13.0 | | 12.3 | |
| Approach LOS | | B | | | B | | | | B | | B | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.65

Intersection Signal Delay: 14.0

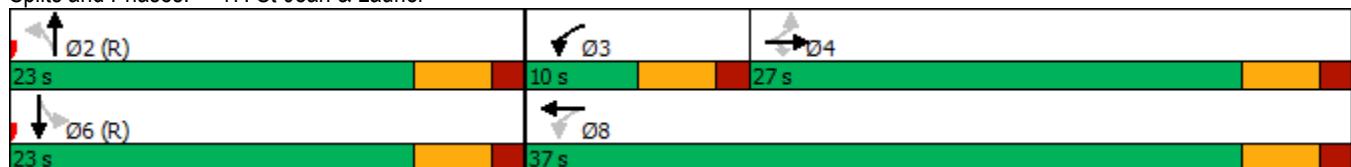
Intersection LOS: B

Intersection Capacity Utilization 67.0%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



Intersection

Intersection Delay, s/veh 10
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 176 | 28 | 33 | 172 | 9 |
| Future Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 176 | 28 | 33 | 172 | 9 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 6 | 3 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 0 |
| Mvmt Flow | 17 | 39 | 52 | 34 | 47 | 18 | 64 | 191 | 30 | 36 | 187 | 10 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | EB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 9.1 | | | 9.2 | | | 10.6 | | | 10 | | |
| HCM LOS | A | | | A | | | B | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 22% | 16% | 34% | 15% |
| Vol Thru, % | 67% | 36% | 47% | 80% |
| Vol Right, % | 11% | 48% | 19% | 4% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 263 | 100 | 91 | 214 |
| LT Vol | 59 | 16 | 31 | 33 |
| Through Vol | 176 | 36 | 43 | 172 |
| RT Vol | 28 | 48 | 17 | 9 |
| Lane Flow Rate | 286 | 109 | 99 | 233 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.375 | 0.154 | 0.143 | 0.309 |
| Departure Headway (Hd) | 4.724 | 5.098 | 5.221 | 4.775 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 758 | 697 | 680 | 747 |
| Service Time | 2.786 | 3.182 | 3.307 | 2.841 |
| HCM Lane V/C Ratio | 0.377 | 0.156 | 0.146 | 0.312 |
| HCM Control Delay | 10.6 | 9.1 | 9.2 | 10 |
| HCM Lane LOS | B | A | A | A |
| HCM 95th-tile Q | 1.7 | 0.5 | 0.5 | 1.3 |

Intersection

Intersection Delay, s/veh 8.3

Intersection LOS A

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 4 | 22 | 137 | 4 | 25 | 150 |
| Future Vol, veh/h | 4 | 22 | 137 | 4 | 25 | 150 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 8 | 1 |
| Mvmt Flow | 4 | 24 | 149 | 4 | 27 | 163 |
| Number of Lanes | 1 | 0 | 1 | 0 | 1 | 1 |
| Approach | WB | NB | SB | | | |
| Opposing Approach | | SB | NB | | | |
| Opposing Lanes | 0 | 2 | 1 | | | |
| Conflicting Approach Left | NB | | WB | | | |
| Conflicting Lanes Left | 1 | 0 | 1 | | | |
| Conflicting Approach Right | SB | WB | | | | |
| Conflicting Lanes Right | 2 | 1 | 0 | | | |
| HCM Control Delay | 7.3 | 8.2 | 8.5 | | | |
| HCM LOS | A | A | A | | | |

| Lane | NBLn1 | WBLn1 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 0% | 15% | 100% | 0% |
| Vol Thru, % | 97% | 0% | 0% | 100% |
| Vol Right, % | 3% | 85% | 0% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 141 | 26 | 25 | 150 |
| LT Vol | 0 | 4 | 25 | 0 |
| Through Vol | 137 | 0 | 0 | 150 |
| RT Vol | 4 | 22 | 0 | 0 |
| Lane Flow Rate | 153 | 28 | 27 | 163 |
| Geometry Grp | 5 | 2 | 7 | 7 |
| Degree of Util (X) | 0.178 | 0.033 | 0.04 | 0.21 |
| Departure Headway (Hd) | 4.187 | 4.203 | 5.262 | 4.642 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 846 | 857 | 679 | 771 |
| Service Time | 2.267 | 2.203 | 3.003 | 2.383 |
| HCM Lane V/C Ratio | 0.181 | 0.033 | 0.04 | 0.211 |
| HCM Control Delay | 8.2 | 7.3 | 8.2 | 8.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.6 | 0.1 | 0.1 | 0.8 |

| Intersection | | | | | | |
|--------------------------|--------|--------|-------|--------|-------|------|
| Int Delay, s/veh | 4.6 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | W | B | N | B | S | T |
| Traffic Vol, veh/h | 52 | 103 | 166 | 114 | 117 | 93 |
| Future Vol, veh/h | 52 | 103 | 166 | 114 | 117 | 93 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 1 | 1 |
| Mvmt Flow | 57 | 112 | 180 | 124 | 127 | 101 |
| Major/Minor | Minor1 | Major1 | | Major2 | | |
| Conflicting Flow All | 597 | 242 | 0 | 0 | 304 | 0 |
| Stage 1 | 242 | - | - | - | - | - |
| Stage 2 | 355 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | - | - | 4.11 | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.209 | - |
| Pot Cap-1 Maneuver | 469 | 802 | - | - | 1263 | - |
| Stage 1 | 803 | - | - | - | - | - |
| Stage 2 | 714 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 419 | 802 | - | - | 1263 | - |
| Mov Cap-2 Maneuver | 419 | - | - | - | - | - |
| Stage 1 | 717 | - | - | - | - | - |
| Stage 2 | 714 | - | - | - | - | - |
| Approach | WB | NB | | SB | | |
| HCM Control Delay, s | 13.1 | 0 | | 4.6 | | |
| HCM LOS | B | | | | | |
| Minor Lane/Major Mvmt | NBT | NBR | WBLn1 | SBL | SBT | |
| Capacity (veh/h) | - | - | 614 | 1263 | - | |
| HCM Lane V/C Ratio | - | - | 0.274 | 0.101 | - | |
| HCM Control Delay (s) | - | - | 13.1 | 8.2 | 0 | |
| HCM Lane LOS | - | - | B | A | A | |
| HCM 95th %tile Q(veh) | - | - | 1.1 | 0.3 | - | |

Intersection

Intersection Delay, s/veh 9.2
Intersection LOS A

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 73 | 81 | 101 | 23 | 78 | 185 |
| Future Vol, veh/h | 73 | 81 | 101 | 23 | 78 | 185 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 1 | 2 | 2 | 4 | 3 | 2 |
| Mvmt Flow | 79 | 88 | 110 | 25 | 85 | 201 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 0 |
| Approach | EB | WB | | NB | | |
| Opposing Approach | WB | | EB | | | |
| Opposing Lanes | 1 | | 1 | | 0 | |
| Conflicting Approach Left | | | NB | | EB | |
| Conflicting Lanes Left | 0 | | 1 | | 1 | |
| Conflicting Approach Right | NB | | | WB | | |
| Conflicting Lanes Right | 1 | | 0 | | 1 | |
| HCM Control Delay | 8.6 | | 9.1 | | 9.5 | |
| HCM LOS | A | | A | | A | |

| Lane | NBLn1 | EBLn1 | WBLn1 |
|------------------------|-------|-------|-------|
| Vol Left, % | 30% | 0% | 81% |
| Vol Thru, % | 0% | 47% | 19% |
| Vol Right, % | 70% | 53% | 0% |
| Sign Control | Stop | Stop | Stop |
| Traffic Vol by Lane | 263 | 154 | 124 |
| LT Vol | 78 | 0 | 101 |
| Through Vol | 0 | 73 | 23 |
| RT Vol | 185 | 81 | 0 |
| Lane Flow Rate | 286 | 167 | 135 |
| Geometry Grp | 1 | 1 | 1 |
| Degree of Util (X) | 0.341 | 0.205 | 0.185 |
| Departure Headway (Hd) | 4.291 | 4.414 | 4.932 |
| Convergence, Y/N | Yes | Yes | Yes |
| Cap | 838 | 812 | 726 |
| Service Time | 2.322 | 2.452 | 2.972 |
| HCM Lane V/C Ratio | 0.341 | 0.206 | 0.186 |
| HCM Control Delay | 9.5 | 8.6 | 9.1 |
| HCM Lane LOS | A | A | A |
| HCM 95th-tile Q | 1.5 | 0.8 | 0.7 |

Intersection

Intersection Delay, s/veh 9

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | | ↔ | | ↔ | | ↔ | | ↔ | | ↔ |
| Traffic Vol, veh/h | 123 | 55 | 76 | 9 | 24 | 17 | 25 | 50 | 14 | 22 | 43 | 99 |
| Future Vol, veh/h | 123 | 55 | 76 | 9 | 24 | 17 | 25 | 50 | 14 | 22 | 43 | 99 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Mvmt Flow | 134 | 60 | 83 | 10 | 26 | 18 | 27 | 54 | 15 | 24 | 47 | 108 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 9.3 | | | 8.5 | | | 8.7 | | | 8.8 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 28% | 100% | 0% | 18% | 13% |
| Vol Thru, % | 56% | 0% | 42% | 48% | 26% |
| Vol Right, % | 16% | 0% | 58% | 34% | 60% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 89 | 123 | 131 | 50 | 164 |
| LT Vol | 25 | 123 | 0 | 9 | 22 |
| Through Vol | 50 | 0 | 55 | 24 | 43 |
| RT Vol | 14 | 0 | 76 | 17 | 99 |
| Lane Flow Rate | 97 | 134 | 142 | 54 | 178 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.131 | 0.211 | 0.189 | 0.075 | 0.222 |
| Departure Headway (Hd) | 4.877 | 5.69 | 4.778 | 4.999 | 4.488 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 733 | 630 | 748 | 713 | 799 |
| Service Time | 2.921 | 3.439 | 2.527 | 3.059 | 2.525 |
| HCM Lane V/C Ratio | 0.132 | 0.213 | 0.19 | 0.076 | 0.223 |
| HCM Control Delay | 8.7 | 10 | 8.6 | 8.5 | 8.8 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.8 | 0.7 | 0.2 | 0.8 |

Intersection

Intersection Delay, s/veh 8

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | 3 | 5 | 13 | 105 | 0 | 49 | 11 | 18 | 68 | 21 |
| Traffic Vol, veh/h | 17 | 15 | 3 | 5 | 13 | 105 | 0 | 49 | 11 | 18 | 68 | 21 |
| Future Vol, veh/h | 17 | 15 | 3 | 5 | 13 | 105 | 0 | 49 | 11 | 18 | 68 | 21 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 19 |
| Mvmt Flow | 18 | 16 | 3 | 5 | 14 | 114 | 0 | 53 | 12 | 20 | 74 | 23 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 2 | | | 2 | | | 2 | | | 2 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 2 | | | 2 | | | 2 | | | 2 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 2 | | | 2 | | | 2 | | | 2 | | |
| HCM Control Delay | 8.1 | | | 7.9 | | | 7.8 | | | 8.3 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 21% | 0% |
| Vol Thru, % | 100% | 60% | 0% | 83% | 0% | 11% | 79% | 0% |
| Vol Right, % | 0% | 40% | 0% | 17% | 0% | 89% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 33 | 27 | 17 | 18 | 5 | 118 | 86 | 21 |
| LT Vol | 0 | 0 | 17 | 0 | 5 | 0 | 18 | 0 |
| Through Vol | 33 | 16 | 0 | 15 | 0 | 13 | 68 | 0 |
| RT Vol | 0 | 11 | 0 | 3 | 0 | 105 | 0 | 21 |
| Lane Flow Rate | 36 | 30 | 18 | 20 | 5 | 128 | 93 | 23 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.05 | 0.039 | 0.029 | 0.027 | 0.008 | 0.155 | 0.132 | 0.027 |
| Departure Headway (Hd) | 5.042 | 4.725 | 5.562 | 4.943 | 5.488 | 4.362 | 5.065 | 4.275 |
| Convergence, Y/N | Yes |
| Cap | 712 | 760 | 645 | 726 | 654 | 825 | 709 | 839 |
| Service Time | 2.759 | 2.442 | 3.281 | 2.662 | 3.204 | 2.078 | 2.781 | 1.991 |
| HCM Lane V/C Ratio | 0.051 | 0.039 | 0.028 | 0.028 | 0.008 | 0.155 | 0.131 | 0.027 |
| HCM Control Delay | 8 | 7.6 | 8.4 | 7.8 | 8.2 | 7.9 | 8.6 | 7.1 |
| HCM Lane LOS | A | A | A | A | A | A | A | A |
| HCM 95th-tile Q | 0.2 | 0.1 | 0.1 | 0.1 | 0 | 0.5 | 0.5 | 0.1 |

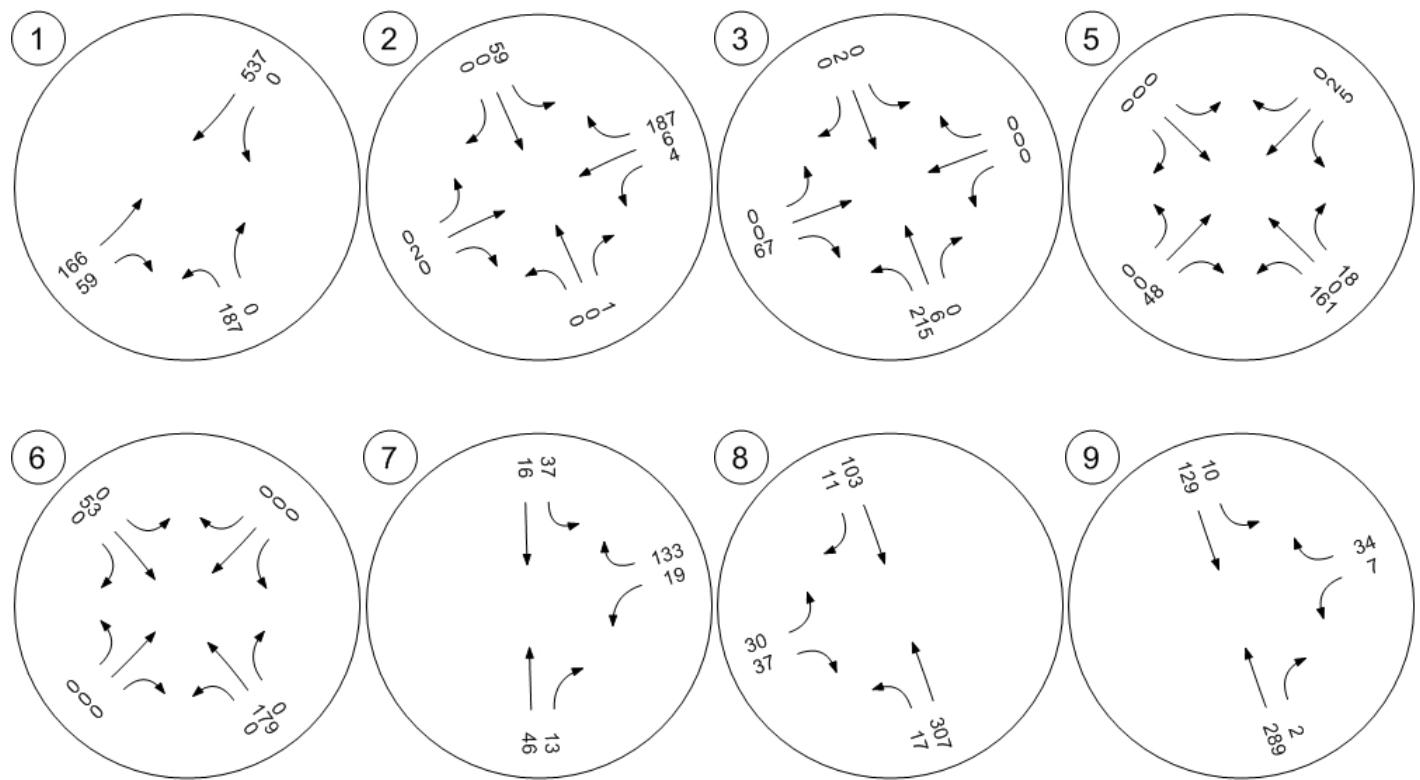
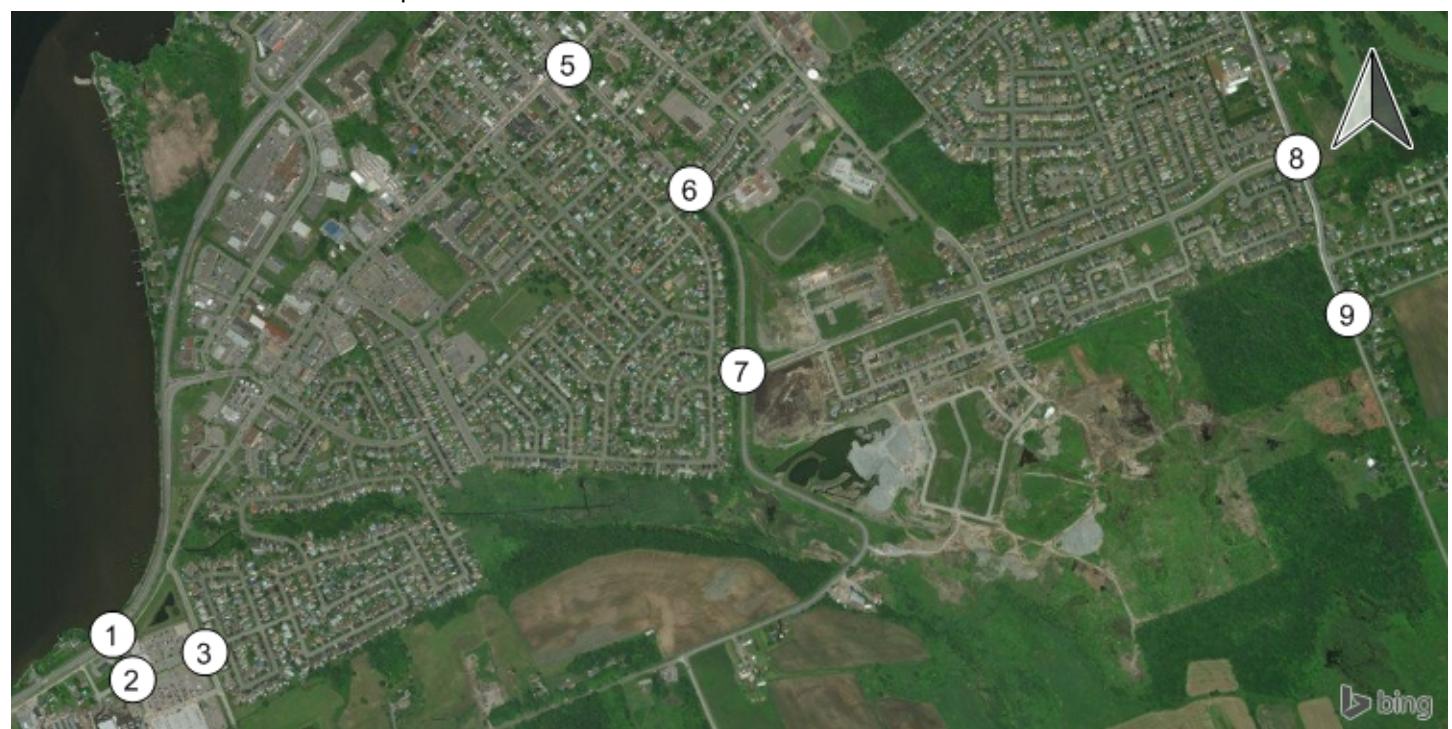
| Intersection | | | | | | |
|--------------------------|--------|--------|-------|--------|------|------|
| Int Delay, s/veh | 4.8 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | W | | T | ↑ | ↑ | |
| Traffic Vol, veh/h | 79 | 92 | 60 | 116 | 106 | 64 |
| Future Vol, veh/h | 79 | 92 | 60 | 116 | 106 | 64 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 400 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 86 | 100 | 65 | 126 | 115 | 70 |
| Major/Minor | Minor2 | Major1 | | Major2 | | |
| Conflicting Flow All | 406 | 150 | 185 | 0 | - | 0 |
| Stage 1 | 150 | - | - | - | - | - |
| Stage 2 | 256 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 605 | 902 | 1402 | - | - | - |
| Stage 1 | 883 | - | - | - | - | - |
| Stage 2 | 791 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 577 | 902 | 1402 | - | - | - |
| Mov Cap-2 Maneuver | 577 | - | - | - | - | - |
| Stage 1 | 842 | - | - | - | - | - |
| Stage 2 | 791 | - | - | - | - | - |
| Approach | EB | NB | | SB | | |
| HCM Control Delay, s | 11.8 | 2.6 | | 0 | | |
| HCM LOS | B | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR | |
| Capacity (veh/h) | 1402 | - | 716 | - | - | |
| HCM Lane V/C Ratio | 0.047 | - | 0.26 | - | - | |
| HCM Control Delay (s) | 7.7 | - | 11.8 | - | - | |
| HCM Lane LOS | A | - | B | - | - | |
| HCM 95th %tile Q(veh) | 0.1 | - | 1 | - | - | |

| Intersection | | | | | | | | | | | | | | | | | | | |
|--------------------------|------|--------|------|------|--------|------|------|--------|-------|------|------|------|--|--|--|--|--|--|--|
| Int Delay, s/veh | 6.5 | | | | | | | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | | | | | |
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | | | | | | | |
| Traffic Vol, veh/h | 66 | 122 | 22 | 40 | 45 | 63 | 25 | 13 | 70 | 62 | 13 | 53 | | | | | | | |
| Future Vol, veh/h | 66 | 122 | 22 | 40 | 45 | 63 | 25 | 13 | 70 | 62 | 13 | 53 | | | | | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | | | | | | | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | | | | | | | |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - | | | | | | | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | | | | | | | |
| Heavy Vehicles, % | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Mvmt Flow | 72 | 133 | 24 | 43 | 49 | 68 | 27 | 14 | 76 | 67 | 14 | 58 | | | | | | | |
| Major/Minor | | | | | | | | | | | | | | | | | | | |
| Major1 | | Major2 | | | Minor1 | | | Minor2 | | | | | | | | | | | |
| Conflicting Flow All | 117 | 0 | 0 | 157 | 0 | 0 | 494 | 492 | 145 | 503 | 470 | 83 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 289 | 289 | - | 169 | 169 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 205 | 203 | - | 334 | 301 | - | | | | | | | |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | | | | | | | |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | | | | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | | | | | |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 | | | | | | | |
| Pot Cap-1 Maneuver | 1484 | - | - | 1435 | - | - | 489 | 481 | 908 | 482 | 495 | 982 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 723 | 677 | - | 838 | 763 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 802 | 737 | - | 684 | 669 | - | | | | | | | |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - | | | | | | | |
| Mov Cap-1 Maneuver | 1484 | - | - | 1435 | - | - | 423 | 443 | 908 | 406 | 456 | 982 | | | | | | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 423 | 443 | - | 406 | 456 | - | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 688 | 644 | - | 797 | 740 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 718 | 715 | - | 583 | 636 | - | | | | | | | |
| Approach | | | | | | | | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | | | | | | | | |
| HCM Control Delay, s | 2.4 | | 2.1 | | | 11.7 | | | 13.9 | | | | | | | | | | |
| HCM LOS | B | | | | | | B | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | | | | | | | | | | | | | | | | | | |
| Capacity (veh/h) | 652 | 1484 | - | - | 1435 | - | - | - | 544 | | | | | | | | | | |
| HCM Lane V/C Ratio | 0.18 | 0.048 | - | - | 0.03 | - | - | - | 0.256 | | | | | | | | | | |
| HCM Control Delay (s) | 11.7 | 7.5 | - | - | 7.6 | - | - | - | 13.9 | | | | | | | | | | |
| HCM Lane LOS | B | A | - | - | A | - | - | - | B | | | | | | | | | | |
| HCM 95th %tile Q(veh) | 0.7 | 0.2 | - | - | 0.1 | - | - | - | 1 | | | | | | | | | | |

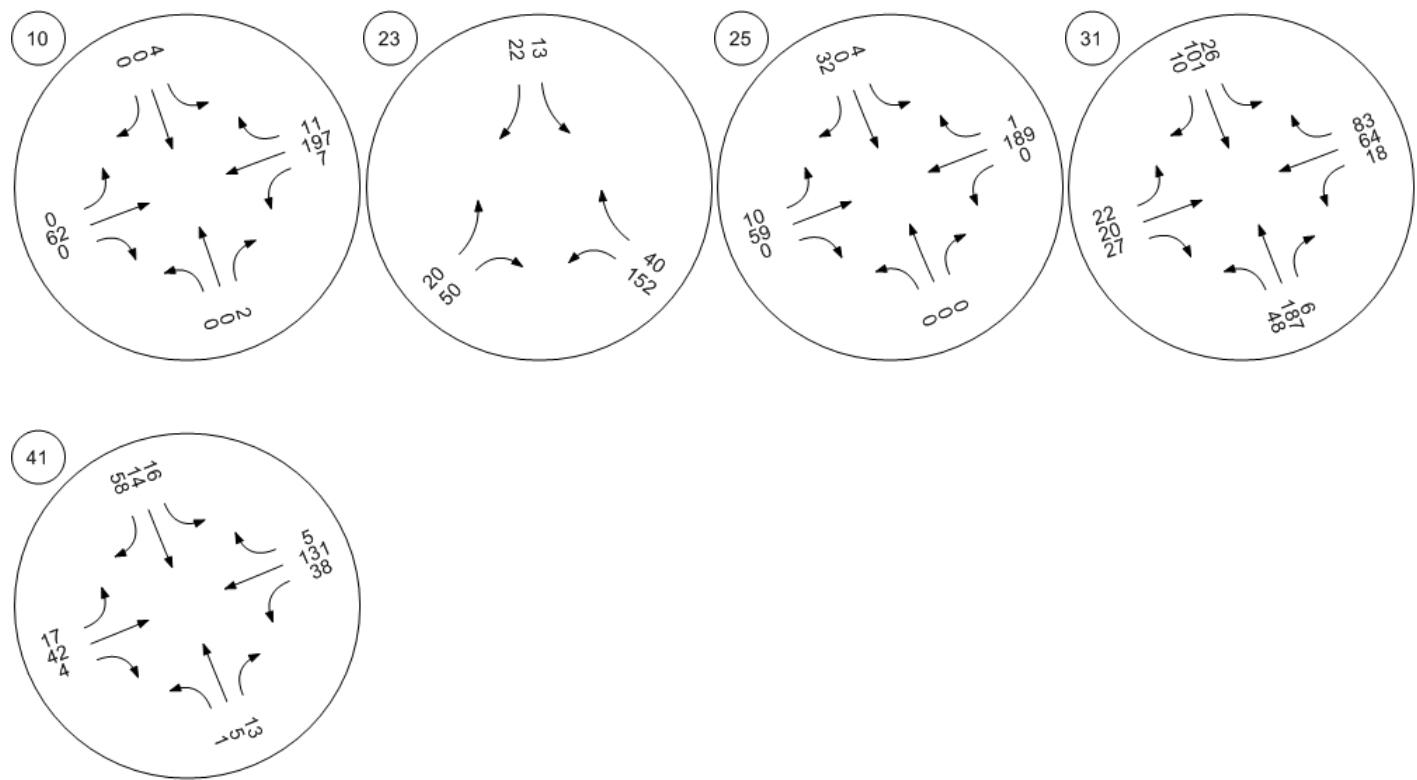
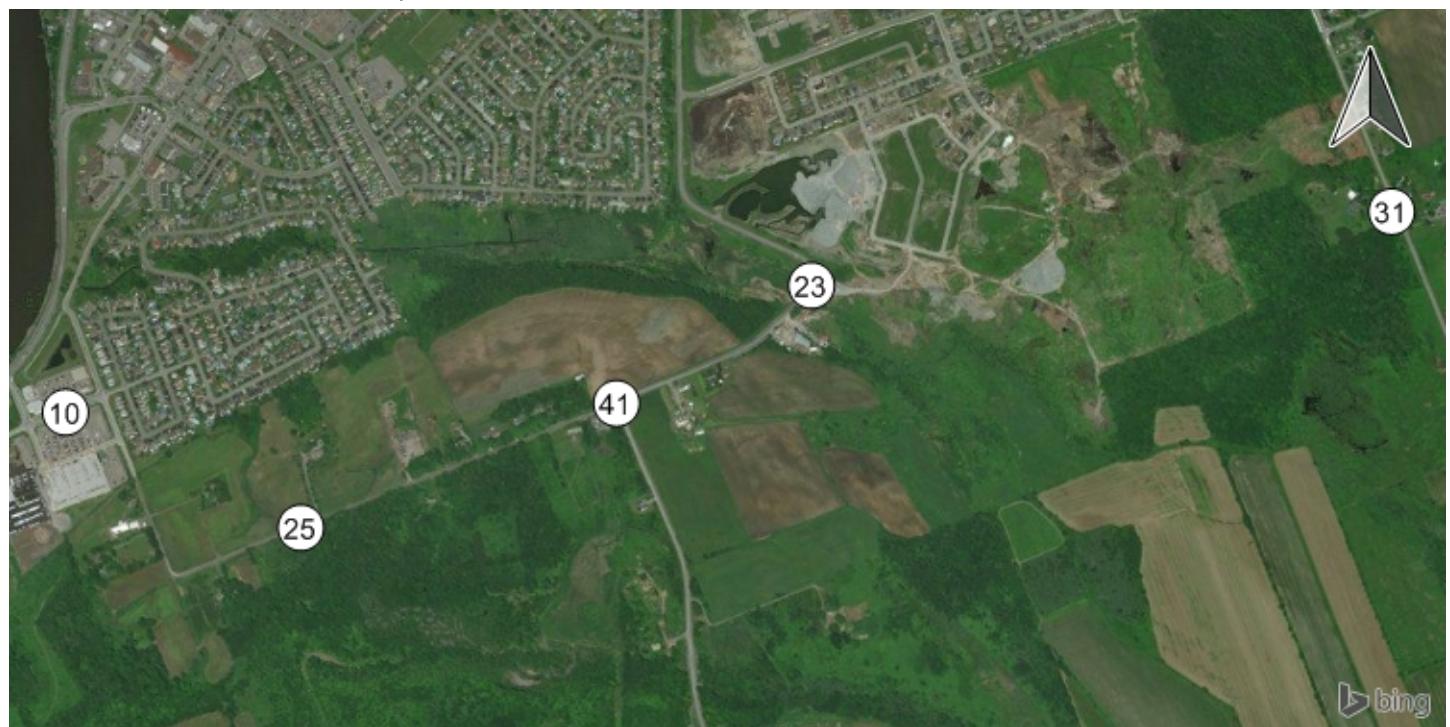
Appendix B

Site and Forecast Traffic Volumes

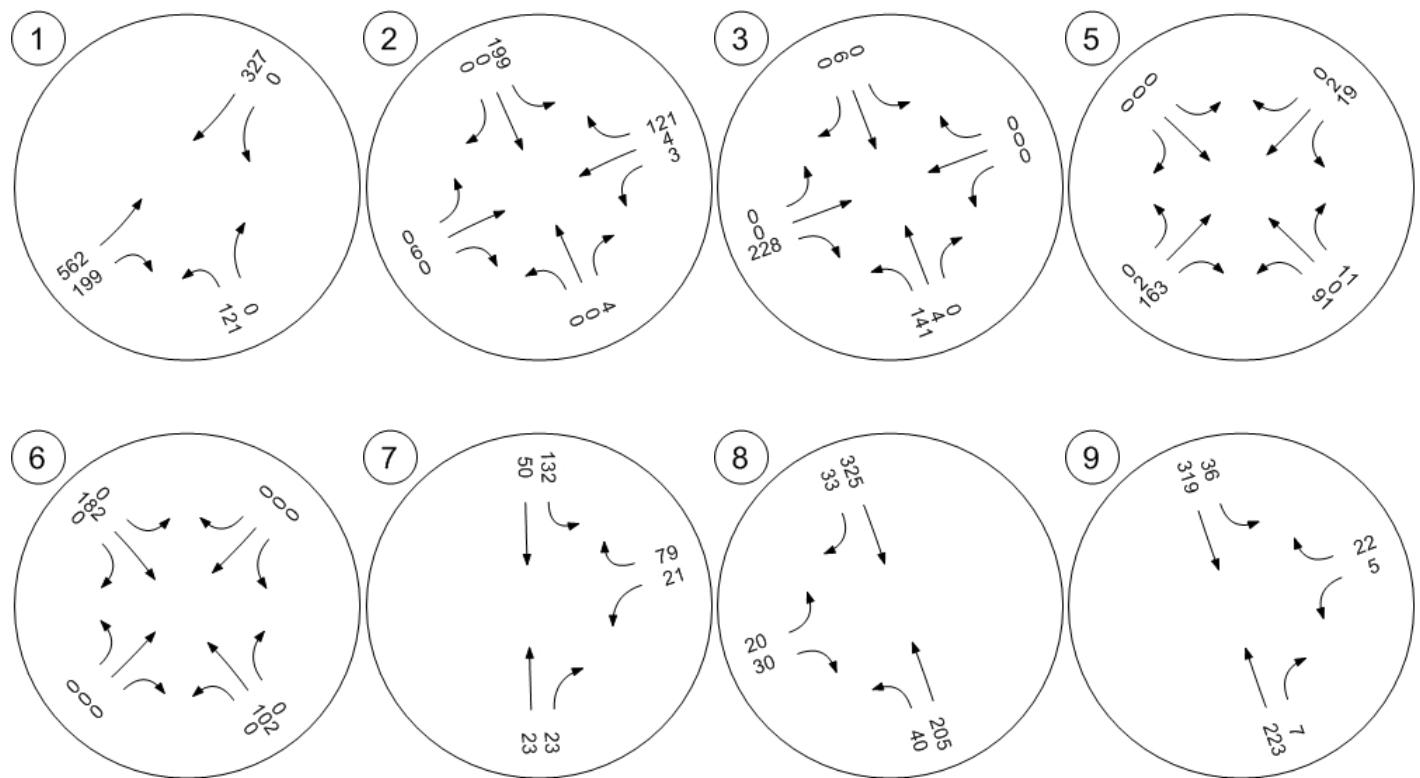
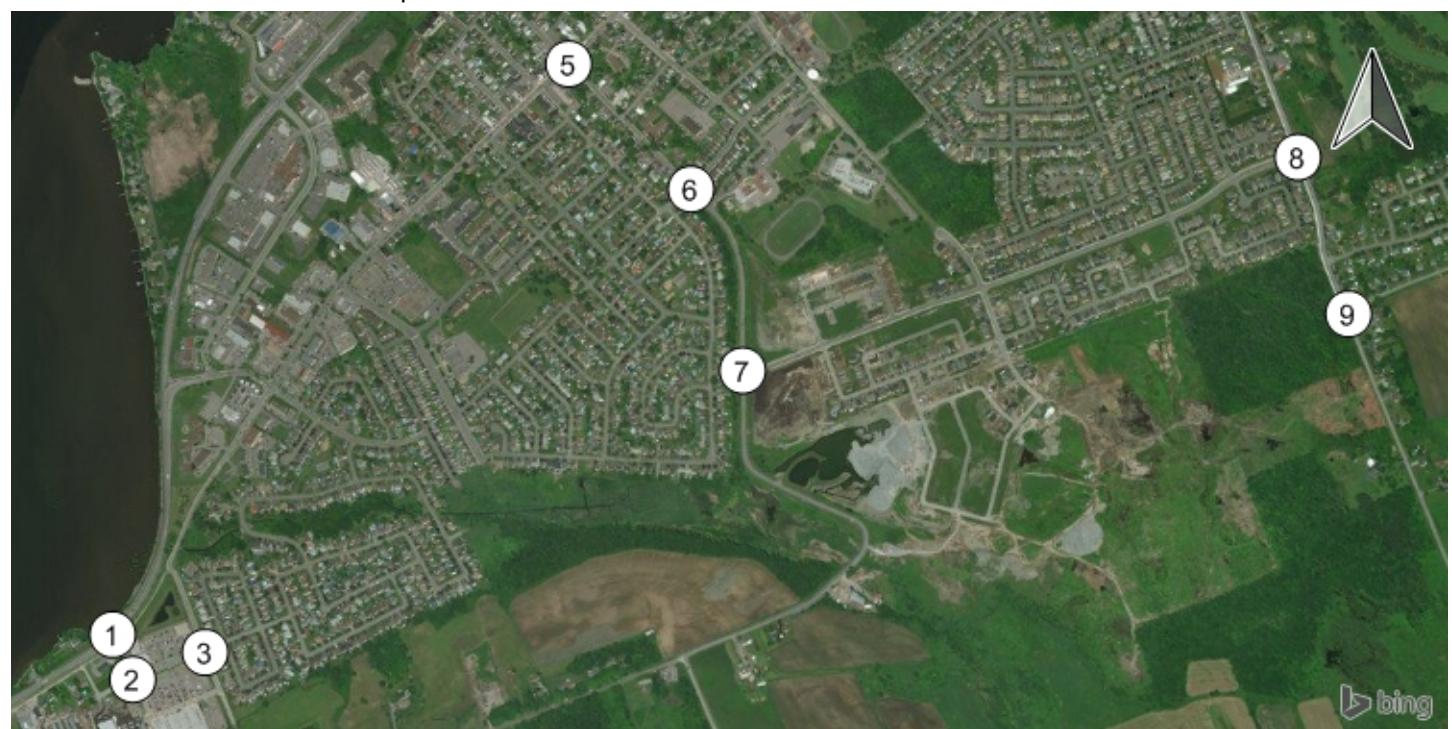
Traffic Volume - Net New Site Trips



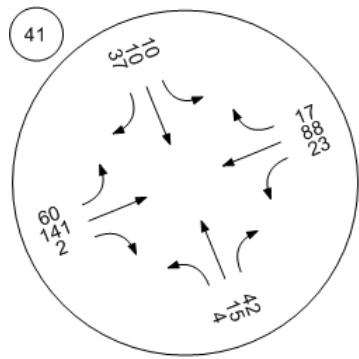
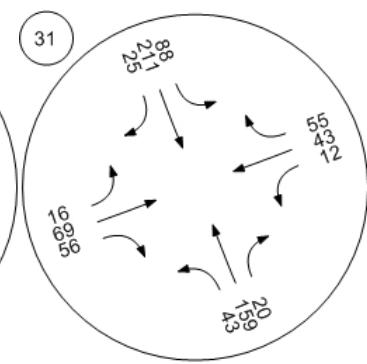
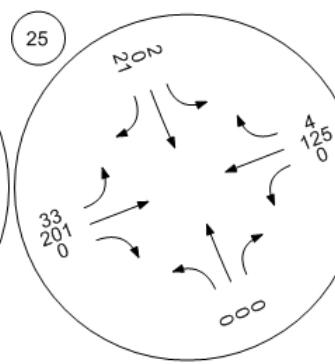
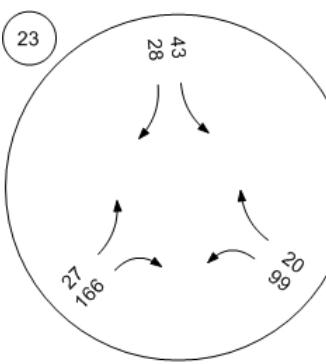
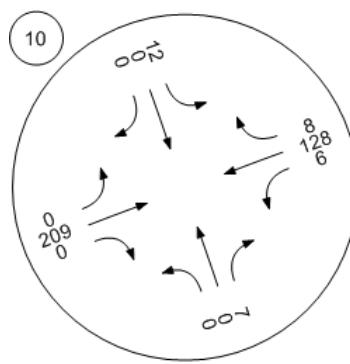
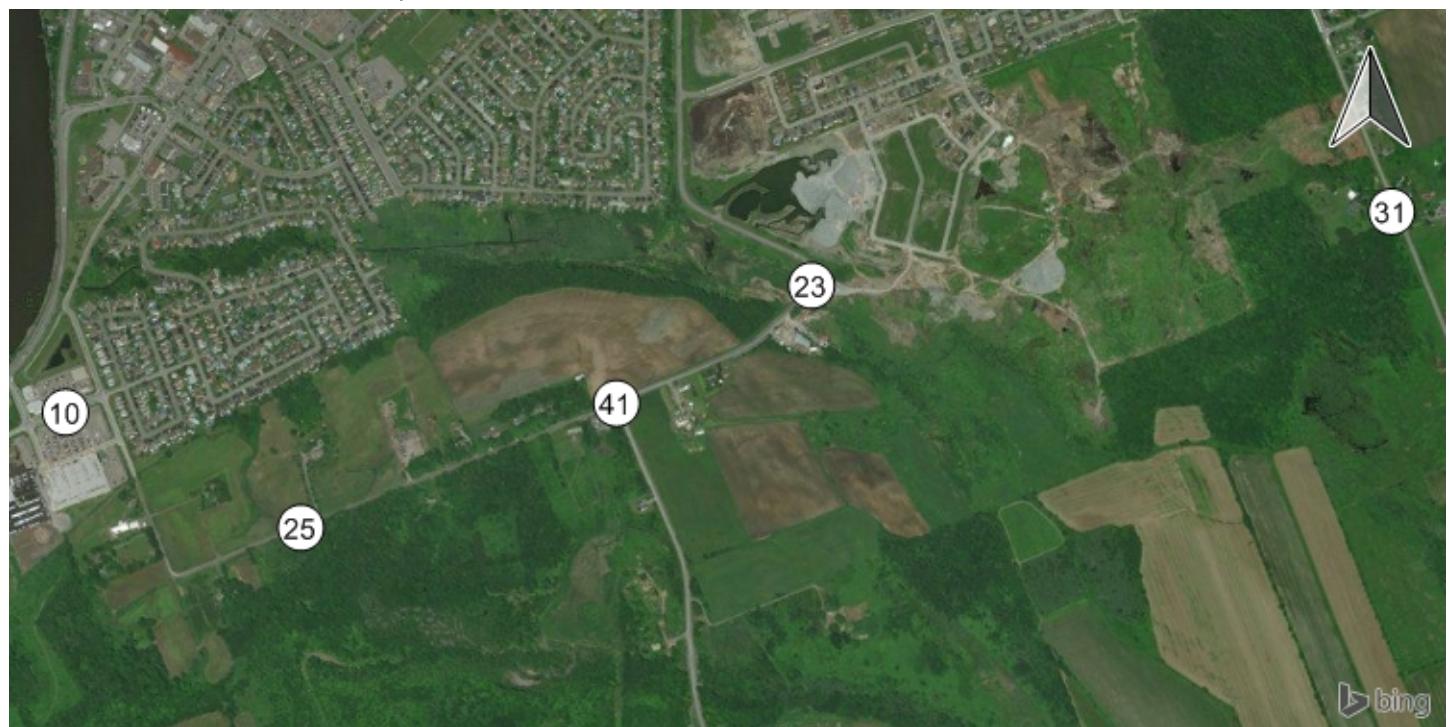
Traffic Volume - Net New Site Trips



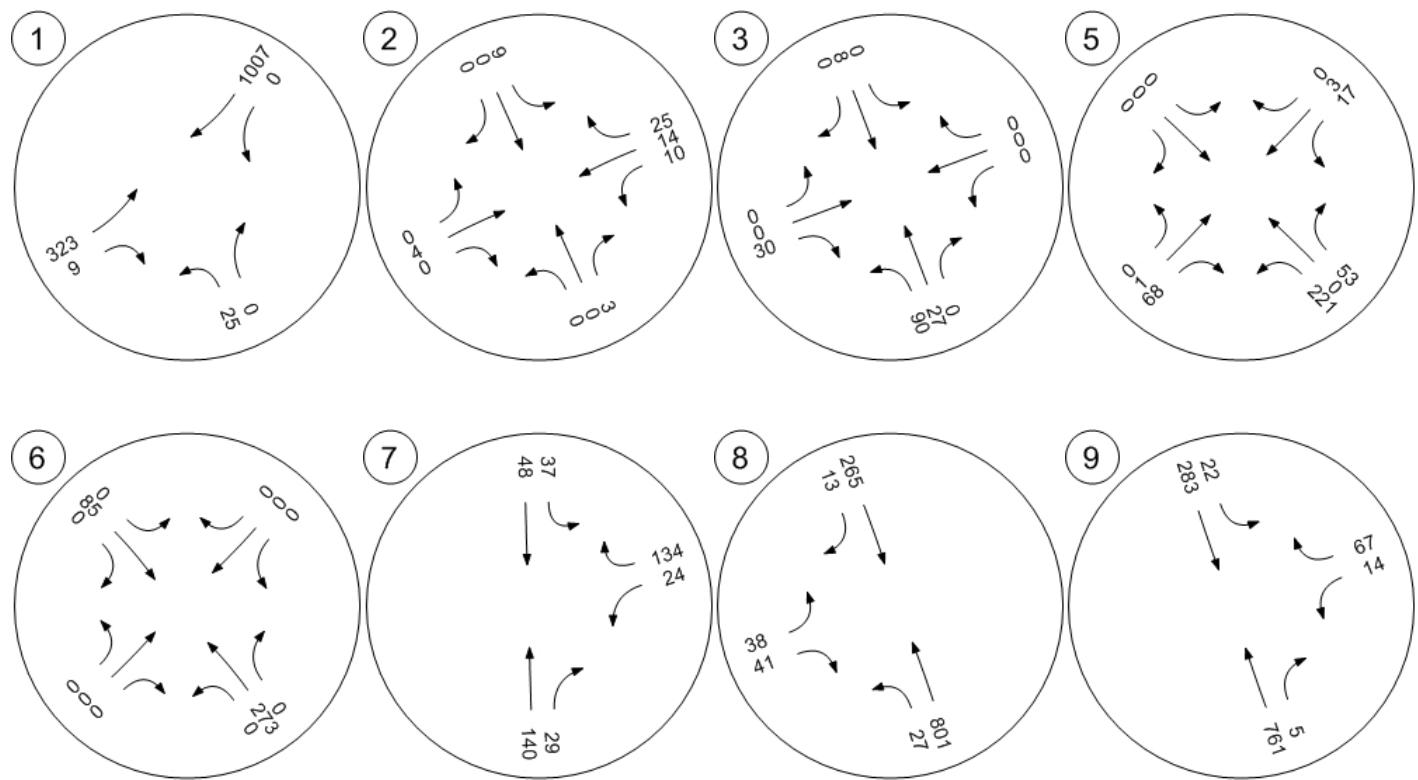
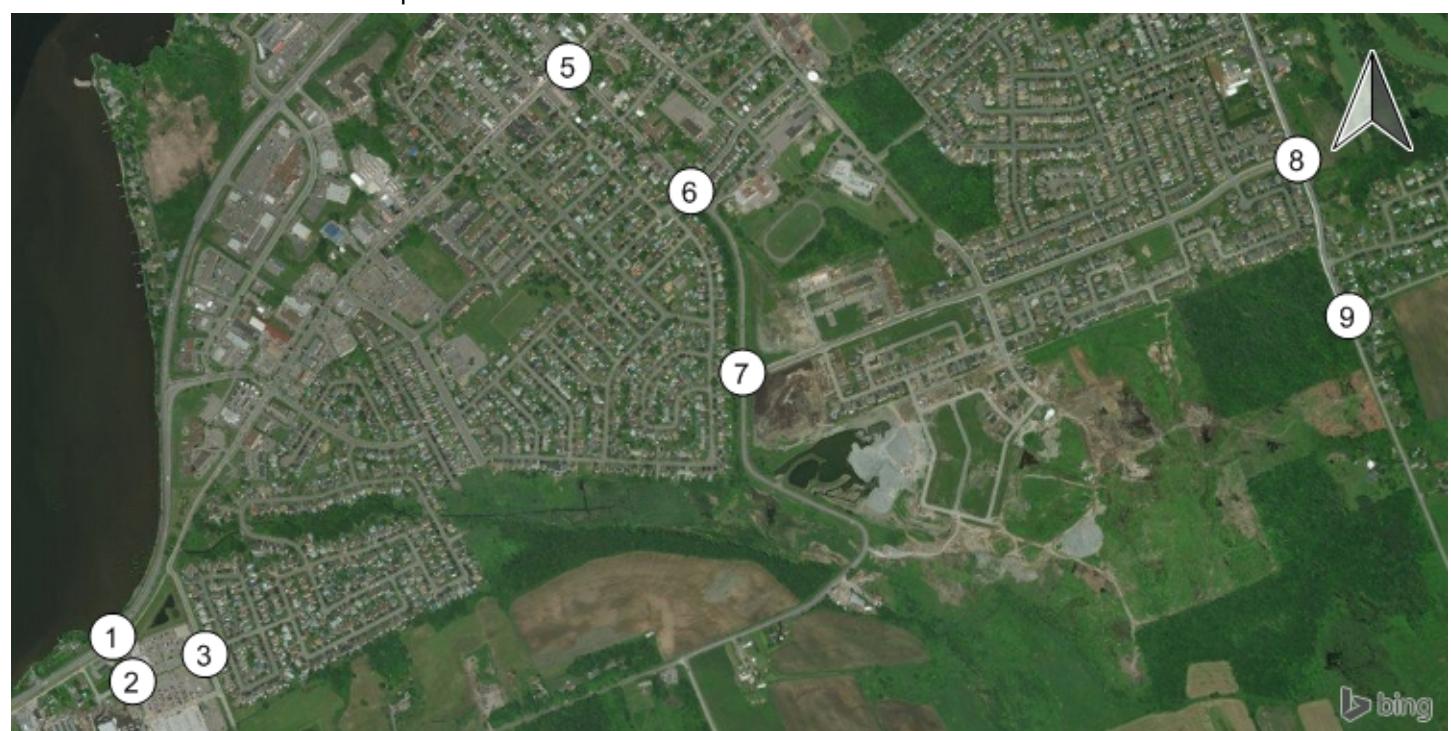
Traffic Volume - Net New Site Trips



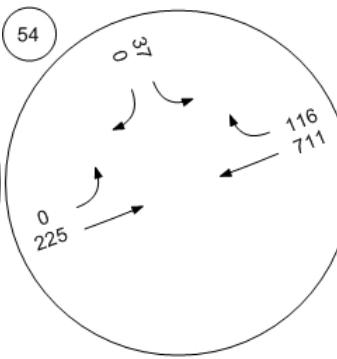
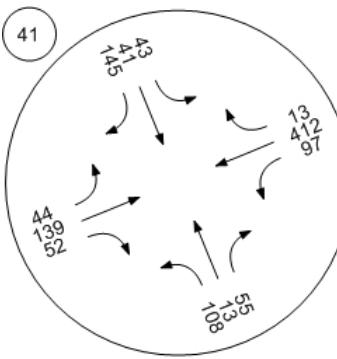
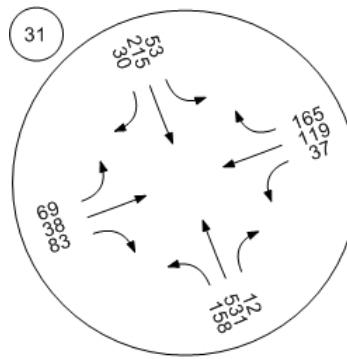
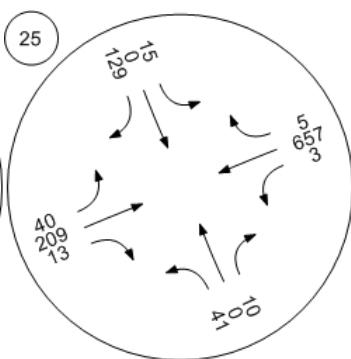
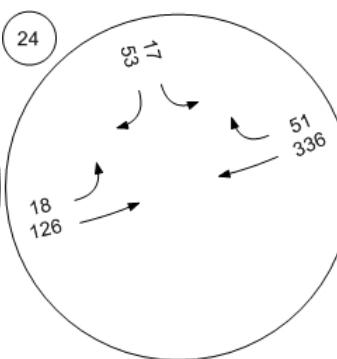
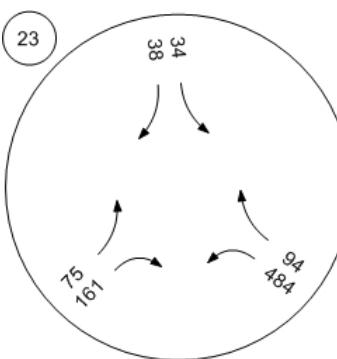
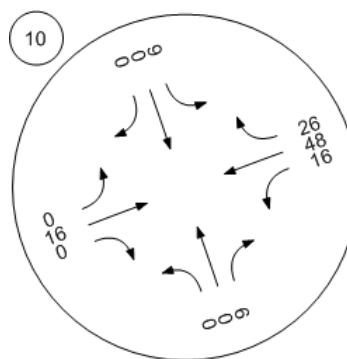
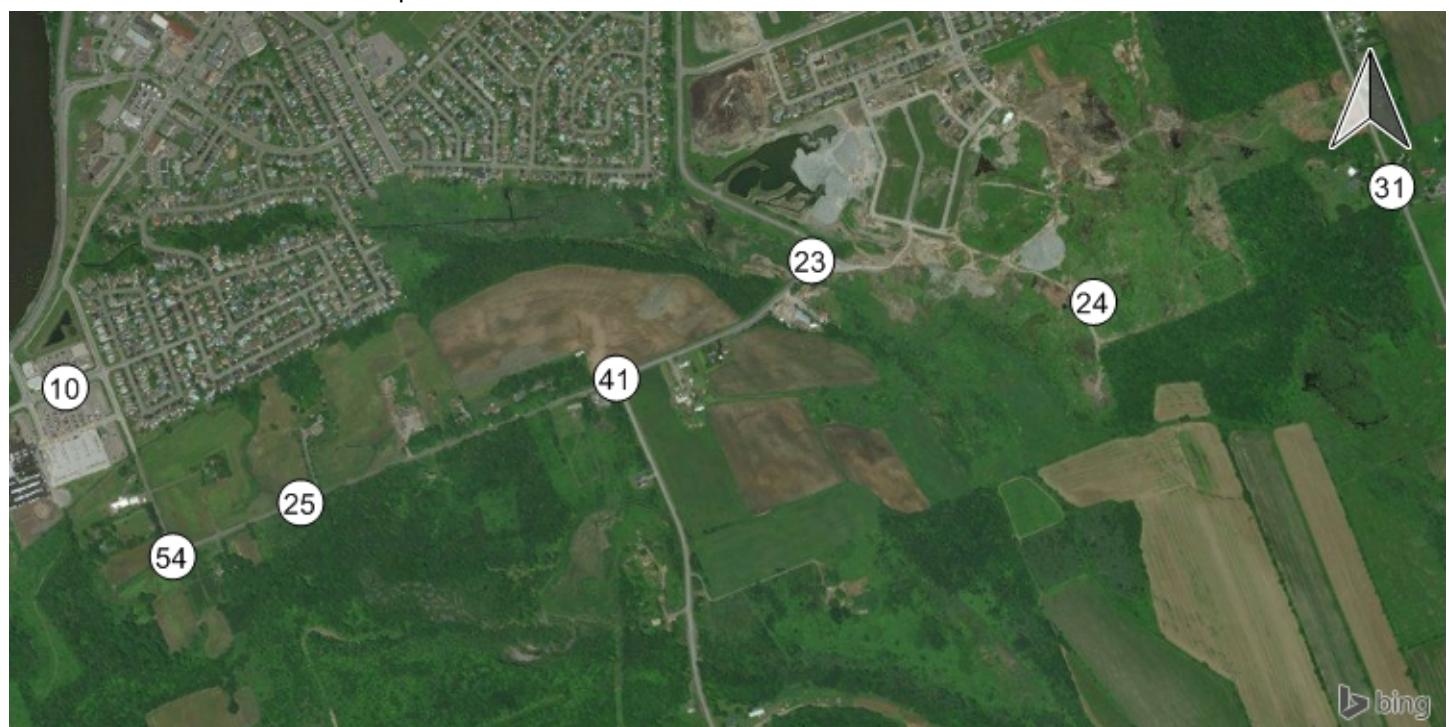
Traffic Volume - Net New Site Trips



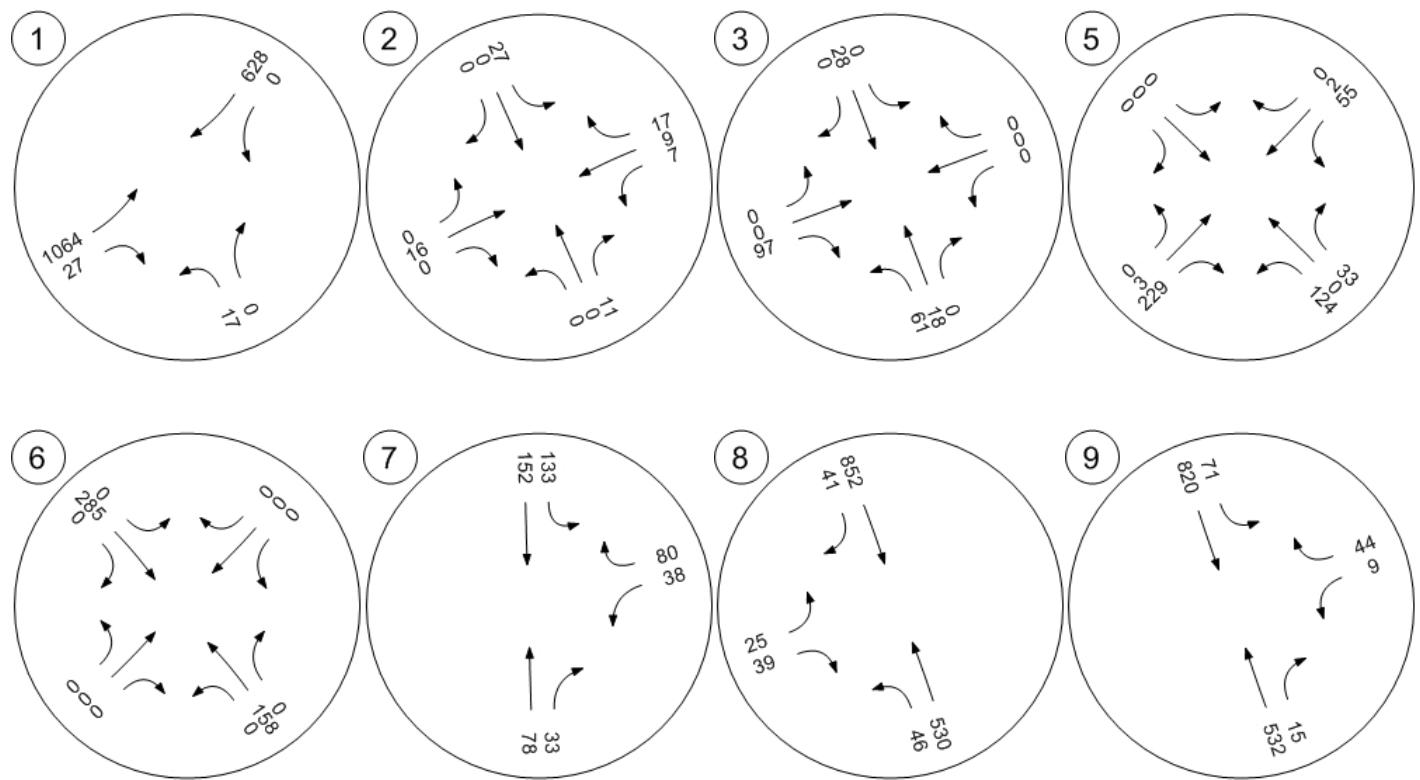
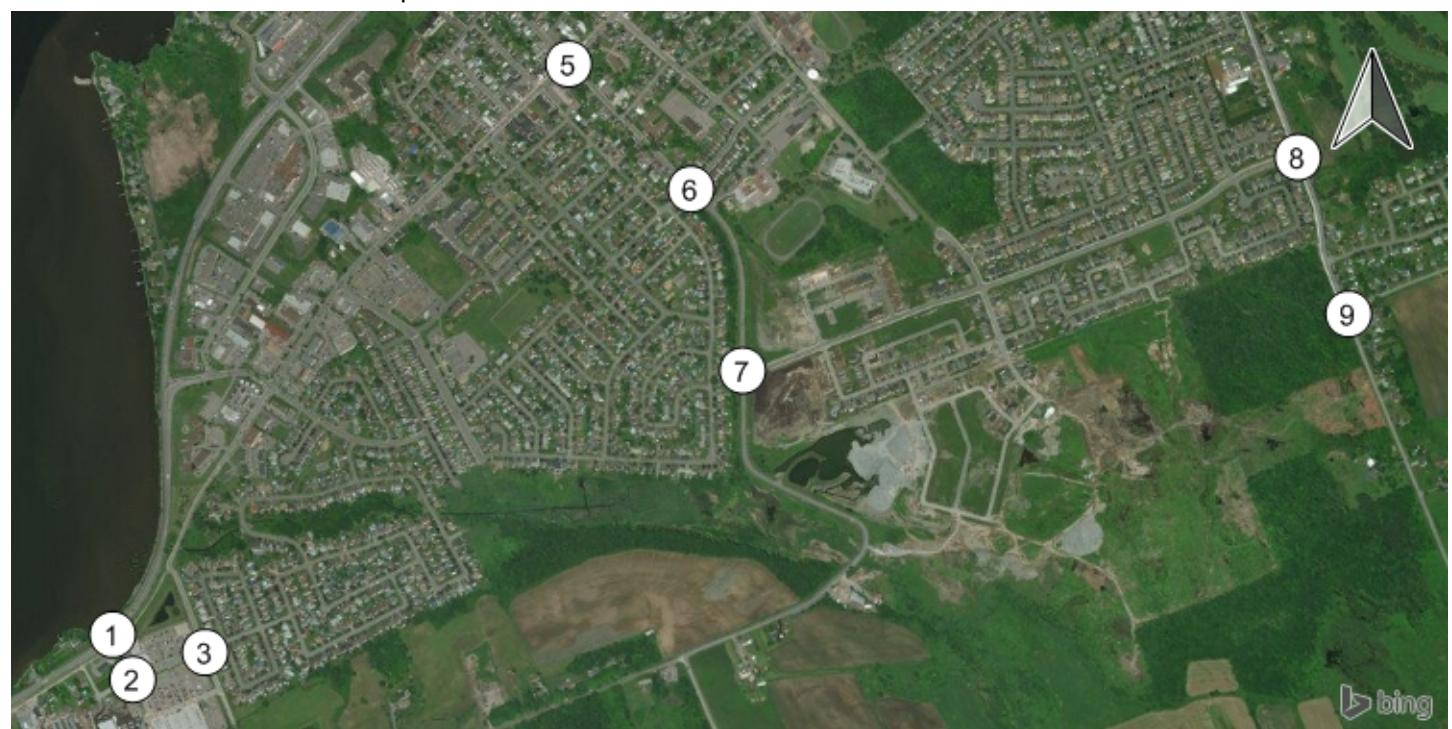
Traffic Volume - Net New Site Trips



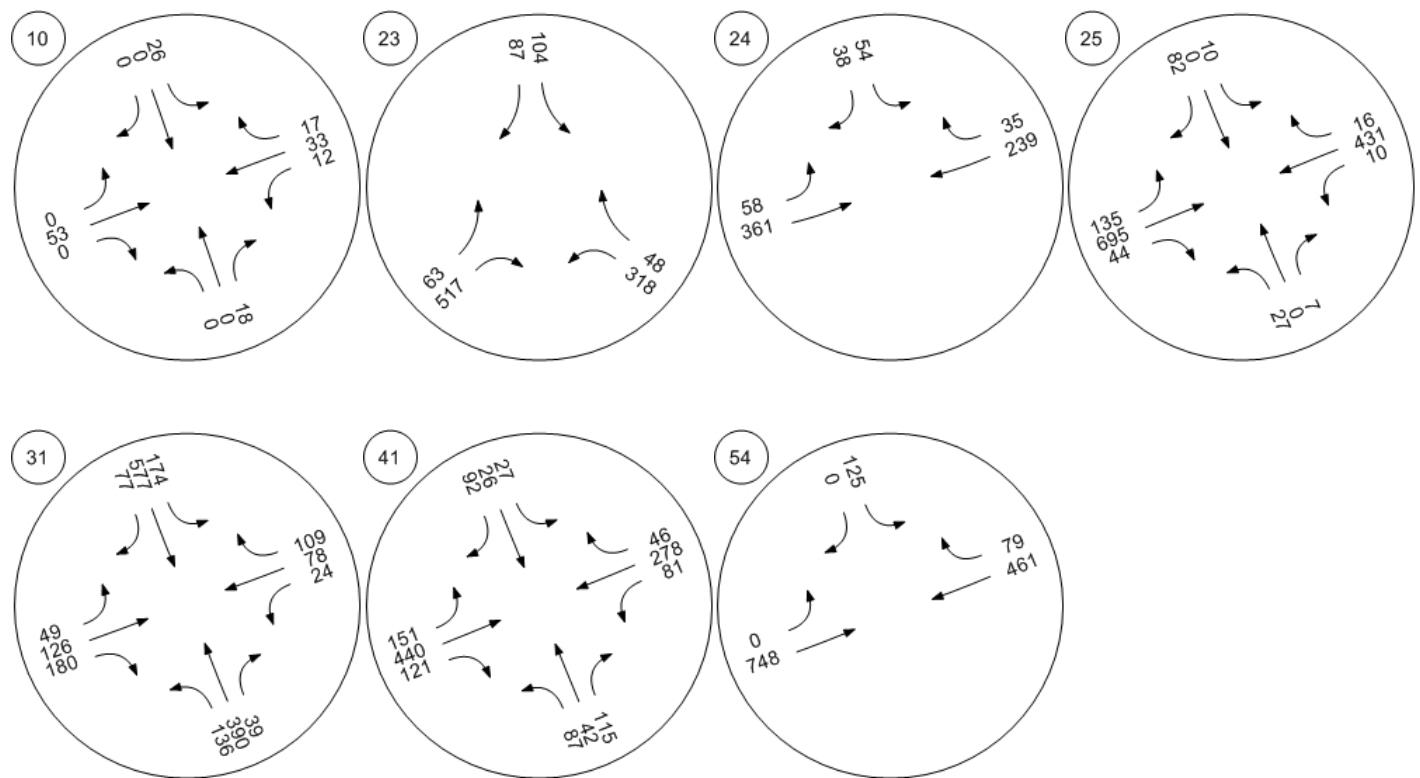
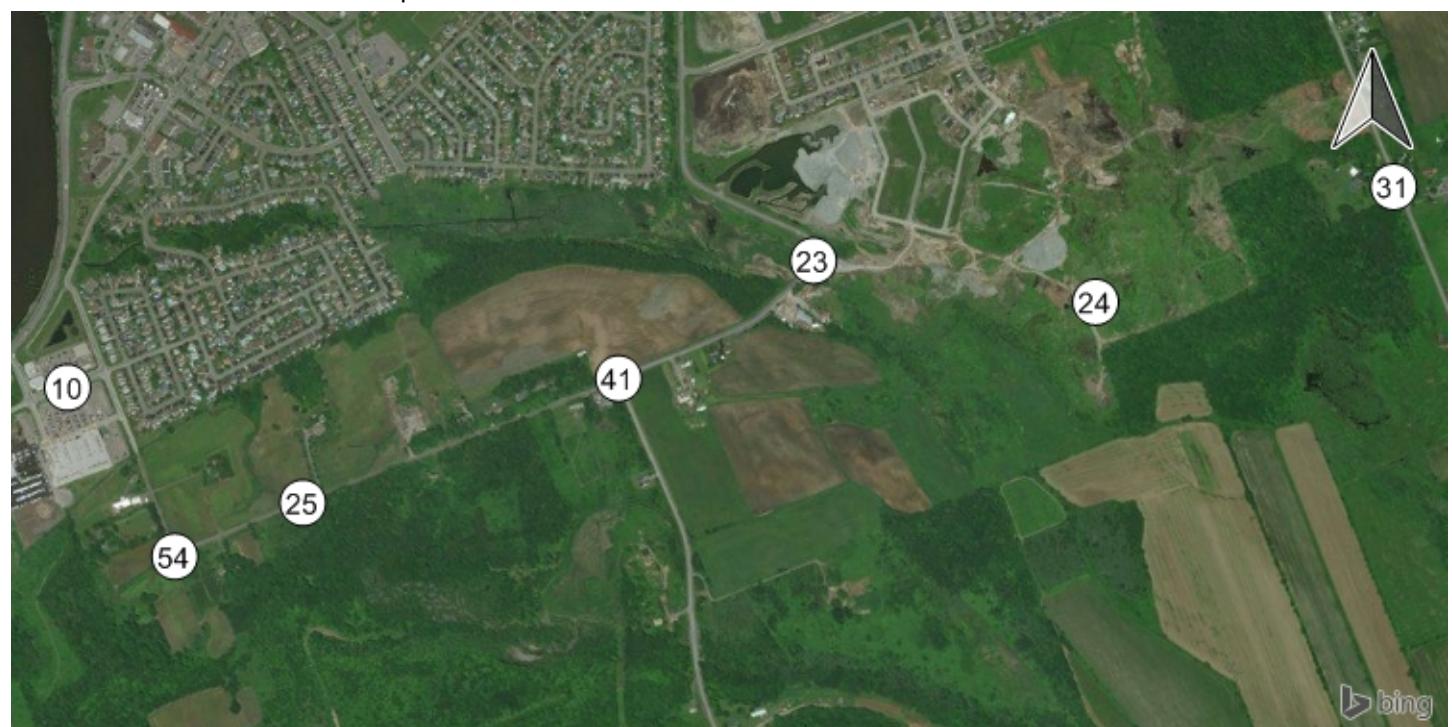
Traffic Volume - Net New Site Trips



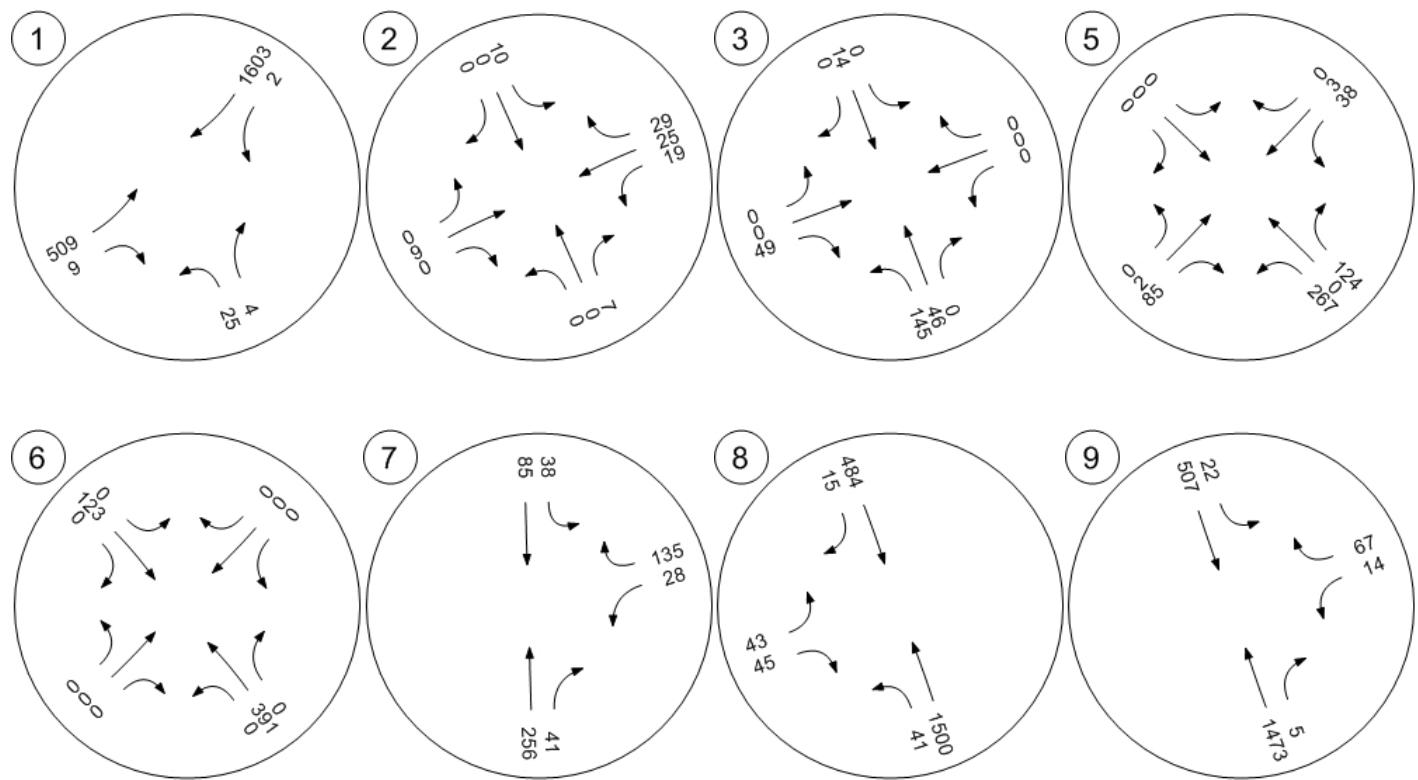
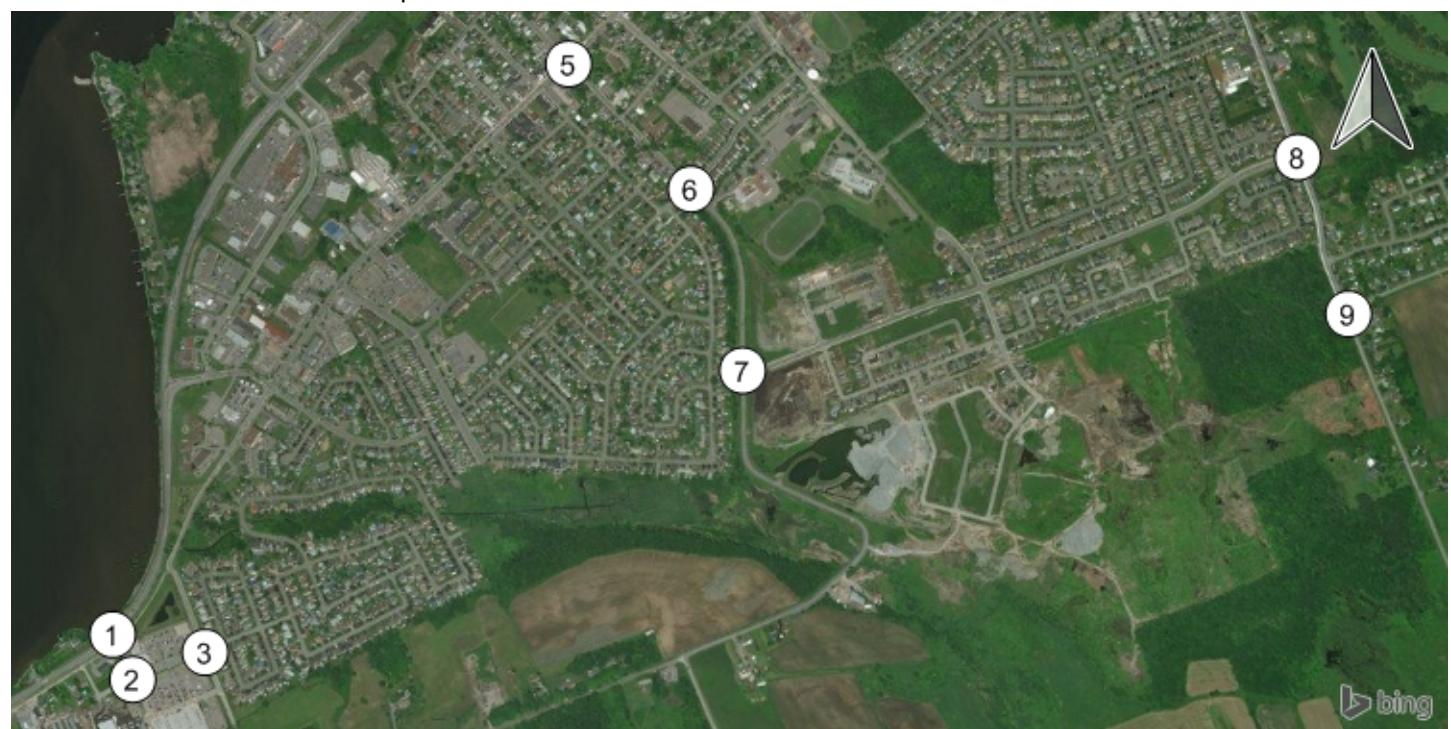
Traffic Volume - Net New Site Trips



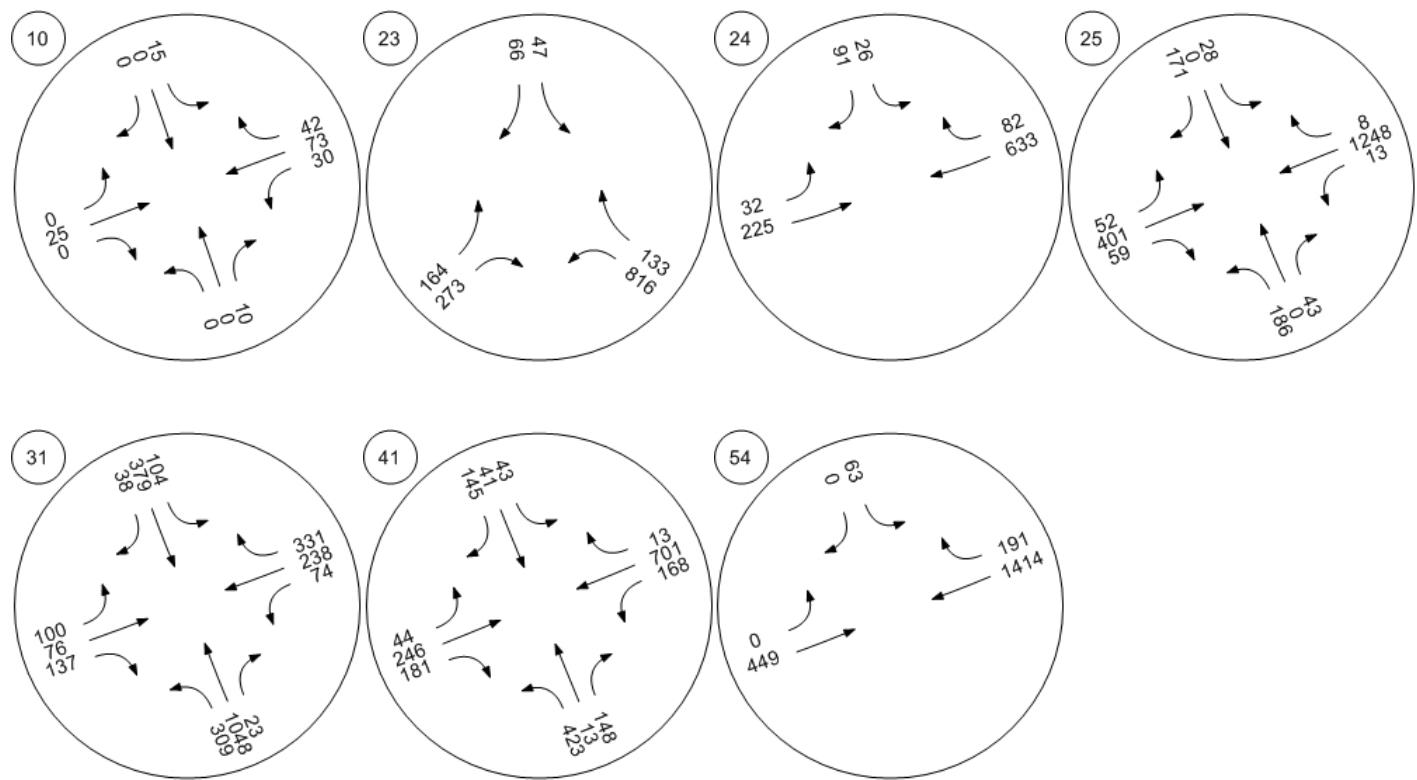
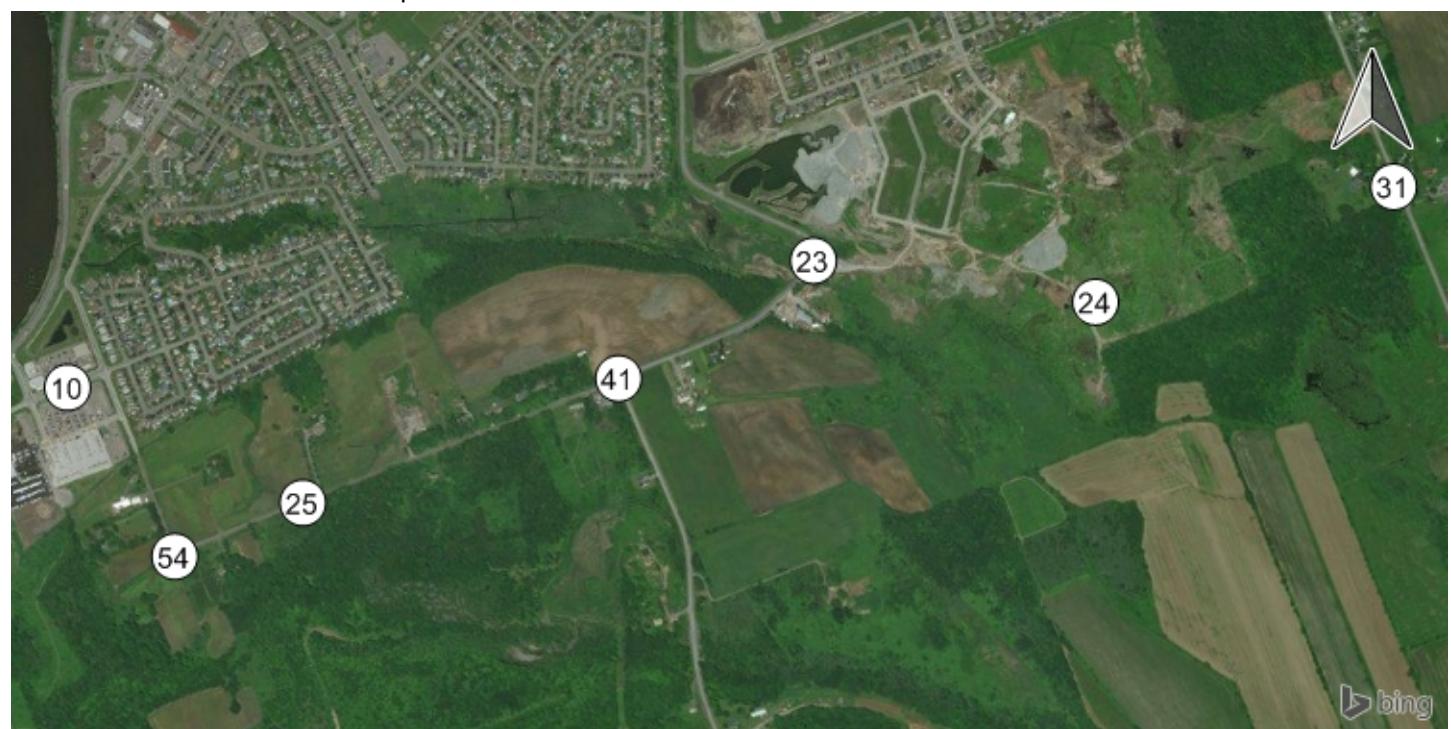
Traffic Volume - Net New Site Trips



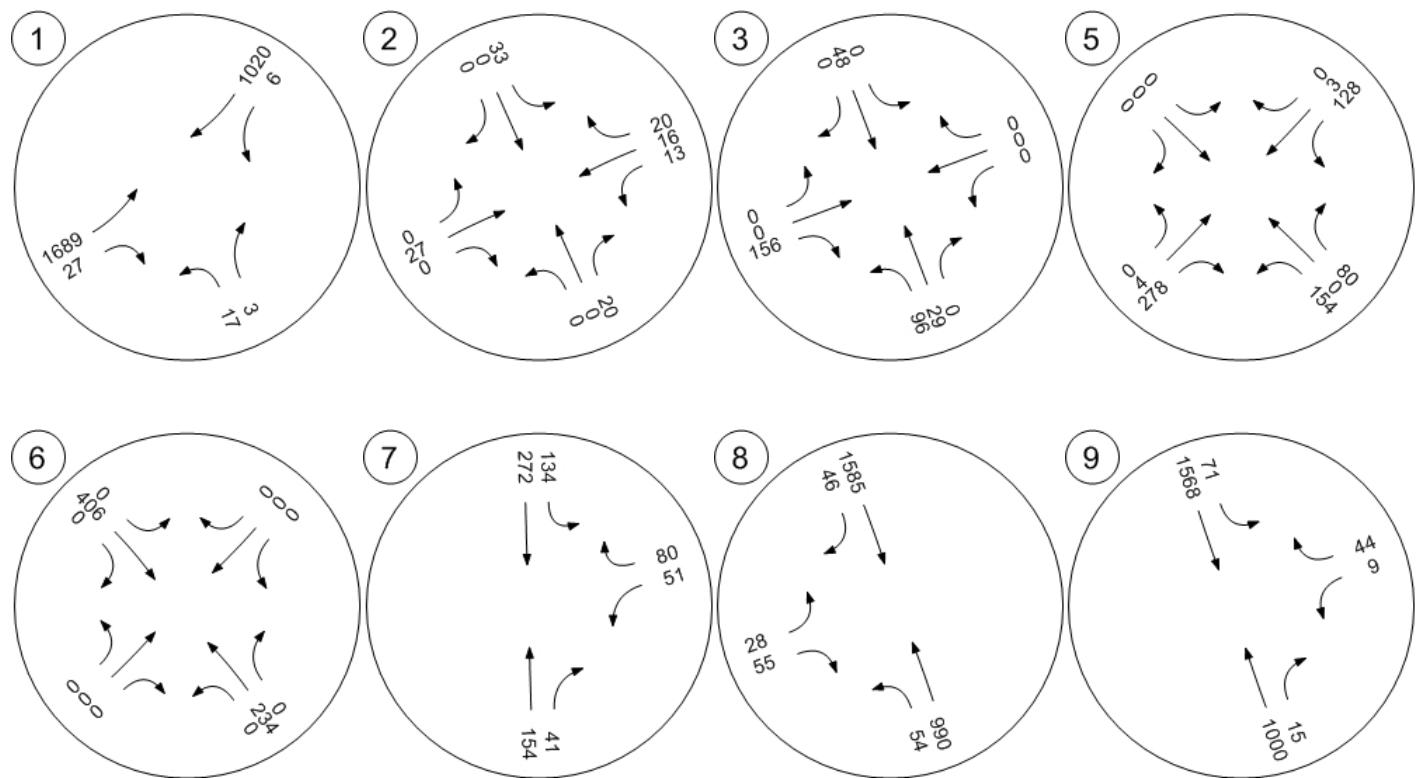
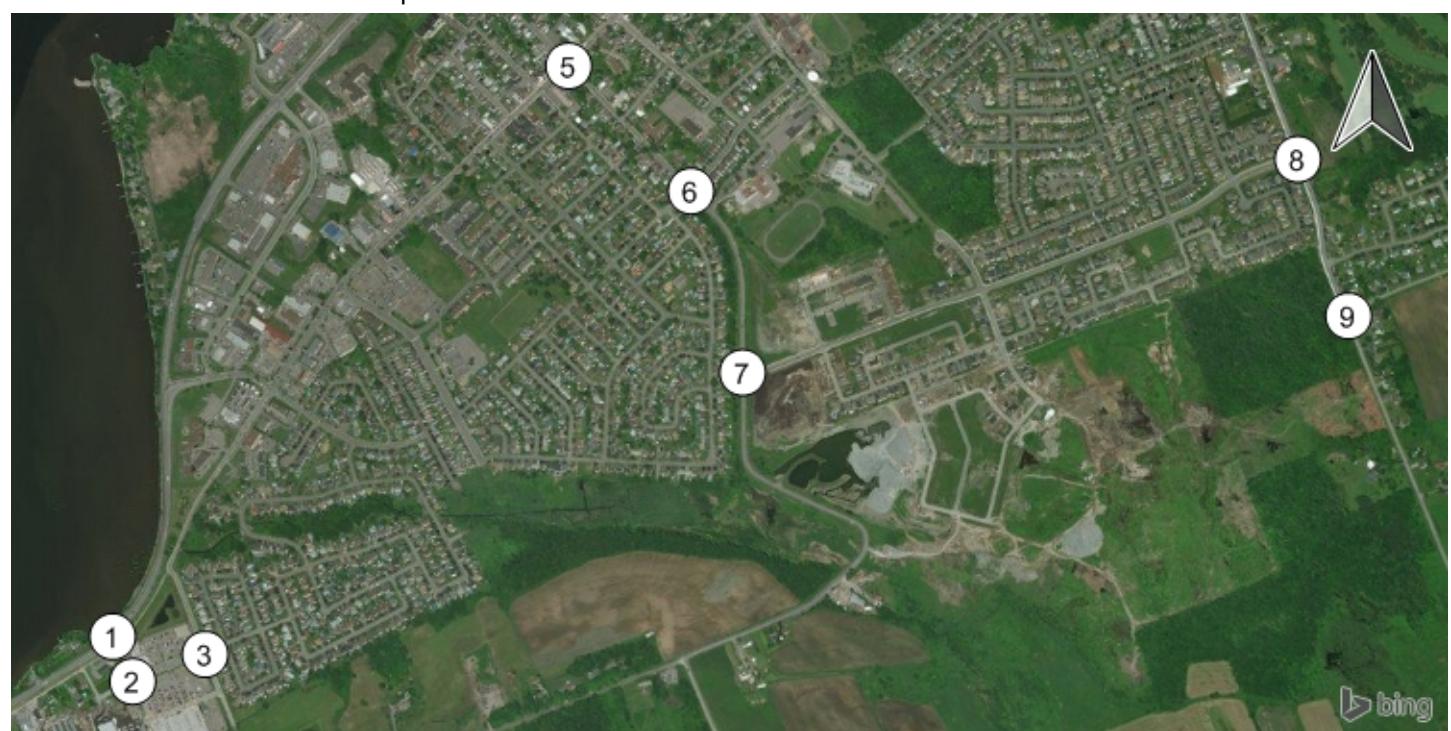
Traffic Volume - Net New Site Trips



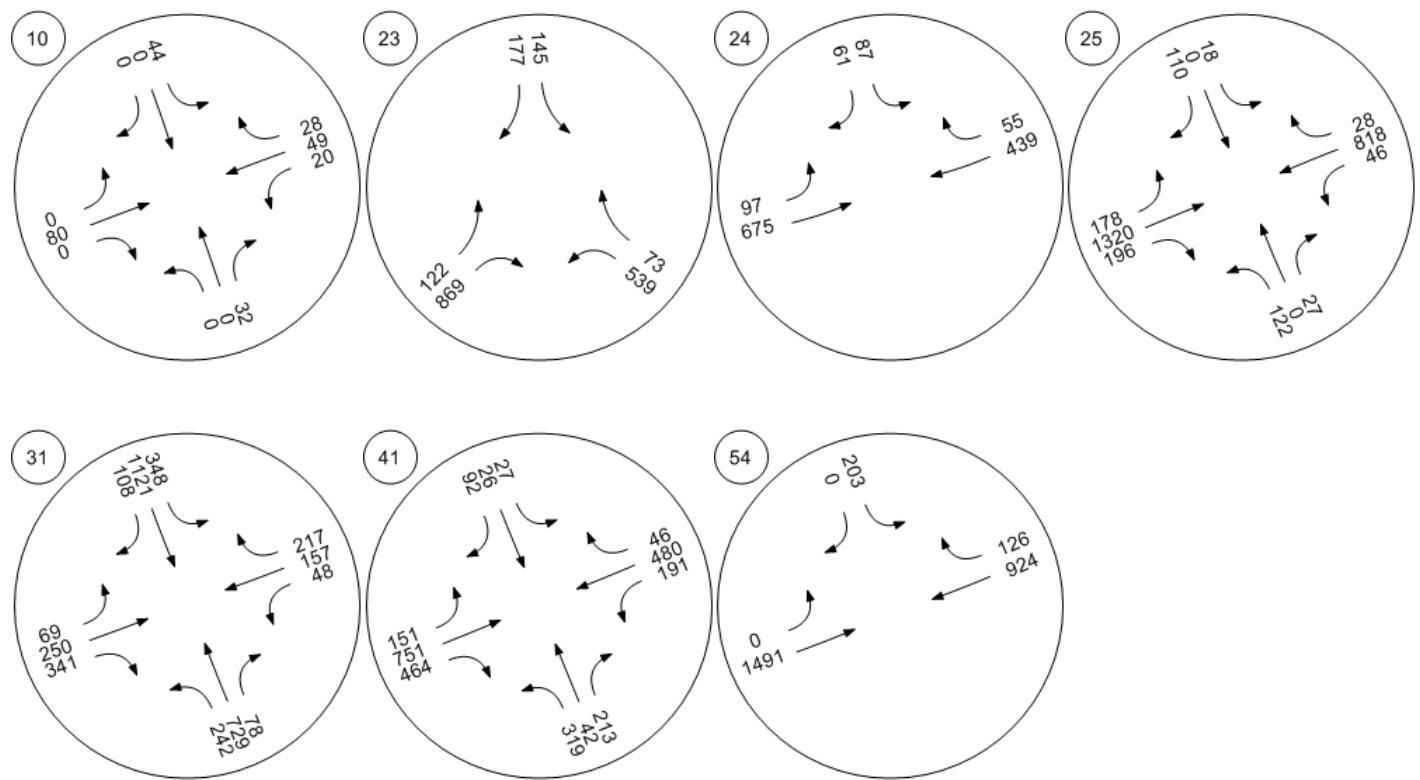
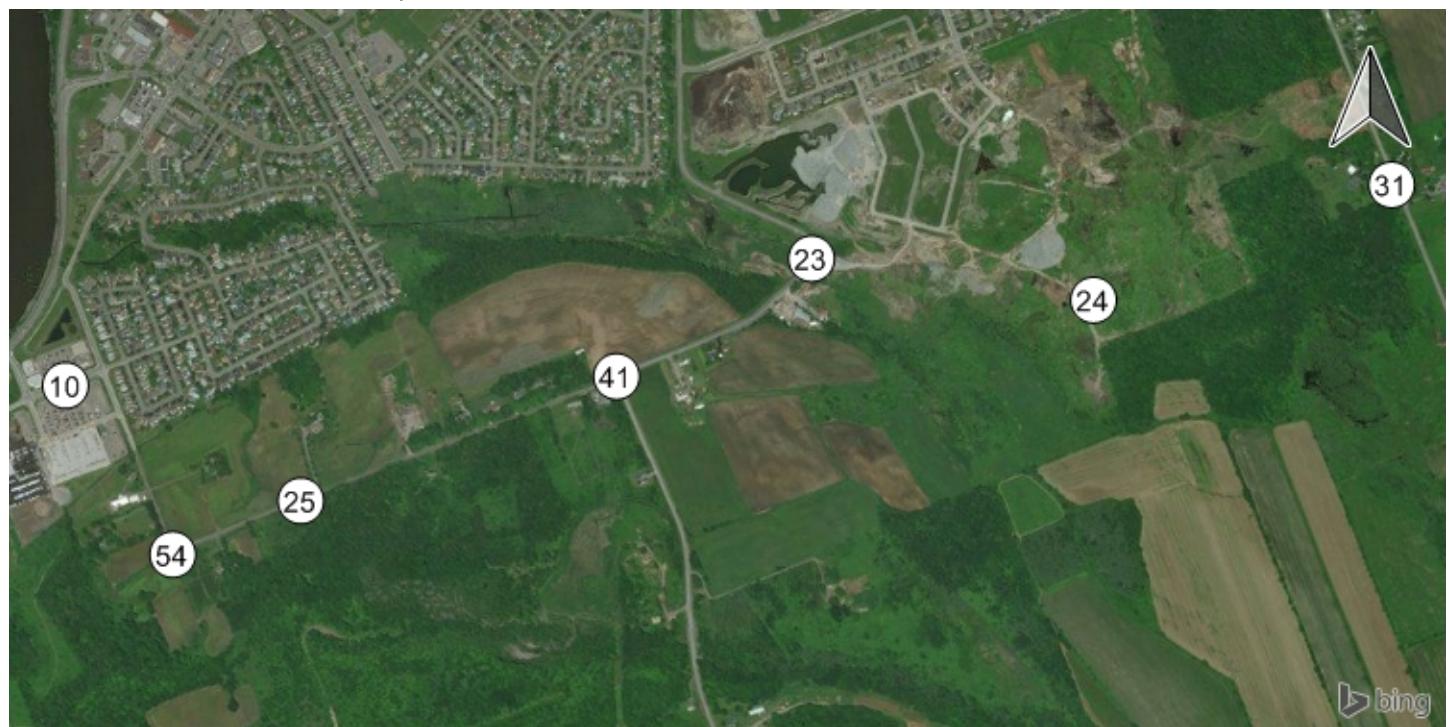
Traffic Volume - Net New Site Trips



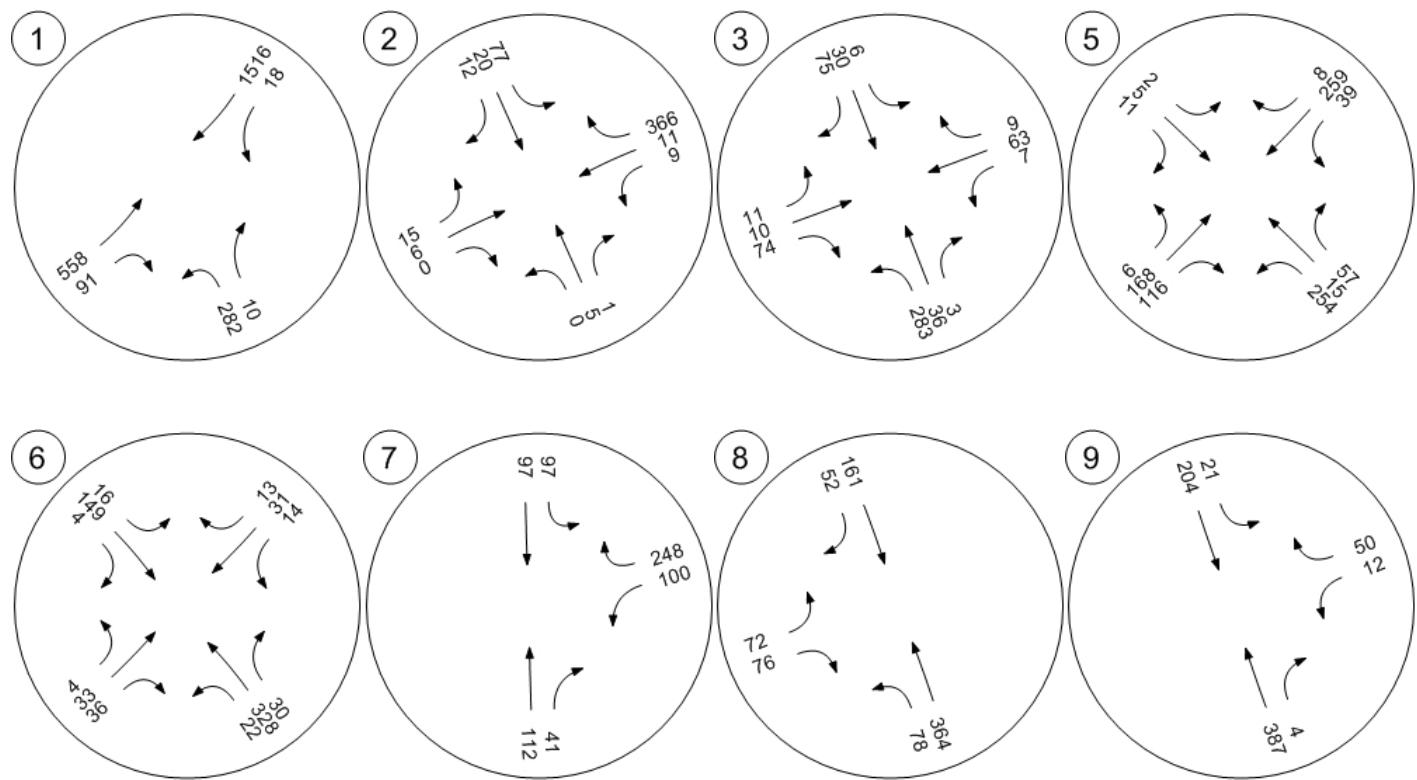
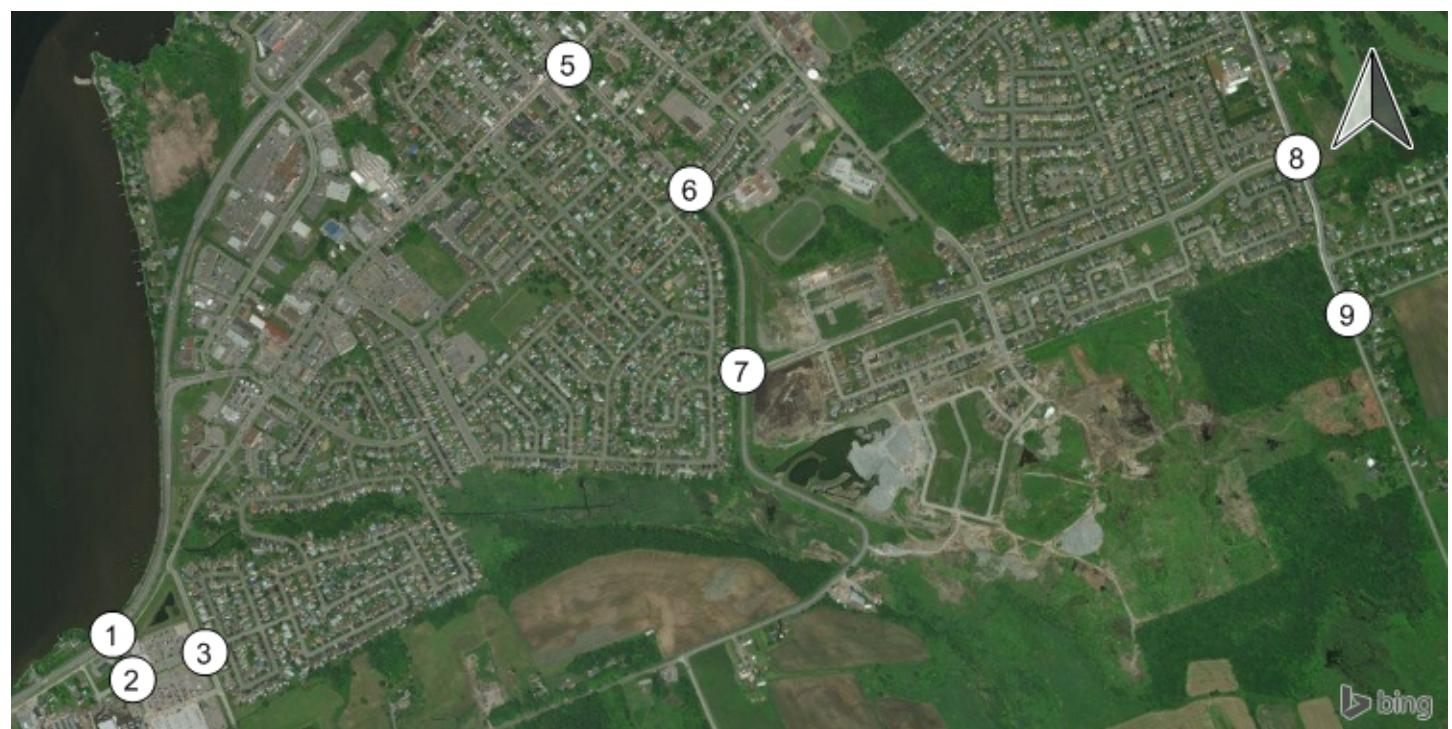
Traffic Volume - Net New Site Trips



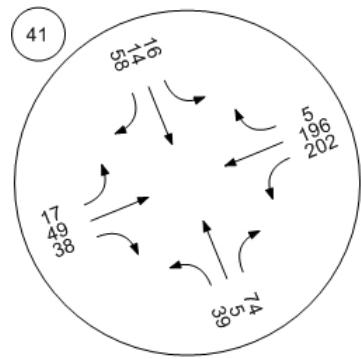
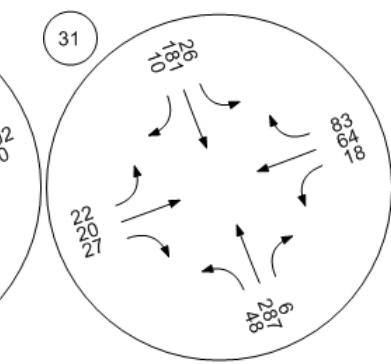
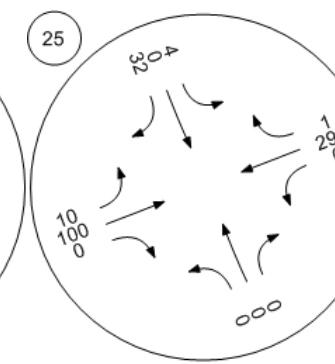
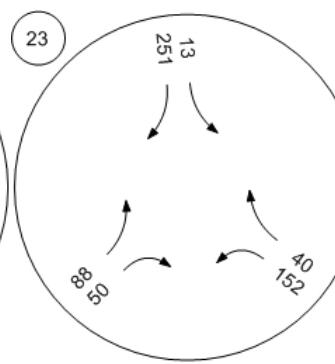
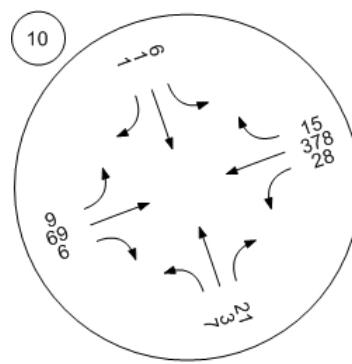
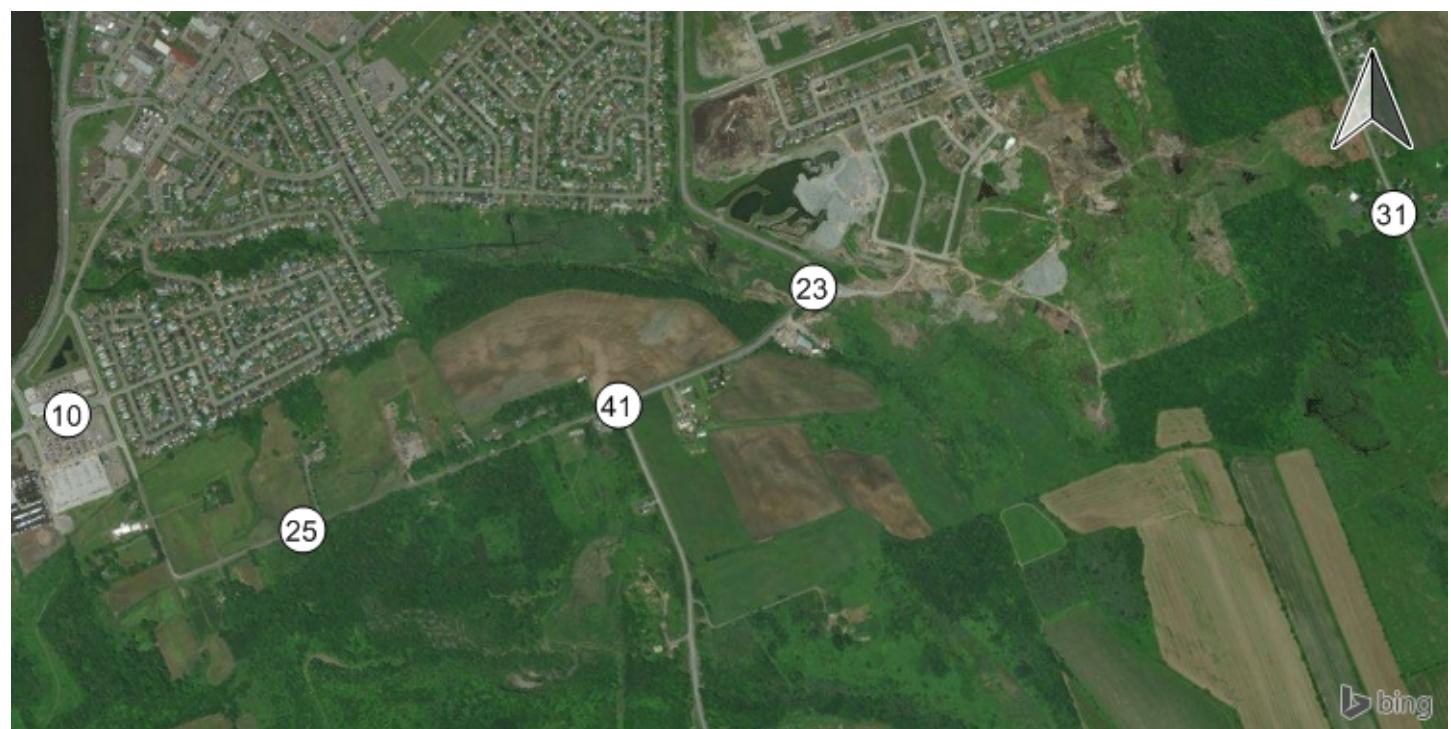
Traffic Volume - Net New Site Trips



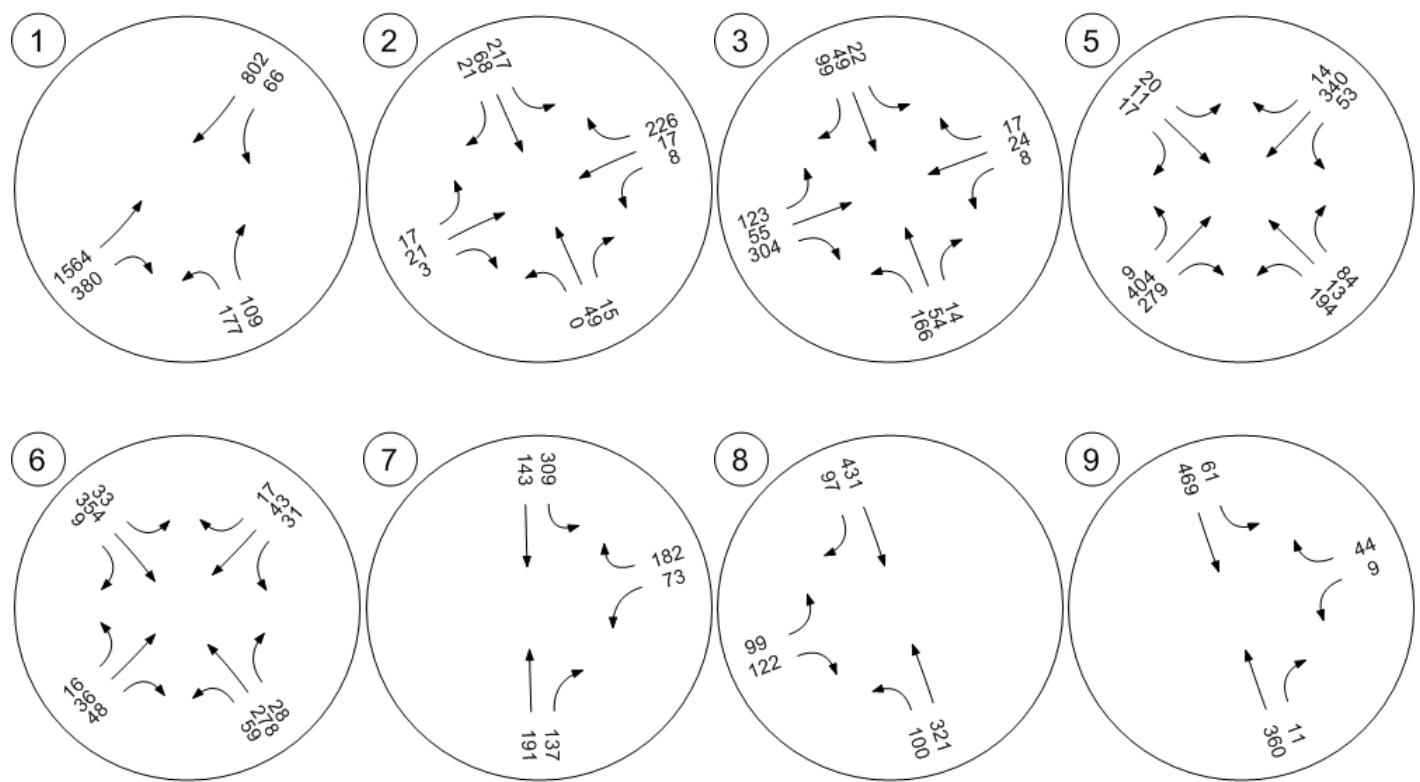
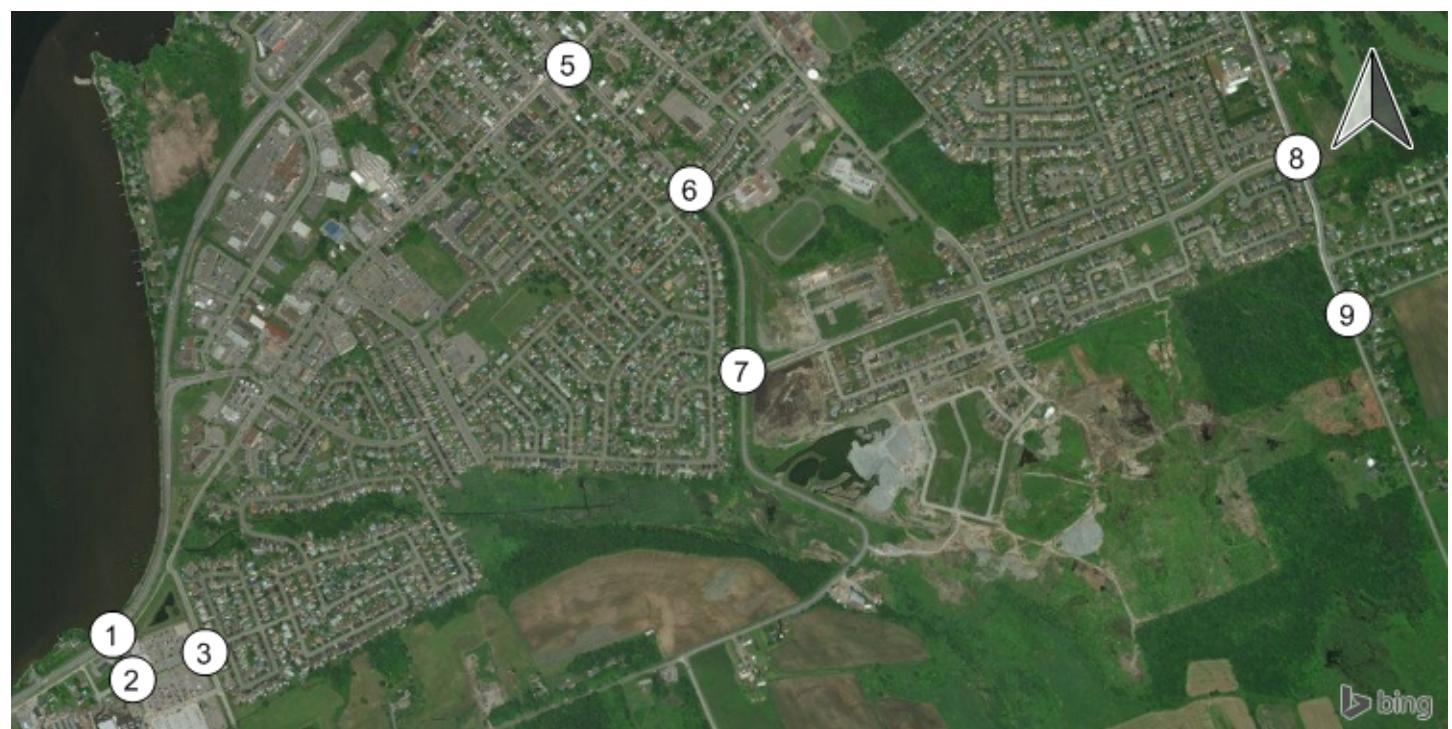
Traffic Volume - Future Total Volume



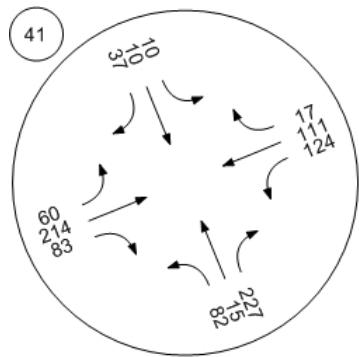
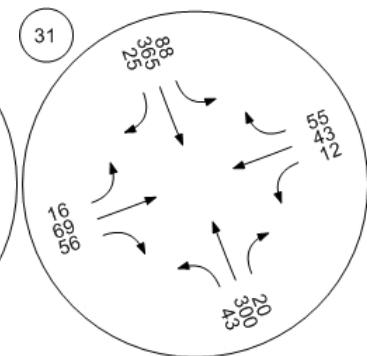
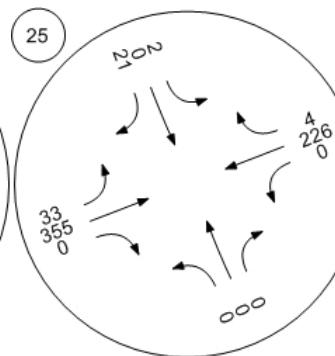
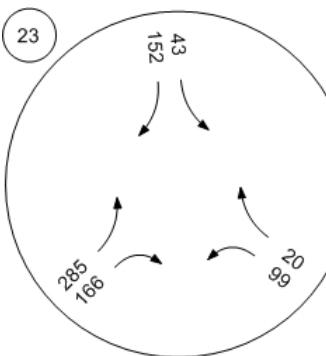
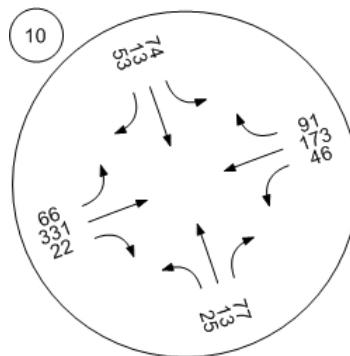
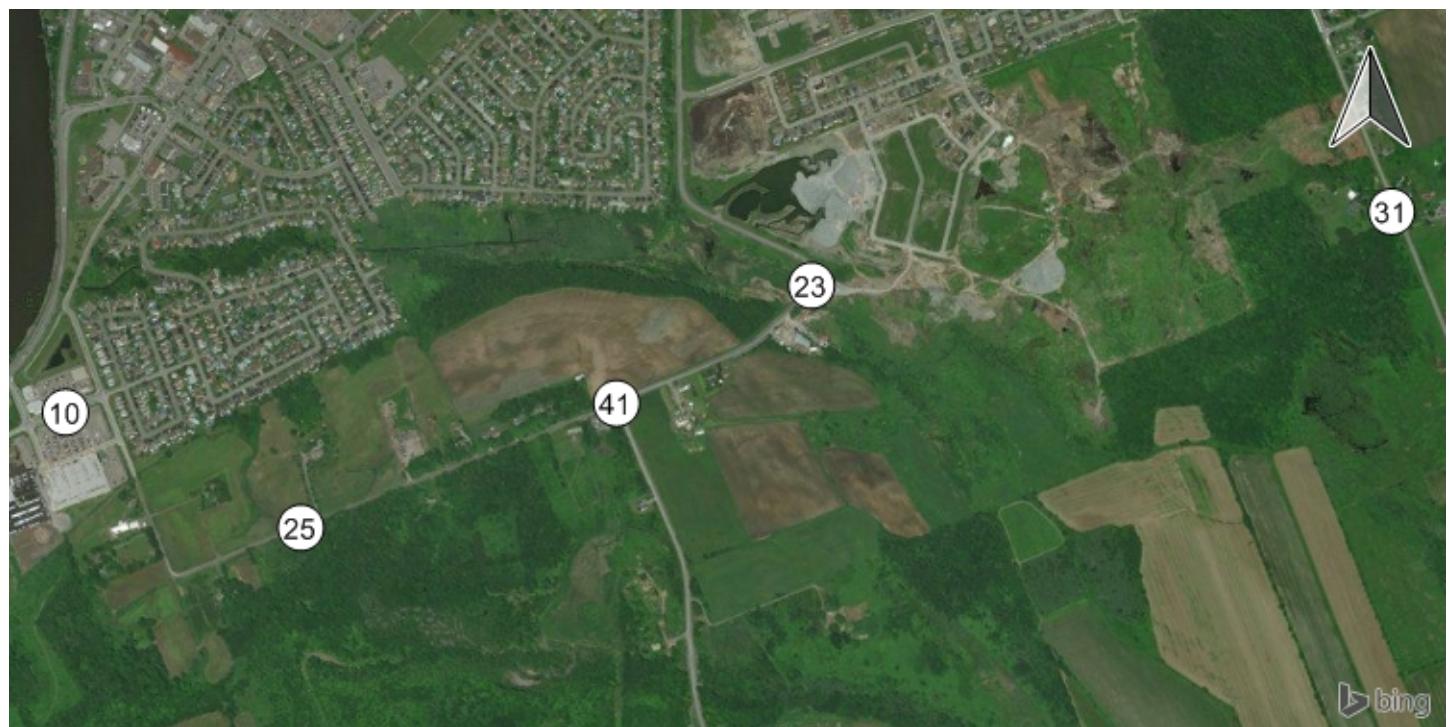
Traffic Volume - Future Total Volume



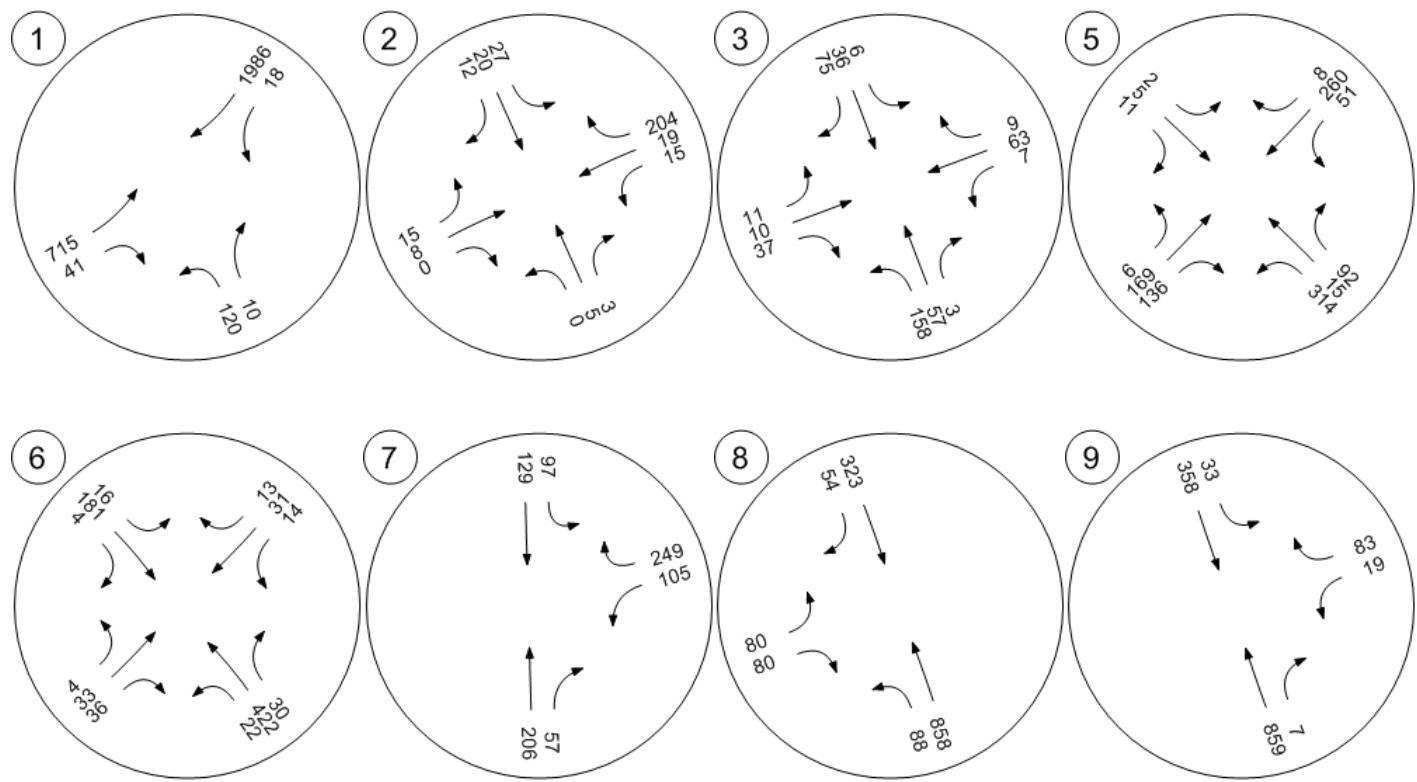
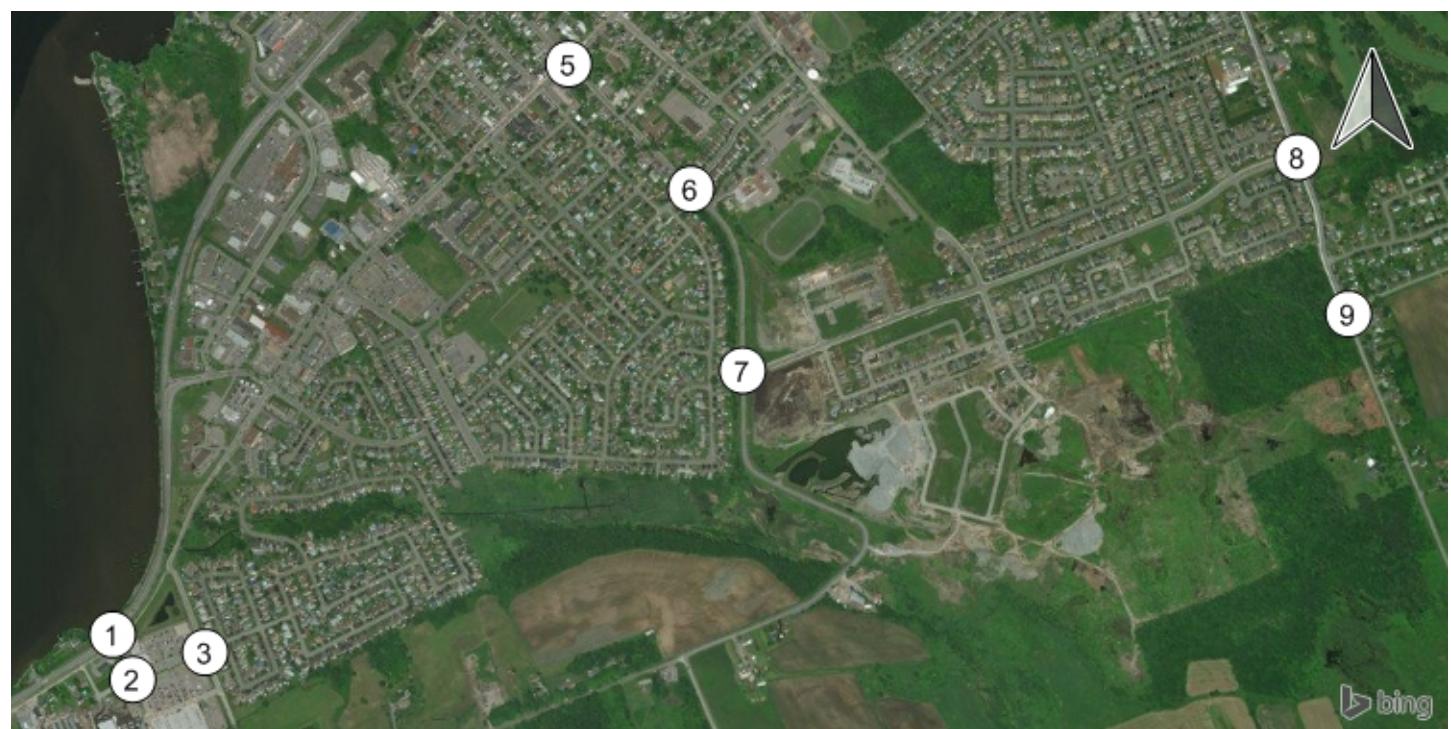
Traffic Volume - Future Total Volume



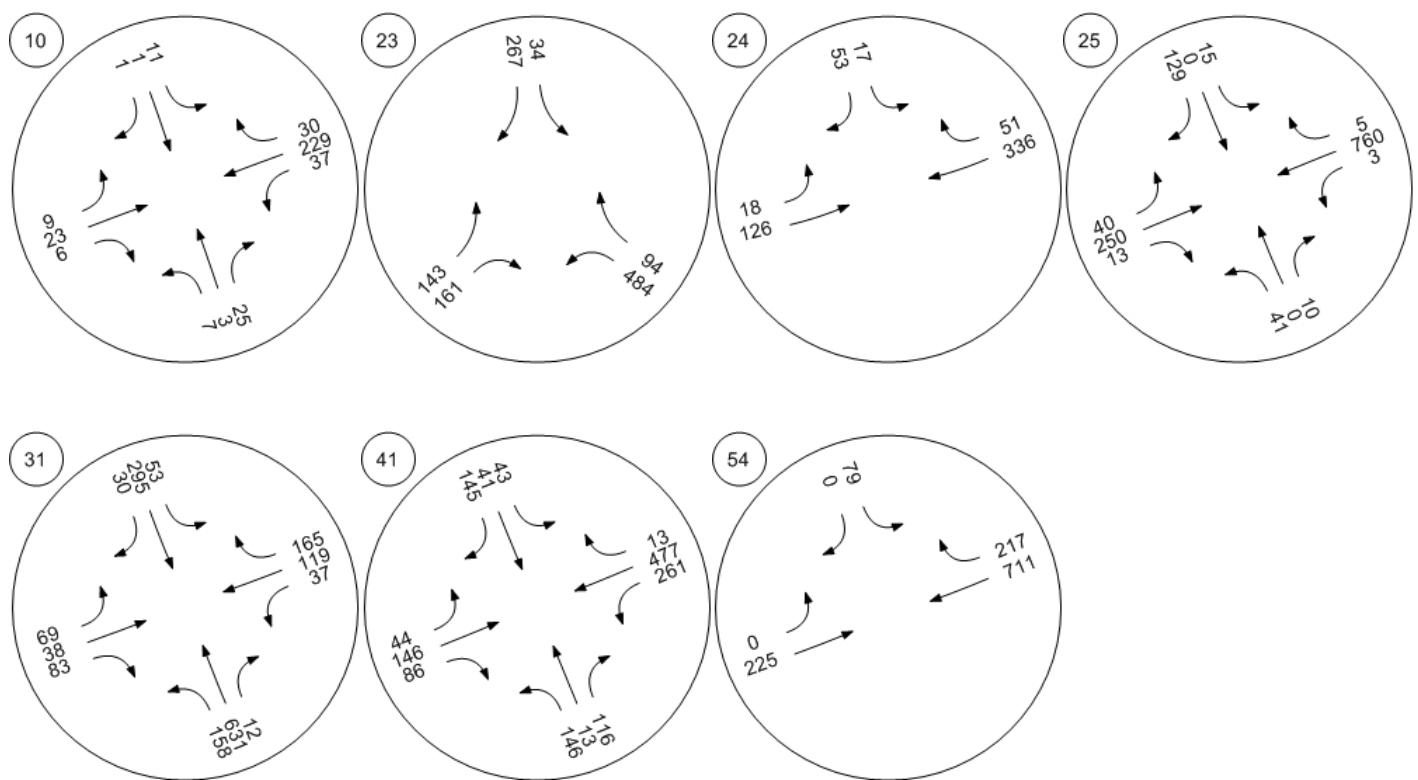
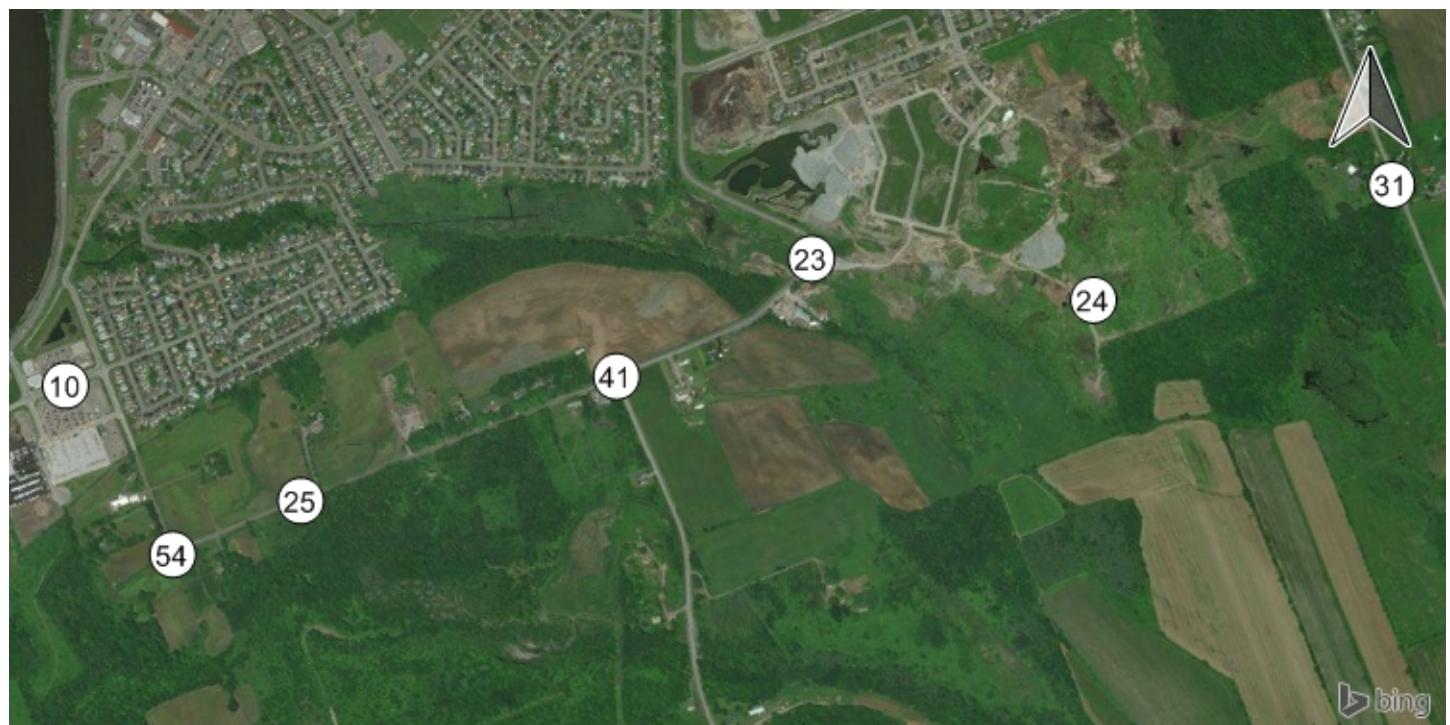
Traffic Volume - Future Total Volume



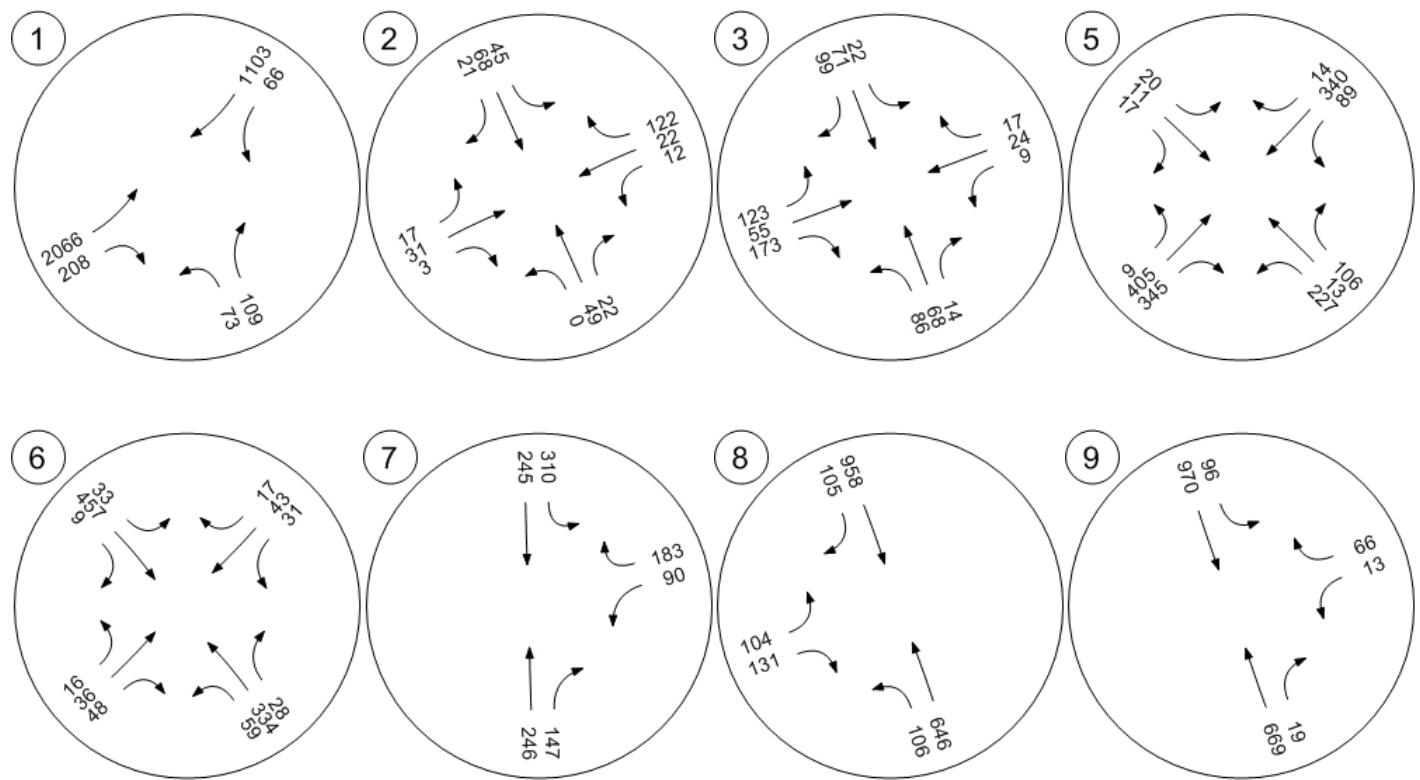
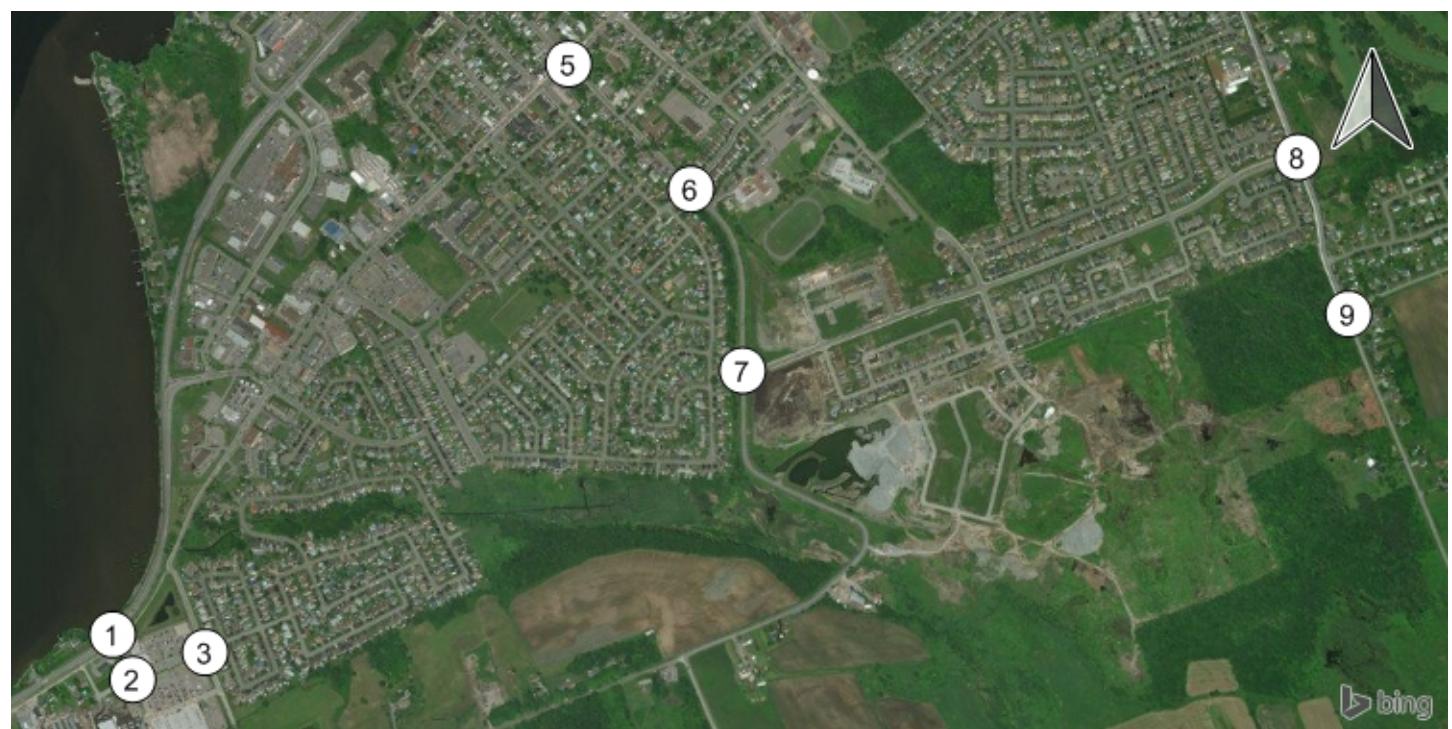
Traffic Volume - Future Total Volume



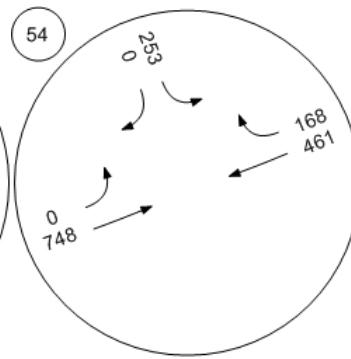
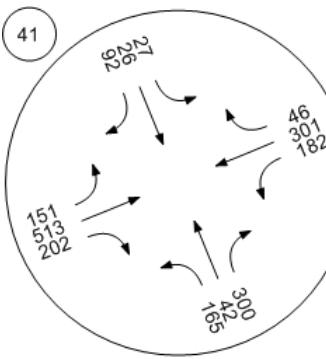
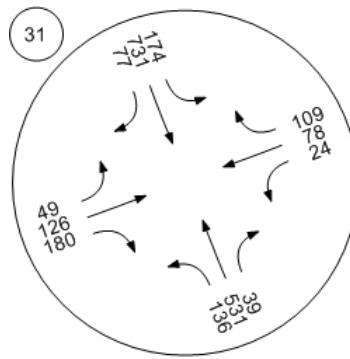
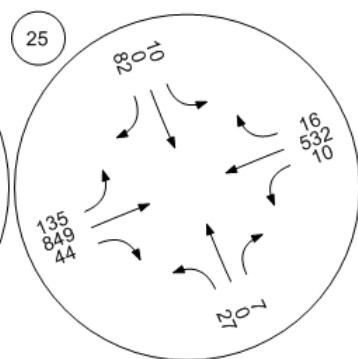
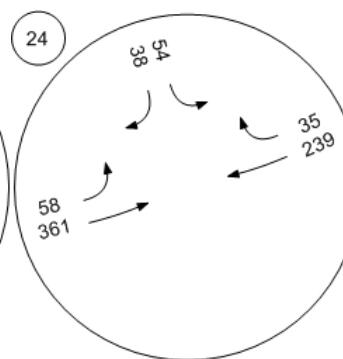
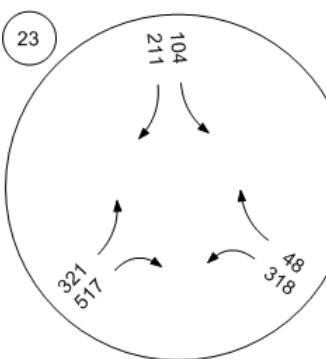
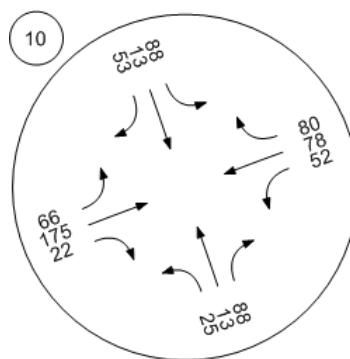
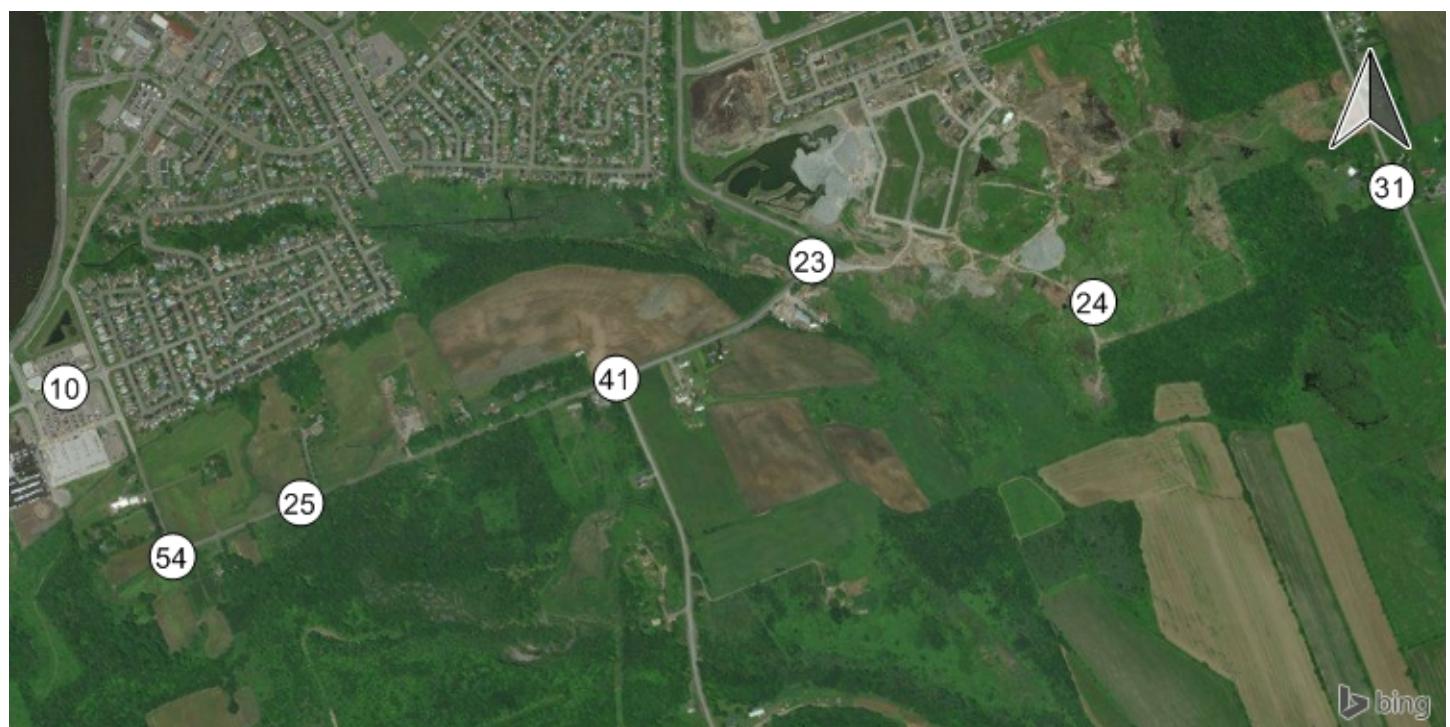
Traffic Volume - Future Total Volume



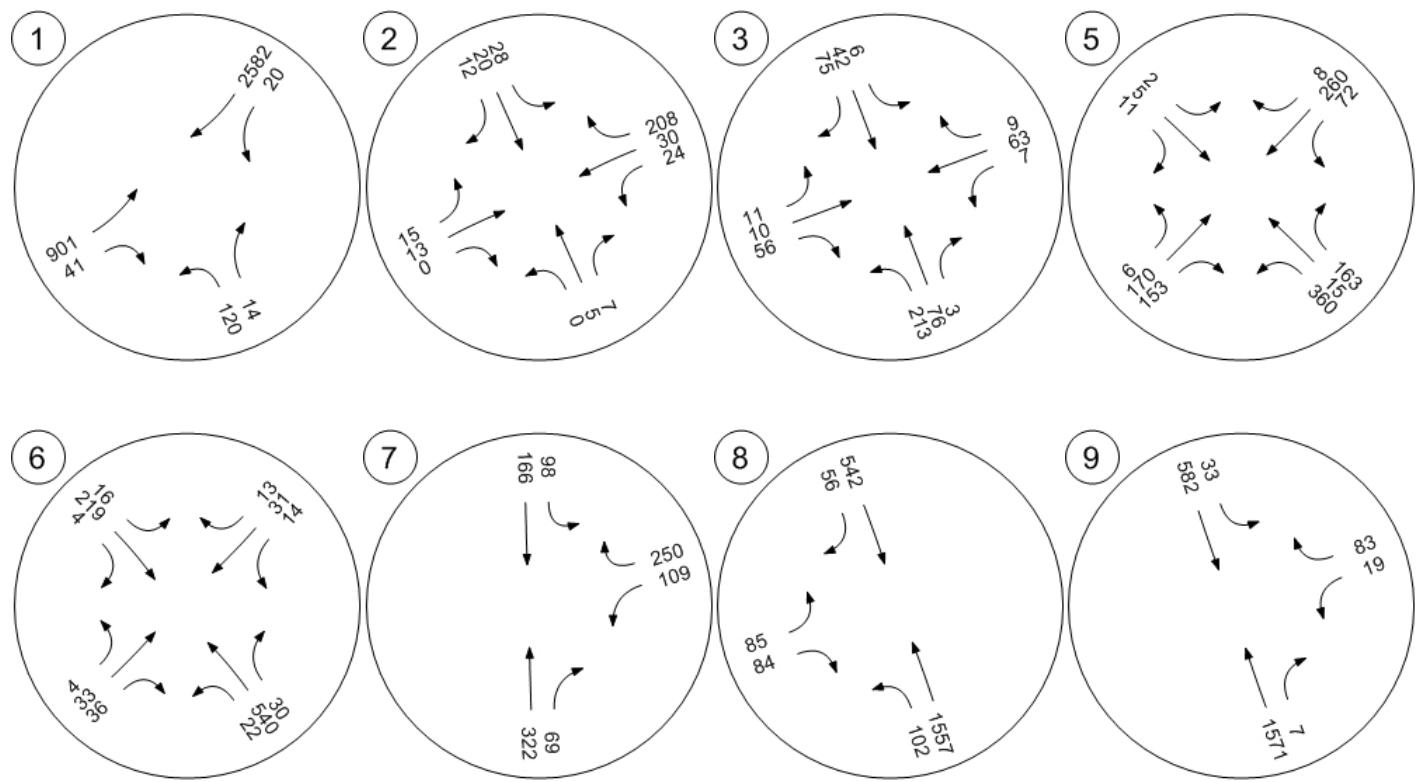
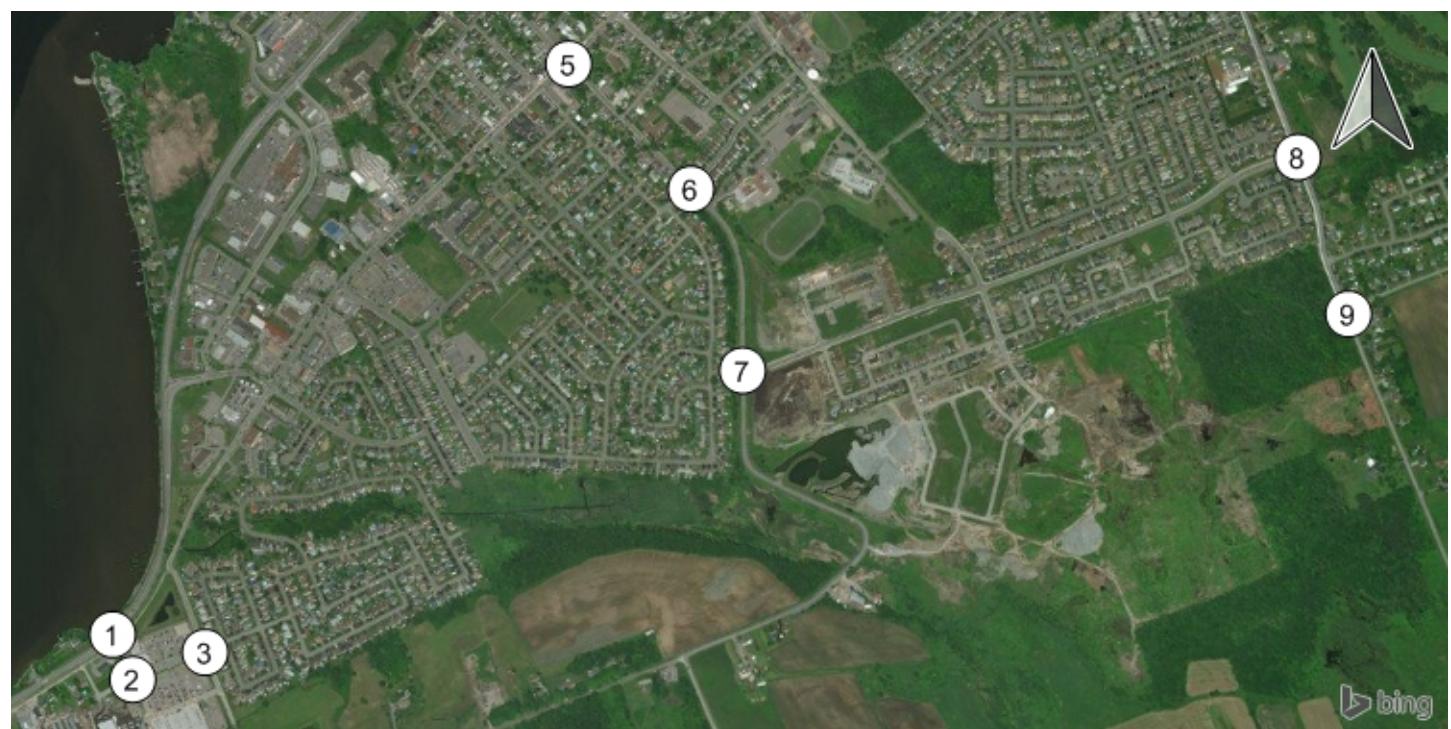
Traffic Volume - Future Total Volume



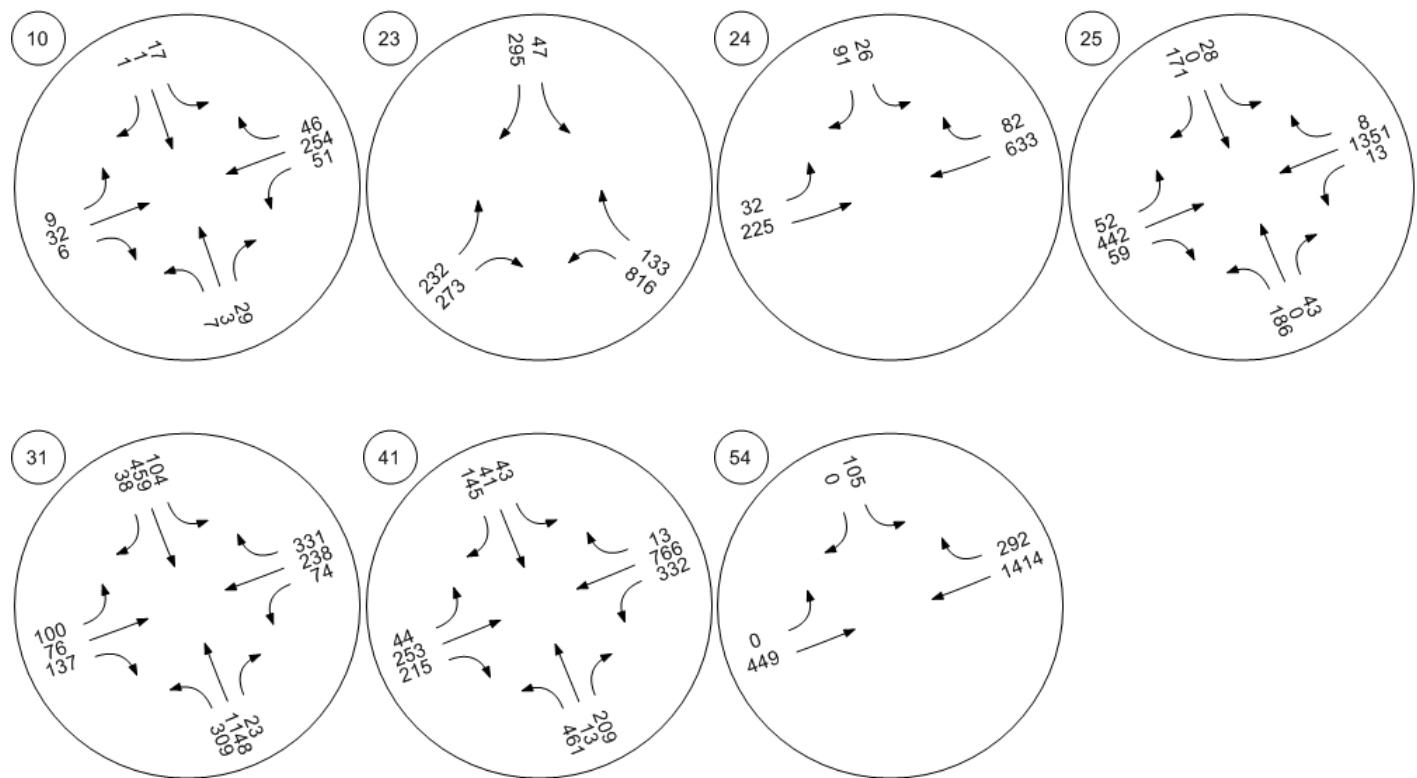
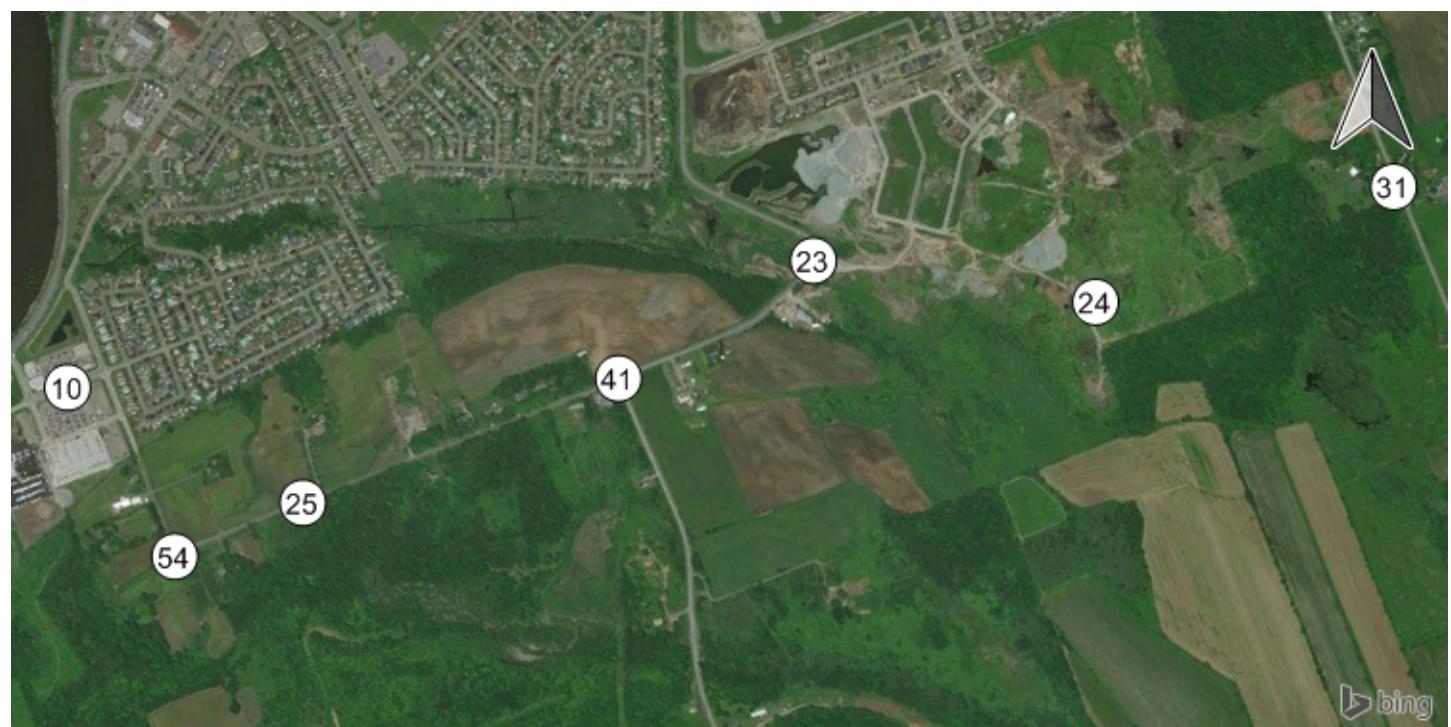
Traffic Volume - Future Total Volume



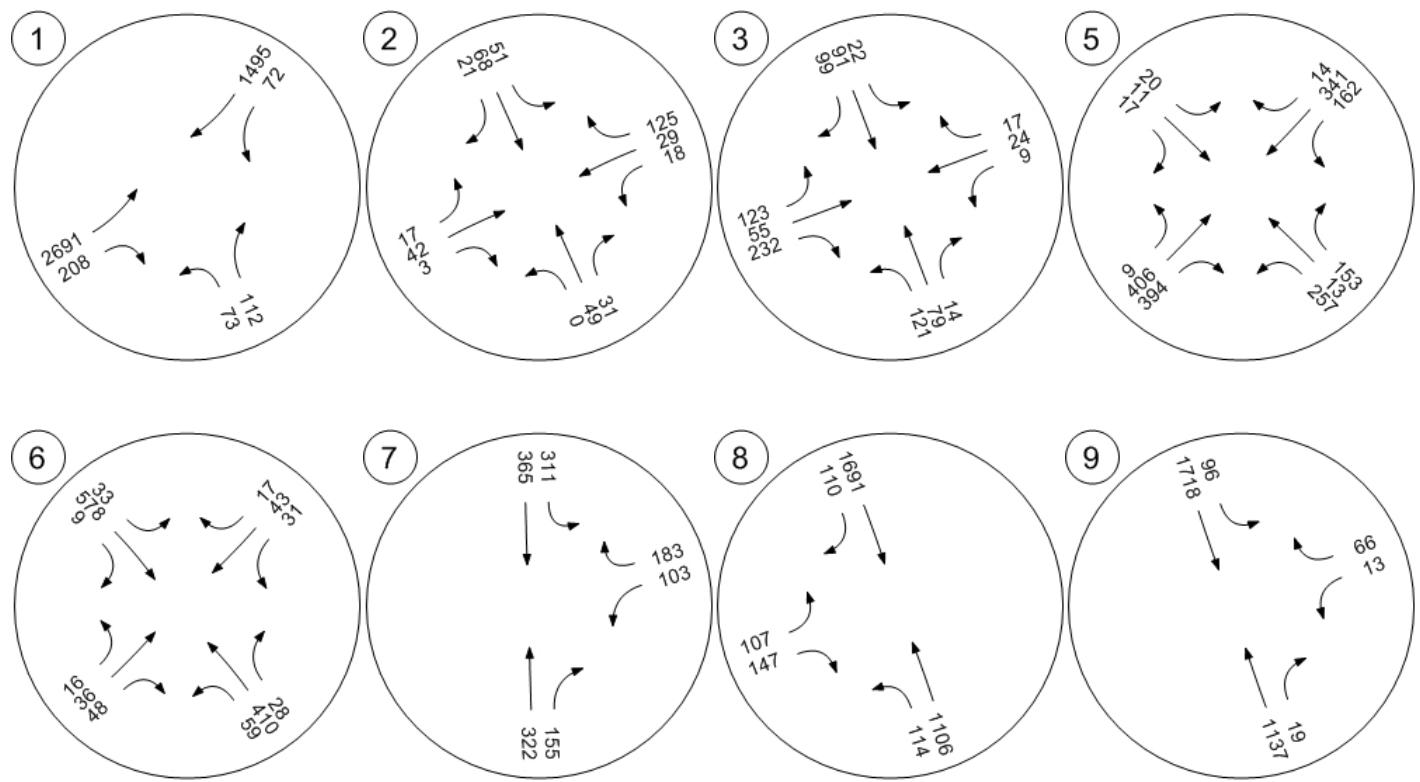
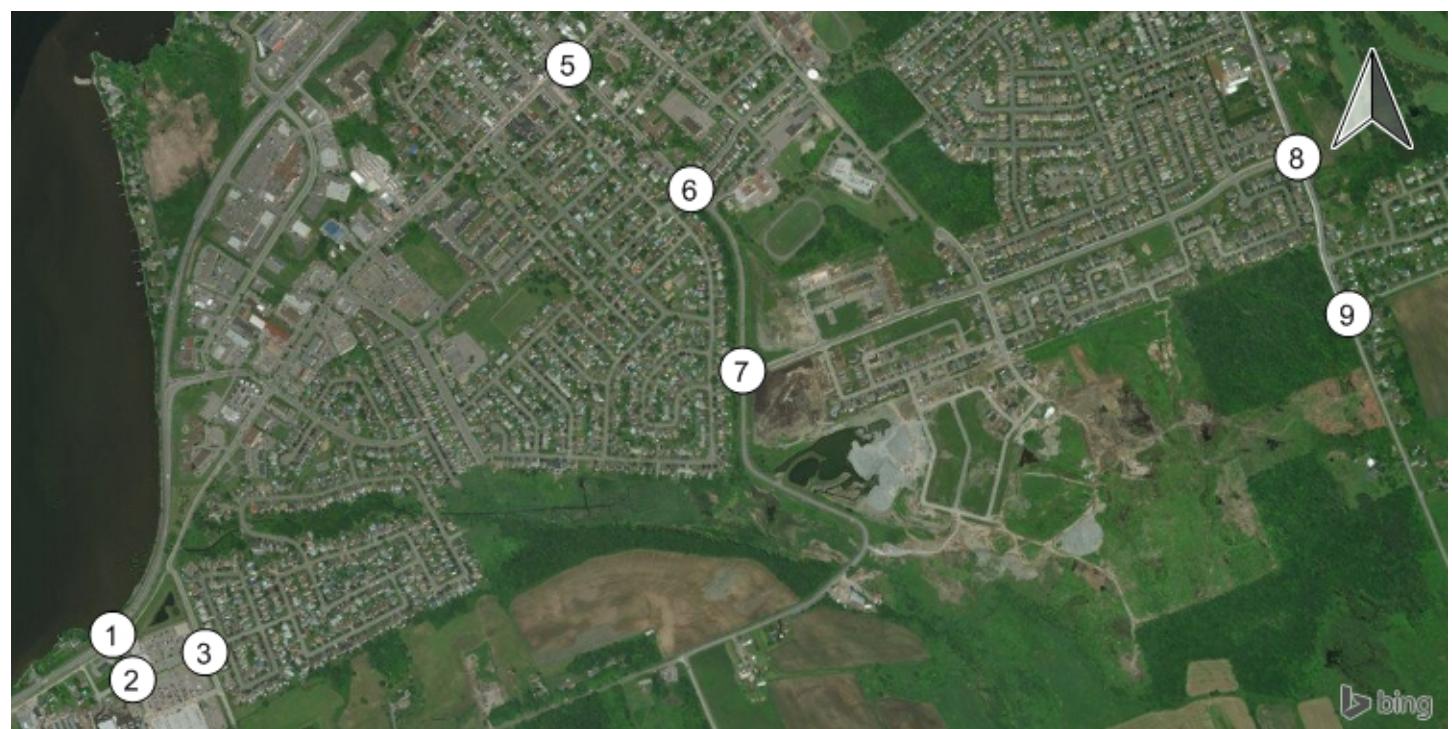
Traffic Volume - Future Total Volume



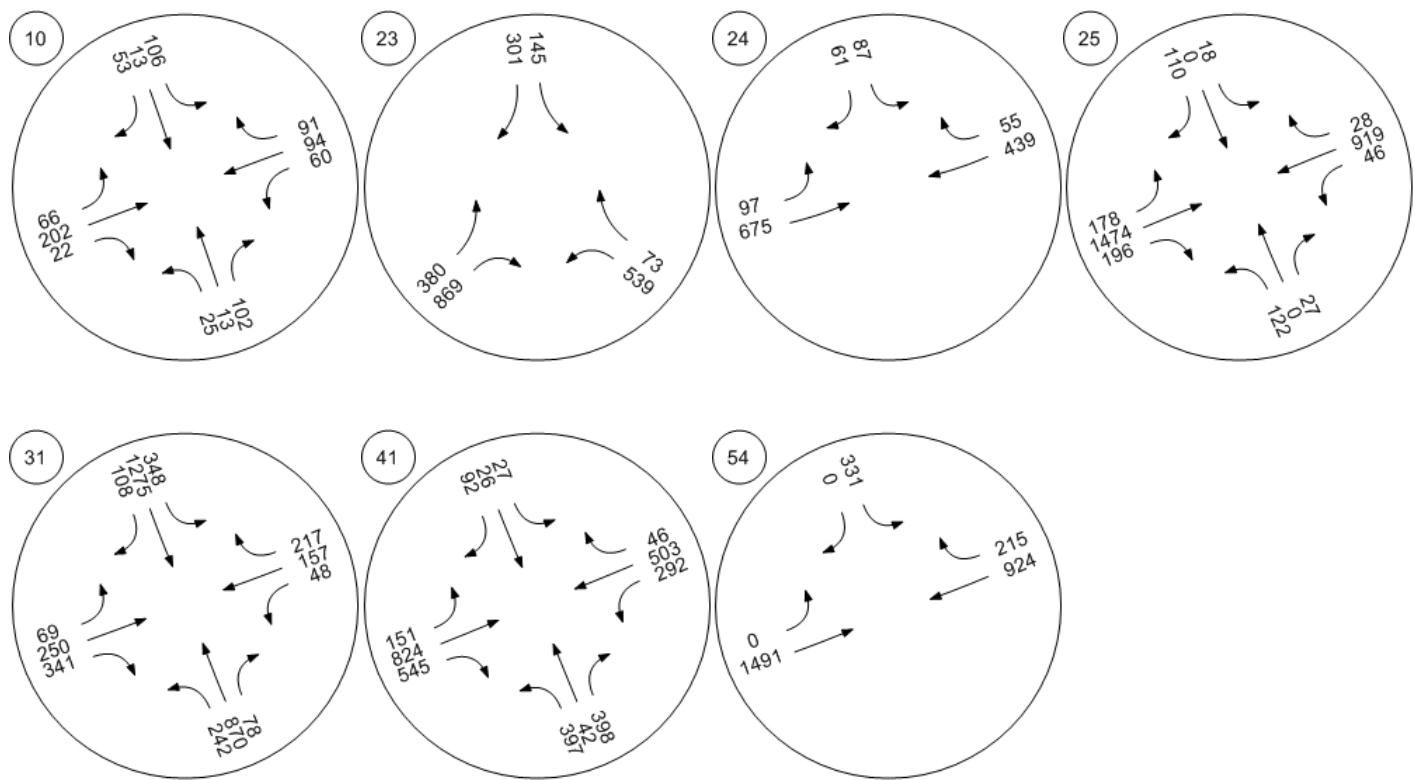
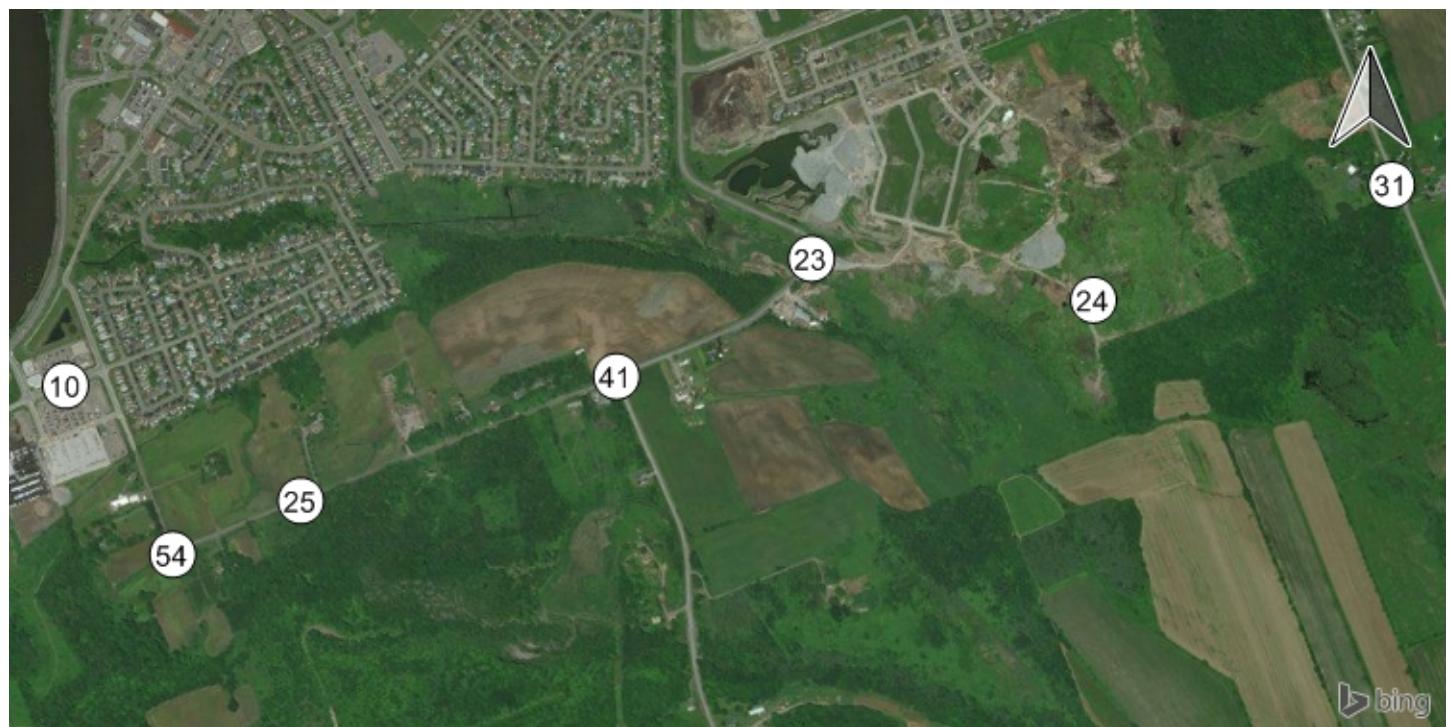
Traffic Volume - Future Total Volume



Traffic Volume - Future Total Volume



Traffic Volume - Future Total Volume



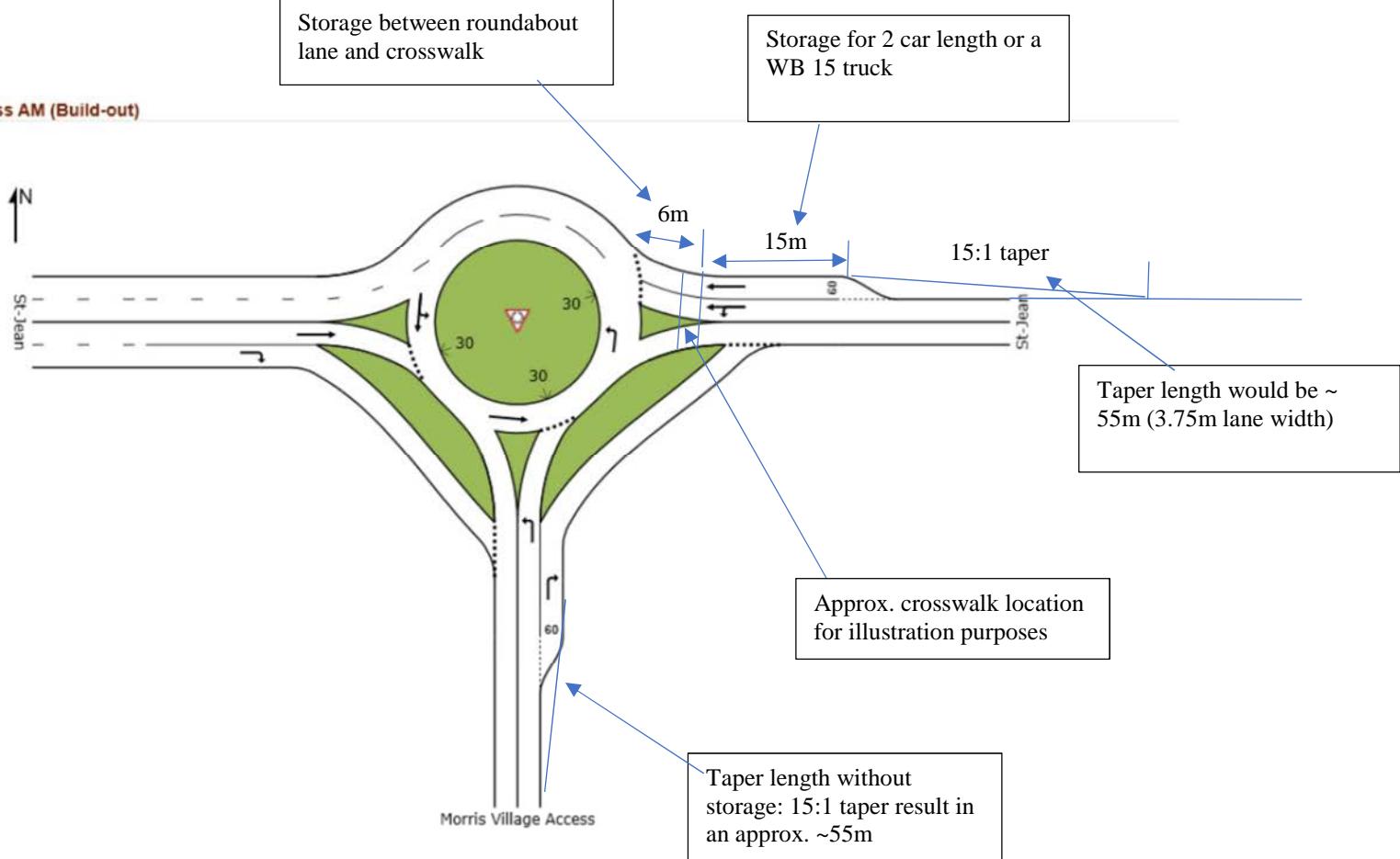
Appendix C

Roundabout Configuration (St-Jean/Street No.1 & St-Jean/Poupart)

SITE LAYOUT

Site: St-Jean / Morris Village Access AM (Build-out)

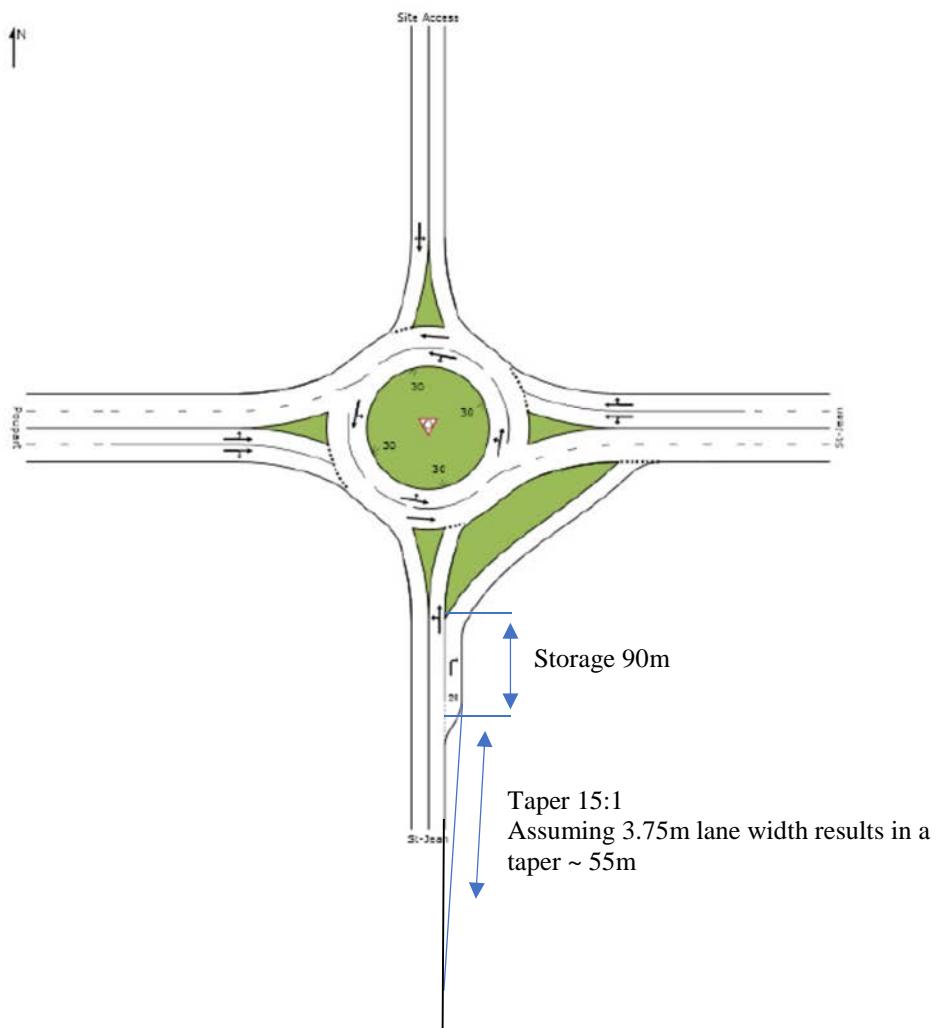
New Site
Roundabout



SITE LAYOUT

▼ Site: St-Jean / Poupart AM (Build-out)

New Site
Roundabout

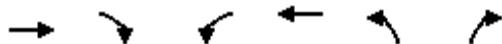


Appendix D

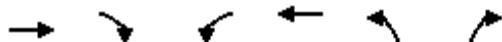
Forecast Traffic Analysis

Appendix D-1

Forecast Short-Term Traffic Analysis



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↗ | ↖ | ↖ | ↘ | ↗ |
| Traffic Volume (vph) | 558 | 91 | 18 | 1516 | 282 | 10 |
| Future Volume (vph) | 558 | 91 | 18 | 1516 | 282 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 1810 | 1524 | 1703 | 1881 | 1770 | 1346 |
| Flt Permitted | | | 0.335 | | 0.950 | |
| Satd. Flow (perm) | 1810 | 1524 | 600 | 1881 | 1770 | 1346 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 99 | | | 11 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 5% | 6% | 6% | 1% | 2% | 20% |
| Adj. Flow (vph) | 607 | 99 | 20 | 1648 | 307 | 11 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 607 | 99 | 20 | 1648 | 307 | 11 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 82.8 | 82.8 | 11.2 | 94.0 | 26.0 | 26.0 |
| Total Split (%) | 69.0% | 69.0% | 9.3% | 78.3% | 21.7% | 21.7% |
| Maximum Green (s) | 76.6 | 76.6 | 5.0 | 87.8 | 20.8 | 20.8 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 83.3 | 83.3 | 87.8 | 87.8 | 20.8 | 20.8 |
| Actuated g/C Ratio | 0.69 | 0.69 | 0.73 | 0.73 | 0.17 | 0.17 |
| v/c Ratio | 0.48 | 0.09 | 0.04 | 1.20 | 1.00 | 0.05 |
| Control Delay | 10.9 | 1.8 | 4.6 | 115.8 | 102.1 | 20.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 10.9 | 1.8 | 4.6 | 115.8 | 102.1 | 20.8 |
| LOS | B | A | A | F | F | C |
| Approach Delay | 9.6 | | | 114.4 | 99.3 | |
| Approach LOS | A | | | F | F | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 120

Natural Cycle: 150

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 1.20

Intersection Signal Delay: 85.2

Intersection LOS: F

Intersection Capacity Utilization 104.9%

ICU Level of Service G

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | → | → | → | ← | ← | ← | ↑ | ↑ | ↓ | ↓ | ↙ | |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 6 | 168 | 116 | 39 | 259 | 8 | 254 | 15 | 57 | 2 | 5 | 11 |
| Future Volume (vph) | 6 | 168 | 116 | 39 | 259 | 8 | 254 | 15 | 57 | 2 | 5 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.996 | | | 0.881 | | | 0.894 | |
| Flt Protected | | 0.998 | | | 0.994 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1843 | 1568 | 0 | 1874 | 0 | 1719 | 1461 | 0 | 1805 | 1604 | 0 |
| Flt Permitted | | 0.984 | | | 0.952 | | 0.746 | | | 0.706 | | |
| Satd. Flow (perm) | 0 | 1817 | 1568 | 0 | 1795 | 0 | 1350 | 1461 | 0 | 1341 | 1604 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 127 | | | 3 | | | 62 | | | 12 | |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 549.0 | | | 622.7 | | | 441.7 | | | 187.4 | |
| Travel Time (s) | | 39.5 | | | 44.8 | | | 31.8 | | | 13.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 3% | 3% | 3% | 0% | 0% | 5% | 13% | 15% | 0% | 20% | 0% |
| Adj. Flow (vph) | 7 | 183 | 126 | 42 | 282 | 9 | 276 | 16 | 62 | 2 | 5 | 12 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 190 | 126 | 0 | 333 | 0 | 276 | 78 | 0 | 2 | 17 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 33.0 | | 27.0 | 27.0 | | 27.0 | 27.0 | |
| Total Split (%) | 38.3% | 38.3% | 38.3% | 16.7% | 55.0% | | 45.0% | 45.0% | | 45.0% | 45.0% | |
| Maximum Green (s) | 18.0 | 18.0 | 18.0 | 5.0 | 28.0 | | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 18.0 | 18.0 | | 28.0 | | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Actuated g/C Ratio | | 0.30 | 0.30 | | 0.47 | | 0.37 | 0.37 | | 0.37 | 0.37 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|------|------|-----|------|------|------|------|------|------|------|-----|-----|
| v/c Ratio | 0.35 | 0.23 | | 0.39 | | 0.56 | 0.14 | | 0.00 | 0.03 | | |
| Control Delay | 18.7 | | 4.8 | | 12.0 | | 20.4 | 6.0 | | 12.0 | 8.3 | |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 18.7 | | 4.8 | | 12.0 | | 20.4 | 6.0 | | 12.0 | 8.3 | |
| LOS | B | | A | | B | | C | A | | B | A | |
| Approach Delay | 13.1 | | | | 12.0 | | | 17.2 | | | 8.7 | |
| Approach LOS | B | | | | B | | | B | | | A | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.56

Intersection Signal Delay: 14.1

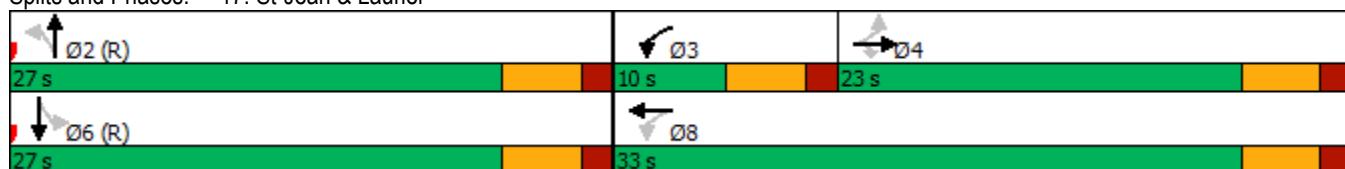
Intersection LOS: B

Intersection Capacity Utilization 58.7%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



Intersection

Intersection Delay, s/veh 11
Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 328 | 30 | 16 | 149 | 4 |
| Future Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 328 | 30 | 16 | 149 | 4 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 6 | 0 | 14 | 6 | 0 | 5 | 3 | 10 | 0 | 1 | 25 |
| Mvmt Flow | 4 | 36 | 39 | 15 | 34 | 14 | 24 | 357 | 33 | 17 | 162 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.8 | | | 9.2 | | | 12.4 | | | 9.3 | | |
| HCM LOS | A | | | A | | | B | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 6% | 5% | 24% | 9% |
| Vol Thru, % | 86% | 45% | 53% | 88% |
| Vol Right, % | 8% | 49% | 22% | 2% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 380 | 73 | 58 | 169 |
| LT Vol | 22 | 4 | 14 | 16 |
| Through Vol | 328 | 33 | 31 | 149 |
| RT Vol | 30 | 36 | 13 | 4 |
| Lane Flow Rate | 413 | 79 | 63 | 184 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.52 | 0.112 | 0.097 | 0.242 |
| Departure Headway (Hd) | 4.532 | 5.069 | 5.528 | 4.738 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 793 | 701 | 643 | 753 |
| Service Time | 2.578 | 3.142 | 3.605 | 2.793 |
| HCM Lane V/C Ratio | 0.521 | 0.113 | 0.098 | 0.244 |
| HCM Control Delay | 12.4 | 8.8 | 9.2 | 9.3 |
| HCM Lane LOS | B | A | A | A |
| HCM 95th-tile Q | 3.1 | 0.4 | 0.3 | 0.9 |

Intersection

Intersection Delay, s/veh 11.9

Intersection LOS B

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|------|------|------|------|------|------|
| Lane Configurations | Y | | P | | T | ↑ |
| Traffic Vol, veh/h | 19 | 50 | 387 | 4 | 21 | 204 |
| Future Vol, veh/h | 19 | 50 | 387 | 4 | 21 | 204 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 40 | 13 | 9 | 0 | 18 | 13 |
| Mvmt Flow | 21 | 54 | 421 | 4 | 23 | 222 |
| Number of Lanes | 1 | 0 | 1 | 0 | 1 | 1 |
| Approach | WB | | NB | | SB | |
| Opposing Approach | | | SB | | NB | |
| Opposing Lanes | 0 | | 2 | | 1 | |
| Conflicting Approach Left | NB | | | WB | | |
| Conflicting Lanes Left | 1 | | 0 | | 1 | |
| Conflicting Approach Right | SB | | WB | | | |
| Conflicting Lanes Right | 2 | | 1 | | 0 | |
| HCM Control Delay | 9.6 | | 13.3 | | 10.3 | |
| HCM LOS | A | | B | | B | |

| Lane | NBLn1 | WBLn1 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 0% | 28% | 100% | 0% |
| Vol Thru, % | 99% | 0% | 0% | 100% |
| Vol Right, % | 1% | 72% | 0% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 391 | 69 | 21 | 204 |
| LT Vol | 0 | 19 | 21 | 0 |
| Through Vol | 387 | 0 | 0 | 204 |
| RT Vol | 4 | 50 | 0 | 0 |
| Lane Flow Rate | 425 | 75 | 23 | 222 |
| Geometry Grp | 5 | 2 | 7 | 7 |
| Degree of Util (X) | 0.55 | 0.12 | 0.037 | 0.324 |
| Departure Headway (Hd) | 4.66 | 5.759 | 5.856 | 5.266 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 773 | 620 | 611 | 683 |
| Service Time | 2.691 | 3.816 | 3.594 | 3.005 |
| HCM Lane V/C Ratio | 0.55 | 0.121 | 0.038 | 0.325 |
| HCM Control Delay | 13.3 | 9.6 | 8.8 | 10.5 |
| HCM Lane LOS | B | A | A | B |
| HCM 95th-tile Q | 3.4 | 0.4 | 0.1 | 1.4 |

Intersection

Intersection Delay, s/veh 11.8

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 17 | 49 | 38 | 202 | 196 | 5 | 39 | 5 | 74 | 16 | 14 | 58 |
| Future Vol, veh/h | 17 | 49 | 38 | 202 | 196 | 5 | 39 | 5 | 74 | 16 | 14 | 58 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 2 | 43 | 0 | 1 | 0 | 2 | 0 | 2 | 5 | 2 | 2 | 2 |
| Mvmt Flow | 18 | 53 | 41 | 220 | 213 | 5 | 42 | 5 | 80 | 17 | 15 | 63 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | WB | | | NB | | | SB | | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | | 1 | | | 1 | | | 1 | |
| HCM Control Delay | 8.8 | | | 13.9 | | | 9.2 | | | 8.9 | | |
| HCM LOS | A | | B | | | A | | | A | | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 33% | 16% | 50% | 18% |
| Vol Thru, % | 4% | 47% | 49% | 16% |
| Vol Right, % | 63% | 37% | 1% | 66% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 118 | 104 | 403 | 88 |
| LT Vol | 39 | 17 | 202 | 16 |
| Through Vol | 5 | 49 | 196 | 14 |
| RT Vol | 74 | 38 | 5 | 58 |
| Lane Flow Rate | 128 | 113 | 438 | 96 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.179 | 0.152 | 0.572 | 0.134 |
| Departure Headway (Hd) | 5.027 | 4.828 | 4.697 | 5.062 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 707 | 735 | 762 | 700 |
| Service Time | 3.11 | 2.91 | 2.758 | 3.15 |
| HCM Lane V/C Ratio | 0.181 | 0.154 | 0.575 | 0.137 |
| HCM Control Delay | 9.2 | 8.8 | 13.9 | 8.9 |
| HCM Lane LOS | A | A | B | A |
| HCM 95th-tile Q | 0.6 | 0.5 | 3.7 | 0.5 |

Intersection

Intersection Delay, s/veh 10.2

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↓ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 11 | 10 | 74 | 7 | 63 | 9 | 283 | 36 | 3 | 6 | 30 | 75 |
| Future Vol, veh/h | 11 | 10 | 74 | 7 | 63 | 9 | 283 | 36 | 3 | 6 | 30 | 75 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 22 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 33 | 0 | 4 | 0 |
| Mvmt Flow | 12 | 11 | 80 | 8 | 68 | 10 | 308 | 39 | 3 | 7 | 33 | 82 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 8.7 | | | 9 | | | 11.7 | | | 8.2 | | |
| HCM LOS | A | | | A | | | B | | | A | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 88% | 100% | 0% | 9% | 5% |
| Vol Thru, % | 11% | 0% | 12% | 80% | 27% |
| Vol Right, % | 1% | 0% | 88% | 11% | 68% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 322 | 11 | 84 | 79 | 111 |
| LT Vol | 283 | 11 | 0 | 7 | 6 |
| Through Vol | 36 | 0 | 10 | 63 | 30 |
| RT Vol | 3 | 0 | 74 | 9 | 75 |
| Lane Flow Rate | 350 | 12 | 91 | 86 | 121 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.459 | 0.022 | 0.129 | 0.124 | 0.148 |
| Departure Headway (Hd) | 4.72 | 6.594 | 5.086 | 5.206 | 4.408 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 759 | 541 | 700 | 684 | 808 |
| Service Time | 2.764 | 4.357 | 2.849 | 3.272 | 2.464 |
| HCM Lane V/C Ratio | 0.461 | 0.022 | 0.13 | 0.126 | 0.15 |
| HCM Control Delay | 11.7 | 9.5 | 8.6 | 9 | 8.2 |
| HCM Lane LOS | B | A | A | A | A |
| HCM 95th-tile Q | 2.4 | 0.1 | 0.4 | 0.4 | 0.5 |

Intersection

Intersection Delay, s/veh 10.4

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | 0 | 9 | 11 | 366 | 0 | 5 | 1 | 77 | 20 | 12 |
| Traffic Vol, veh/h | 15 | 6 | 0 | 9 | 11 | 366 | 0 | 5 | 1 | 77 | 20 | 12 |
| Future Vol, veh/h | 15 | 6 | 0 | 9 | 11 | 366 | 0 | 5 | 1 | 77 | 20 | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 |
| Mvmt Flow | 16 | 7 | 0 | 10 | 12 | 398 | 0 | 5 | 1 | 84 | 22 | 13 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | WB | | | NB | | SB | | | | |
| Opposing Approach | WB | | EB | | | SB | | NB | | | | |
| Opposing Lanes | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Left | SB | | NB | | | EB | | WB | | | | |
| Conflicting Lanes Left | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Right | NB | | SB | | | WB | | EB | | | | |
| Conflicting Lanes Right | 2 | | 2 | | | 2 | | 2 | | | | |
| HCM Control Delay | 8.4 | | 10.7 | | | 8.3 | | 9.7 | | | | |
| HCM LOS | A | | B | | | A | | A | | | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 79% | 0% |
| Vol Thru, % | 100% | 62% | 0% | 100% | 0% | 3% | 21% | 0% |
| Vol Right, % | 0% | 38% | 0% | 0% | 0% | 97% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 3 | 3 | 15 | 6 | 9 | 377 | 97 | 12 |
| LT Vol | 0 | 0 | 15 | 0 | 9 | 0 | 77 | 0 |
| Through Vol | 3 | 2 | 0 | 6 | 0 | 11 | 20 | 0 |
| RT Vol | 0 | 1 | 0 | 0 | 0 | 366 | 0 | 12 |
| Lane Flow Rate | 4 | 3 | 16 | 7 | 10 | 410 | 105 | 13 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.006 | 0.004 | 0.026 | 0.009 | 0.015 | 0.479 | 0.175 | 0.017 |
| Departure Headway (Hd) | 5.631 | 5.366 | 5.693 | 5.19 | 5.394 | 4.211 | 5.973 | 4.767 |
| Convergence, Y/N | Yes |
| Cap | 634 | 665 | 629 | 690 | 666 | 856 | 600 | 749 |
| Service Time | 3.377 | 3.112 | 3.424 | 2.92 | 3.11 | 1.927 | 3.712 | 2.505 |
| HCM Lane V/C Ratio | 0.006 | 0.005 | 0.025 | 0.01 | 0.015 | 0.479 | 0.175 | 0.017 |
| HCM Control Delay | 8.4 | 8.1 | 8.6 | 8 | 8.2 | 10.8 | 10 | 7.6 |
| HCM Lane LOS | A | A | A | A | A | B | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.1 | 0 | 0 | 2.6 | 0.6 | 0.1 |

| Intersection | | | | | | |
|--------------------------|--------|--------|-------|--------|------|------|
| Int Delay, s/veh | 3.7 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | W | | T | ↑ | ↑ | |
| Traffic Vol, veh/h | 72 | 76 | 78 | 364 | 161 | 52 |
| Future Vol, veh/h | 72 | 76 | 78 | 364 | 161 | 52 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 400 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 13 | 13 | 9 | 0 | 10 |
| Mvmt Flow | 78 | 83 | 85 | 396 | 175 | 57 |
| Major/Minor | Minor2 | Major1 | | Major2 | | |
| Conflicting Flow All | 770 | 204 | 232 | 0 | - | 0 |
| Stage 1 | 204 | - | - | - | - | - |
| Stage 2 | 566 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.33 | 4.23 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.417 | 2.317 | - | - | - |
| Pot Cap-1 Maneuver | 369 | 810 | 1274 | - | - | - |
| Stage 1 | 830 | - | - | - | - | - |
| Stage 2 | 568 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 344 | 810 | 1274 | - | - | - |
| Mov Cap-2 Maneuver | 344 | - | - | - | - | - |
| Stage 1 | 774 | - | - | - | - | - |
| Stage 2 | 568 | - | - | - | - | - |
| Approach | EB | NB | | SB | | |
| HCM Control Delay, s | 16 | 1.4 | | 0 | | |
| HCM LOS | C | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR | |
| Capacity (veh/h) | 1274 | - | 488 | - | - | |
| HCM Lane V/C Ratio | 0.067 | - | 0.33 | - | - | |
| HCM Control Delay (s) | 8 | - | 16 | - | - | |
| HCM Lane LOS | A | - | C | - | - | |
| HCM 95th %tile Q(veh) | 0.2 | - | 1.4 | - | - | |

| Intersection | | | | | | | | | | | | | | | |
|--------------------------|--------|-------|--------|------|--------|------|--------|-------|------|------|------|------|--|--|--|
| Int Delay, s/veh | 1.3 | | | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | |
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | | | |
| Traffic Vol, veh/h | 9 | 69 | 6 | 28 | 378 | 15 | 7 | 3 | 21 | 6 | 1 | 1 | | | |
| Future Vol, veh/h | 9 | 69 | 6 | 28 | 378 | 15 | 7 | 3 | 21 | 6 | 1 | 1 | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | | | |
| RT Channelized | - | - | - | None | - | - | None | - | - | None | - | - | | | |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - | | | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | | | |
| Heavy Vehicles, % | 22 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Mvmt Flow | 10 | 75 | 7 | 30 | 411 | 16 | 8 | 3 | 23 | 7 | 1 | 1 | | | |
| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | | | | |
| Conflicting Flow All | 427 | 0 | 0 | 82 | 0 | 0 | 579 | 586 | 79 | 591 | 581 | 419 | | | |
| Stage 1 | - | - | - | - | - | - | 99 | 99 | - | 479 | 479 | - | | | |
| Stage 2 | - | - | - | - | - | - | 480 | 487 | - | 112 | 102 | - | | | |
| Critical Hdwy | 4.32 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | | | |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | |
| Follow-up Hdwy | 2.398 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 | | | |
| Pot Cap-1 Maneuver | 1033 | - | - | 1528 | - | - | 429 | 425 | 987 | 422 | 428 | 638 | | | |
| Stage 1 | - | - | - | - | - | - | 912 | 817 | - | 571 | 558 | - | | | |
| Stage 2 | - | - | - | - | - | - | 571 | 554 | - | 898 | 815 | - | | | |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - | | | |
| Mov Cap-1 Maneuver | 1033 | - | - | 1528 | - | - | 418 | 412 | 987 | 400 | 415 | 638 | | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 418 | 412 | - | 400 | 415 | - | | | |
| Stage 1 | - | - | - | - | - | - | 903 | 809 | - | 565 | 547 | - | | | |
| Stage 2 | - | - | - | - | - | - | 558 | 543 | - | 865 | 807 | - | | | |
| Approach | EB | | | WB | | | NB | | | SB | | | | | |
| HCM Control Delay, s | 0.9 | | | 0.5 | | | 10.5 | | | 13.7 | | | | | |
| HCM LOS | | | | | | | B | | | B | | | | | |
| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | | | | | |
| Capacity (veh/h) | 684 | 1033 | - | - | 1528 | - | - | 422 | | | | | | | |
| HCM Lane V/C Ratio | 0.049 | 0.009 | - | - | 0.02 | - | - | 0.021 | | | | | | | |
| HCM Control Delay (s) | 10.5 | 8.5 | - | - | 7.4 | - | - | 13.7 | | | | | | | |
| HCM Lane LOS | B | A | - | - | A | - | - | B | | | | | | | |
| HCM 95th %tile Q(veh) | 0.2 | 0 | - | - | 0.1 | - | - | 0.1 | | | | | | | |

| Intersection | | | | | | | | | | | | | | | | | | | |
|--------------------------|-------|--------|------|-------|--------|------|-------|--------|-------|-------|-------|-------|--|--|--|--|--|--|--|
| Int Delay, s/veh | 1 | | | | | | | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | | | | | |
| Lane Configurations | + | + | + | + | + | + | + | + | + | + | + | + | | | | | | | |
| Traffic Vol, veh/h | 10 | 100 | 0 | 0 | 292 | 1 | 0 | 0 | 0 | 4 | 0 | 32 | | | | | | | |
| Future Vol, veh/h | 10 | 100 | 0 | 0 | 292 | 1 | 0 | 0 | 0 | 4 | 0 | 32 | | | | | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | | | | | | | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | | | | | | | |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - | | | | | | | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | | | | | | | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | | | | | | |
| Mvmt Flow | 11 | 109 | 0 | 0 | 317 | 1 | 0 | 0 | 0 | 4 | 0 | 35 | | | | | | | |
| Major/Minor | | | | | | | | | | | | | | | | | | | |
| Major1 | | Major2 | | | Minor1 | | | Minor2 | | | | | | | | | | | |
| Conflicting Flow All | 318 | 0 | 0 | 109 | 0 | 0 | 466 | 449 | 109 | 449 | 449 | 318 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 131 | 131 | - | 318 | 318 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 335 | 318 | - | 131 | 131 | - | | | | | | | |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | | | | | | | |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - | | | | | | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - | | | | | | | |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | | | | | | | |
| Pot Cap-1 Maneuver | 1242 | - | - | 1481 | - | - | 507 | 505 | 945 | 520 | 505 | 723 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 873 | 788 | - | 693 | 654 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 679 | 654 | - | 873 | 788 | - | | | | | | | |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - | | | | | | | |
| Mov Cap-1 Maneuver | 1242 | - | - | 1481 | - | - | 479 | 500 | 945 | 516 | 500 | 723 | | | | | | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 479 | 500 | - | 516 | 500 | - | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 865 | 781 | - | 687 | 654 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 646 | 654 | - | 865 | 781 | - | | | | | | | |
| Approach | | | | | | | | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | | | | | | | | |
| HCM Control Delay, s | 0.7 | | 0 | | | 0 | | | 10.5 | | | | | | | | | | |
| HCM LOS | A | | | | | | B | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | | | | | | | | | | | | | | | | | | |
| Capacity (veh/h) | - | 1242 | - | - | 1481 | - | - | - | - | 692 | - | - | | | | | | | |
| HCM Lane V/C Ratio | - | 0.009 | - | - | - | - | - | - | - | 0.057 | - | - | | | | | | | |
| HCM Control Delay (s) | 0 | 7.9 | 0 | - | 0 | - | - | - | - | 10.5 | - | - | | | | | | | |
| HCM Lane LOS | A | A | A | - | A | - | - | - | - | B | - | - | | | | | | | |
| HCM 95th %tile Q(veh) | - | 0 | - | - | 0 | - | - | - | - | 0.2 | - | - | | | | | | | |

Intersection

Intersection Delay, s/veh 11.7
Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↖ | | | ↖ | | | ↖ | | | ↖ | |
| Traffic Vol, veh/h | 22 | 20 | 27 | 16 | 64 | 83 | 48 | 287 | 6 | 26 | 181 | 10 |
| Future Vol, veh/h | 22 | 20 | 27 | 16 | 64 | 83 | 48 | 287 | 6 | 26 | 181 | 10 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 24 | 22 | 29 | 17 | 70 | 90 | 52 | 312 | 7 | 28 | 197 | 11 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 9.4 | | | 10.3 | | | 13.3 | | | 10.8 | | |
| HCM LOS | A | | | B | | | B | | | B | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 14% | 32% | 10% | 12% |
| Vol Thru, % | 84% | 29% | 39% | 83% |
| Vol Right, % | 2% | 39% | 51% | 5% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 341 | 69 | 163 | 217 |
| LT Vol | 48 | 22 | 16 | 26 |
| Through Vol | 287 | 20 | 64 | 181 |
| RT Vol | 6 | 27 | 83 | 10 |
| Lane Flow Rate | 371 | 75 | 177 | 236 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.517 | 0.117 | 0.262 | 0.338 |
| Departure Headway (Hd) | 5.021 | 5.631 | 5.322 | 5.152 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 723 | 635 | 675 | 698 |
| Service Time | 3.021 | 3.676 | 3.36 | 3.184 |
| HCM Lane V/C Ratio | 0.513 | 0.118 | 0.262 | 0.338 |
| HCM Control Delay | 13.3 | 9.4 | 10.3 | 10.8 |
| HCM Lane LOS | B | A | B | B |
| HCM 95th-tile Q | 3 | 0.4 | 1 | 1.5 |

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|------|-------|-------|
| Int Delay, s/veh | 0.2 | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 0 | 45 | 117 | 10 | 4 | 0 |
| Future Vol, veh/h | 0 | 45 | 117 | 10 | 4 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | - | 0 | 0 | - | 0 | - |
| Grade, % | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 49 | 127 | 11 | 4 | 0 |
| Major/Minor | Major1 | Major2 | Minor2 | | | |
| Conflicting Flow All | 138 | 0 | - | 0 | 182 | 133 |
| Stage 1 | - | - | - | - | 133 | - |
| Stage 2 | - | - | - | - | 49 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1446 | - | - | - | 807 | 916 |
| Stage 1 | - | - | - | - | 893 | - |
| Stage 2 | - | - | - | - | 973 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1446 | - | - | - | 807 | 916 |
| Mov Cap-2 Maneuver | - | - | - | - | 807 | - |
| Stage 1 | - | - | - | - | 893 | - |
| Stage 2 | - | - | - | - | 973 | - |
| Approach | EB | WB | SB | | | |
| HCM Control Delay, s | 0 | 0 | 9.5 | | | |
| HCM LOS | | | A | | | |
| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | 1446 | - | - | - | 807 | |
| HCM Lane V/C Ratio | - | - | - | - | 0.005 | |
| HCM Control Delay (s) | 0 | - | - | - | 9.5 | |
| HCM Lane LOS | A | - | - | - | A | |
| HCM 95th %tile Q(veh) | 0 | - | - | - | 0 | |

LANE SUMMARY

 Site: St-Jean / Morris Village Access AM (short-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|-------------------------------------|--------------|------|-------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | Cap. | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV % | veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: Morris Village Access | | | | | | | | | | | | | |
| Lane 1 ^d | 165 | 3.0 | 1327 | 0.124 | 100 | 10.6 | LOS B | 0.6 | 4.9 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 43 | 3.0 | 1327 | 0.033 | 100 | 4.0 | LOS A | 0.2 | 1.2 | Short | 60 | 0.0 | NA |
| Approach | 209 | 3.0 | | 0.124 | | 9.2 | LOS A | 0.6 | 4.9 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 287 | 3.0 | 1021 | 0.281 | 100 | 5.0 | LOS A | 1.7 | 12.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 287 | 3.0 | | 0.281 | | 5.0 | LOS A | 1.7 | 12.9 | | | | |
| West: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 150 | 3.0 | 1197 | 0.125 | 100 | 3.6 | LOS A | 0.7 | 5.4 | Full | 500 | 0.0 | 0.0 |
| Approach | 150 | 3.0 | | 0.125 | | 3.6 | LOS A | 0.7 | 5.4 | | | | |
| Intersection | 646 | 3.0 | | 0.281 | | 6.0 | LOS A | 1.7 | 12.9 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Dr Corbeil AM (short-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 166 | 3.0 | 996 | 0.167 | 100 | 5.1 | LOS A | 0.9 | 7.1 | Full | 500 | 0.0 | 0.0 |
| Approach | 166 | 3.0 | | 0.167 | | 5.1 | LOS A | 0.9 | 7.1 | | | | |
| East: Dr. Corbeil | | | | | | | | | | | | | |
| Lane 1 ^d | 378 | 3.0 | 978 | 0.387 | 100 | 7.0 | LOS A | 2.6 | 20.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 378 | 3.0 | | 0.387 | | 7.0 | LOS A | 2.6 | 20.3 | | | | |
| North: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 211 | 3.0 | 989 | 0.213 | 100 | 7.8 | LOS A | 1.2 | 9.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 211 | 3.0 | | 0.213 | | 7.8 | LOS A | 1.2 | 9.6 | | | | |
| Intersection | 755 | 3.0 | | 0.387 | | 6.8 | LOS A | 2.6 | 20.3 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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| | → | ↓ | ↖ | ← | ↗ | ↑ |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 1564 | 380 | 66 | 802 | 177 | 109 |
| Future Volume (vph) | 1564 | 380 | 66 | 802 | 177 | 109 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 1845 | 1599 | 1752 | 1863 | 1805 | 1615 |
| Flt Permitted | | | 0.047 | | 0.950 | |
| Satd. Flow (perm) | 1845 | 1599 | 87 | 1863 | 1805 | 1615 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 247 | | | 96 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 3% | 1% | 3% | 2% | 0% | 0% |
| Adj. Flow (vph) | 1700 | 413 | 72 | 872 | 192 | 118 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 1700 | 413 | 72 | 872 | 192 | 118 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 85.0 | 85.0 | 11.2 | 96.2 | 23.8 | 23.8 |
| Total Split (%) | 70.8% | 70.8% | 9.3% | 80.2% | 19.8% | 19.8% |
| Maximum Green (s) | 78.8 | 78.8 | 5.0 | 90.0 | 18.6 | 18.6 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 78.9 | 78.9 | 87.7 | 87.7 | 18.6 | 18.6 |
| Actuated g/C Ratio | 0.67 | 0.67 | 0.74 | 0.74 | 0.16 | 0.16 |
| v/c Ratio | 1.38 | 0.36 | 0.53 | 0.63 | 0.67 | 0.35 |
| Control Delay | 196.2 | 4.3 | 26.4 | 9.6 | 60.2 | 16.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 196.2 | 4.3 | 26.4 | 9.6 | 60.2 | 16.2 |
| LOS | F | A | C | A | E | B |
| Approach Delay | 158.7 | | | 10.9 | 43.5 | |
| Approach LOS | F | | | B | D | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 117.8

Natural Cycle: 150

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 1.38

Intersection Signal Delay: 106.6

Intersection LOS: F

Intersection Capacity Utilization 101.6%

ICU Level of Service G

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 9 | 404 | 279 | 53 | 340 | 14 | 194 | 13 | 84 | 20 | 11 | 17 |
| Future Volume (vph) | 9 | 404 | 279 | 53 | 340 | 14 | 194 | 13 | 84 | 20 | 11 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.995 | | | 0.870 | | | 0.910 | |
| Flt Protected | | 0.999 | | | 0.993 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1898 | 1568 | 0 | 1873 | 0 | 1752 | 1653 | 0 | 1805 | 1729 | 0 |
| Flt Permitted | | 0.988 | | | 0.757 | | 0.738 | | | 0.689 | | |
| Satd. Flow (perm) | 0 | 1877 | 1568 | 0 | 1428 | 0 | 1361 | 1653 | 0 | 1309 | 1729 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 140 | | | 4 | | | 91 | | | 18 | |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 549.0 | | | 622.7 | | | 441.7 | | | 187.4 | |
| Travel Time (s) | | 39.5 | | | 44.8 | | | 31.8 | | | 13.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 3% | 0% | 0% | 7% | 3% | 0% | 0% | 0% | 0% | 0% |
| Adj. Flow (vph) | 10 | 439 | 303 | 58 | 370 | 15 | 211 | 14 | 91 | 22 | 12 | 18 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 449 | 303 | 0 | 443 | 0 | 211 | 105 | 0 | 22 | 30 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.1 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 26.0 | 26.0 | 26.0 | 10.1 | 36.1 | | 23.9 | 23.9 | | 23.9 | 23.9 | |
| Total Split (%) | 43.3% | 43.3% | 43.3% | 16.8% | 60.2% | | 39.8% | 39.8% | | 39.8% | 39.8% | |
| Maximum Green (s) | 21.0 | 21.0 | 21.0 | 5.1 | 31.1 | | 18.9 | 18.9 | | 18.9 | 18.9 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 21.0 | 21.0 | | 31.1 | | 18.9 | 18.9 | | 18.9 | 18.9 | |
| Actuated g/C Ratio | | 0.35 | 0.35 | | 0.52 | | 0.32 | 0.32 | | 0.32 | 0.32 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|------|------|-----|------|-----|------|------|-----|------|------|-----|-----|
| v/c Ratio | 0.68 | 0.47 | | 0.57 | | 0.49 | 0.18 | | 0.05 | 0.05 | | |
| Control Delay | 23.1 | 10.9 | | 12.8 | | 21.5 | 6.0 | | 14.9 | 9.5 | | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | 23.1 | 10.9 | | 12.8 | | 21.5 | 6.0 | | 14.9 | 9.5 | | |
| LOS | C | B | | B | | C | A | | B | A | | |
| Approach Delay | 18.2 | | | 12.8 | | | 16.3 | | | 11.8 | | |
| Approach LOS | B | | | B | | | B | | | B | | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.68

Intersection Signal Delay: 16.1

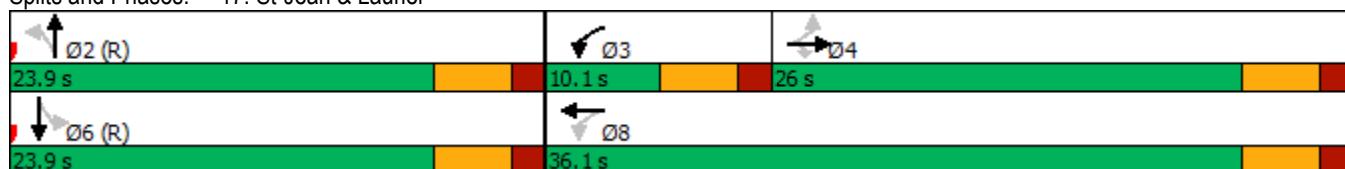
Intersection LOS: B

Intersection Capacity Utilization 73.3%

ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



Intersection

Intersection Delay, s/veh 14.4

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↖ | | | ↖ | | | ↖ | | | ↖ | |
| Traffic Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 278 | 28 | 33 | 354 | 9 |
| Future Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 278 | 28 | 33 | 354 | 9 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 6 | 3 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 0 |
| Mvmt Flow | 17 | 39 | 52 | 34 | 47 | 18 | 64 | 302 | 30 | 36 | 385 | 10 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 10.5 | | | 10.5 | | | 14.9 | | | 15.9 | | |
| HCM LOS | B | | | B | | | B | | | C | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 16% | 16% | 34% | 8% |
| Vol Thru, % | 76% | 36% | 47% | 89% |
| Vol Right, % | 8% | 48% | 19% | 2% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 365 | 100 | 91 | 396 |
| LT Vol | 59 | 16 | 31 | 33 |
| Through Vol | 278 | 36 | 43 | 354 |
| RT Vol | 28 | 48 | 17 | 9 |
| Lane Flow Rate | 397 | 109 | 99 | 430 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.57 | 0.182 | 0.17 | 0.611 |
| Departure Headway (Hd) | 5.17 | 6.041 | 6.175 | 5.112 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 698 | 591 | 579 | 706 |
| Service Time | 3.21 | 4.103 | 4.236 | 3.151 |
| HCM Lane V/C Ratio | 0.569 | 0.184 | 0.171 | 0.609 |
| HCM Control Delay | 14.9 | 10.5 | 10.5 | 15.9 |
| HCM Lane LOS | B | B | B | C |
| HCM 95th-tile Q | 3.6 | 0.7 | 0.6 | 4.2 |

Intersection

Intersection Delay, s/veh 15.4

Intersection LOS C

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|------|------|------|------|------|------|
| Lane Configurations | ↑ | | ↑ | | ↑ | ↑ |
| Traffic Vol, veh/h | 9 | 44 | 360 | 11 | 61 | 469 |
| Future Vol, veh/h | 9 | 44 | 360 | 11 | 61 | 469 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 8 | 1 |
| Mvmt Flow | 10 | 48 | 391 | 12 | 66 | 510 |
| Number of Lanes | 1 | 0 | 1 | 0 | 1 | 1 |
| Approach | WB | | NB | | SB | |
| Opposing Approach | | | SB | | NB | |
| Opposing Lanes | 0 | | 2 | | 1 | |
| Conflicting Approach Left | NB | | | WB | | |
| Conflicting Lanes Left | 1 | | 0 | | 1 | |
| Conflicting Approach Right | SB | | WB | | | |
| Conflicting Lanes Right | 2 | | 1 | | 0 | |
| HCM Control Delay | 9.2 | | 13.2 | | 17.6 | |
| HCM LOS | A | | B | | C | |

| Lane | NBLn1 | WBLn1 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 0% | 17% | 100% | 0% |
| Vol Thru, % | 97% | 0% | 0% | 100% |
| Vol Right, % | 3% | 83% | 0% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 371 | 53 | 61 | 469 |
| LT Vol | 0 | 9 | 61 | 0 |
| Through Vol | 360 | 0 | 0 | 469 |
| RT Vol | 11 | 44 | 0 | 0 |
| Lane Flow Rate | 403 | 58 | 66 | 510 |
| Geometry Grp | 5 | 2 | 7 | 7 |
| Degree of Util (X) | 0.534 | 0.089 | 0.103 | 0.704 |
| Departure Headway (Hd) | 4.767 | 5.552 | 5.597 | 4.975 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 754 | 641 | 639 | 724 |
| Service Time | 2.807 | 3.626 | 3.339 | 2.716 |
| HCM Lane V/C Ratio | 0.534 | 0.09 | 0.103 | 0.704 |
| HCM Control Delay | 13.2 | 9.2 | 9 | 18.7 |
| HCM Lane LOS | B | A | A | C |
| HCM 95th-tile Q | 3.2 | 0.3 | 0.3 | 5.8 |

Intersection

Intersection Delay, s/veh 14.9

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 60 | 214 | 83 | 124 | 111 | 17 | 82 | 15 | 227 | 10 | 10 | 37 |
| Future Vol, veh/h | 60 | 214 | 83 | 124 | 111 | 17 | 82 | 15 | 227 | 10 | 10 | 37 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 2 | 1 | 2 | 2 | 4 | 2 | 3 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 65 | 233 | 90 | 135 | 121 | 18 | 89 | 16 | 247 | 11 | 11 | 40 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | WB | | | NB | | | SB | | | |
| Opposing Lanes | 1 | | 1 | | | 1 | | | 1 | | | |
| Conflicting Approach Left | SB | | NB | | | EB | | | WB | | | |
| Conflicting Lanes Left | 1 | | 1 | | | 1 | | | 1 | | | |
| Conflicting Approach Right | NB | | SB | | | WB | | | EB | | | |
| Conflicting Lanes Right | 1 | | 1 | | | 1 | | | 1 | | | |
| HCM Control Delay | 16.4 | | 13.6 | | | 15 | | | 10 | | | |
| HCM LOS | C | | B | | | B | | | A | | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 25% | 17% | 49% | 18% |
| Vol Thru, % | 5% | 60% | 44% | 18% |
| Vol Right, % | 70% | 23% | 7% | 65% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 324 | 357 | 252 | 57 |
| LT Vol | 82 | 60 | 124 | 10 |
| Through Vol | 15 | 214 | 111 | 10 |
| RT Vol | 227 | 83 | 17 | 37 |
| Lane Flow Rate | 352 | 388 | 274 | 62 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.54 | 0.593 | 0.444 | 0.108 |
| Departure Headway (Hd) | 5.517 | 5.503 | 5.837 | 6.253 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 648 | 652 | 614 | 577 |
| Service Time | 3.592 | 3.577 | 3.918 | 4.253 |
| HCM Lane V/C Ratio | 0.543 | 0.595 | 0.446 | 0.107 |
| HCM Control Delay | 15 | 16.4 | 13.6 | 10 |
| HCM Lane LOS | B | C | B | A |
| HCM 95th-tile Q | 3.2 | 3.9 | 2.3 | 0.4 |

Intersection

Intersection Delay, s/veh 12.7

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | | ↔ | ↔ | | ↔ | ↔ | | ↔ | ↔ | |
| Traffic Vol, veh/h | 123 | 55 | 304 | 8 | 24 | 17 | 166 | 54 | 14 | 22 | 49 | 99 |
| Future Vol, veh/h | 123 | 55 | 304 | 8 | 24 | 17 | 166 | 54 | 14 | 22 | 49 | 99 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Mvmt Flow | 134 | 60 | 330 | 9 | 26 | 18 | 180 | 59 | 15 | 24 | 53 | 108 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 13.7 | | | 9.7 | | | 12.7 | | | 10.6 | | |
| HCM LOS | B | | | A | | | B | | | B | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 71% | 100% | 0% | 16% | 13% |
| Vol Thru, % | 23% | 0% | 15% | 49% | 29% |
| Vol Right, % | 6% | 0% | 85% | 35% | 58% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 234 | 123 | 359 | 49 | 170 |
| LT Vol | 166 | 123 | 0 | 8 | 22 |
| Through Vol | 54 | 0 | 55 | 24 | 49 |
| RT Vol | 14 | 0 | 304 | 17 | 99 |
| Lane Flow Rate | 254 | 134 | 390 | 53 | 185 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.406 | 0.235 | 0.567 | 0.09 | 0.28 |
| Departure Headway (Hd) | 5.742 | 6.339 | 5.233 | 6.06 | 5.458 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 626 | 567 | 691 | 590 | 658 |
| Service Time | 3.783 | 4.075 | 2.968 | 4.116 | 3.503 |
| HCM Lane V/C Ratio | 0.406 | 0.236 | 0.564 | 0.09 | 0.281 |
| HCM Control Delay | 12.7 | 11 | 14.6 | 9.7 | 10.6 |
| HCM Lane LOS | B | B | B | A | B |
| HCM 95th-tile Q | 2 | 0.9 | 3.6 | 0.3 | 1.1 |

Intersection

Intersection Delay, s/veh 11.8

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↖ ↗ | ↖ ↗ | 3 | 8 | ↖ ↗ | 226 | 0 | ↖ ↗ | 15 | 217 | ↖ ↗ | 21 |
| Traffic Vol, veh/h | 17 | 21 | 3 | 8 | 17 | 226 | 0 | 49 | 15 | 217 | 68 | 21 |
| Future Vol, veh/h | 17 | 21 | 3 | 8 | 17 | 226 | 0 | 49 | 15 | 217 | 68 | 21 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 19 |
| Mvmt Flow | 18 | 23 | 3 | 9 | 18 | 246 | 0 | 53 | 16 | 236 | 74 | 23 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | WB | | | NB | | SB | | | | |
| Opposing Approach | WB | | EB | | | SB | | NB | | | | |
| Opposing Lanes | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Left | SB | | NB | | | EB | | WB | | | | |
| Conflicting Lanes Left | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Right | NB | | SB | | | WB | | EB | | | | |
| Conflicting Lanes Right | 2 | | 2 | | | 2 | | 2 | | | | |
| HCM Control Delay | 9.1 | | 10.6 | | | 8.7 | | 13.7 | | | | |
| HCM LOS | A | | B | | | A | | B | | | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 76% | 0% |
| Vol Thru, % | 100% | 52% | 0% | 88% | 0% | 7% | 24% | 0% |
| Vol Right, % | 0% | 48% | 0% | 12% | 0% | 93% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 33 | 31 | 17 | 24 | 8 | 243 | 285 | 21 |
| LT Vol | 0 | 0 | 17 | 0 | 8 | 0 | 217 | 0 |
| Through Vol | 33 | 16 | 0 | 21 | 0 | 17 | 68 | 0 |
| RT Vol | 0 | 15 | 0 | 3 | 0 | 226 | 0 | 21 |
| Lane Flow Rate | 36 | 34 | 18 | 26 | 9 | 264 | 310 | 23 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.058 | 0.052 | 0.034 | 0.043 | 0.015 | 0.368 | 0.494 | 0.03 |
| Departure Headway (Hd) | 5.847 | 5.473 | 6.549 | 5.953 | 6.172 | 5.012 | 5.746 | 4.676 |
| Convergence, Y/N | Yes |
| Cap | 616 | 658 | 550 | 605 | 577 | 713 | 623 | 755 |
| Service Time | 3.551 | 3.177 | 4.252 | 3.657 | 3.946 | 2.785 | 3.539 | 2.468 |
| HCM Lane V/C Ratio | 0.058 | 0.052 | 0.033 | 0.043 | 0.016 | 0.37 | 0.498 | 0.03 |
| HCM Control Delay | 8.9 | 8.5 | 9.5 | 8.9 | 9 | 10.7 | 14.1 | 7.6 |
| HCM Lane LOS | A | A | A | A | A | B | B | A |
| HCM 95th-tile Q | 0.2 | 0.2 | 0.1 | 0.1 | 0 | 1.7 | 2.7 | 0.1 |

| Intersection | | | | | | |
|--------------------------|--------|--------|-------|--------|------|------|
| Int Delay, s/veh | 8.6 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | W | | T | ↑ | ↑ | |
| Traffic Vol, veh/h | 99 | 122 | 100 | 321 | 431 | 97 |
| Future Vol, veh/h | 99 | 122 | 100 | 321 | 431 | 97 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 400 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 108 | 133 | 109 | 349 | 468 | 105 |
| Major/Minor | Minor2 | Major1 | | Major2 | | |
| Conflicting Flow All | 1088 | 521 | 573 | 0 | - | 0 |
| Stage 1 | 521 | - | - | - | - | - |
| Stage 2 | 567 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 241 | 559 | 1010 | - | - | - |
| Stage 1 | 600 | - | - | - | - | - |
| Stage 2 | 572 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 215 | 559 | 1010 | - | - | - |
| Mov Cap-2 Maneuver | 215 | - | - | - | - | - |
| Stage 1 | 535 | - | - | - | - | - |
| Stage 2 | 572 | - | - | - | - | - |
| Approach | EB | NB | | SB | | |
| HCM Control Delay, s | 41.5 | 2.1 | | 0 | | |
| HCM LOS | E | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR | |
| Capacity (veh/h) | 1010 | - | 326 | - | - | |
| HCM Lane V/C Ratio | 0.108 | - | 0.737 | - | - | |
| HCM Control Delay (s) | 9 | - | 41.5 | - | - | |
| HCM Lane LOS | A | - | E | - | - | |
| HCM 95th %tile Q(veh) | 0.4 | - | 5.5 | - | - | |

| Intersection | | | | | | | | | | | | |
|--------------------------|--------|-------|--------|------|--------|------|--------|-------|------|------|------|------|
| Int Delay, s/veh | 5.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ |
| Traffic Vol, veh/h | 16 | 331 | 22 | 46 | 173 | 91 | 25 | 13 | 77 | 74 | 13 | 53 |
| Future Vol, veh/h | 16 | 331 | 22 | 46 | 173 | 91 | 25 | 13 | 77 | 74 | 13 | 53 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 17 | 360 | 24 | 50 | 188 | 99 | 27 | 14 | 84 | 80 | 14 | 58 |
| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | |
| Conflicting Flow All | 287 | 0 | 0 | 384 | 0 | 0 | 780 | 793 | 372 | 793 | 756 | 238 |
| Stage 1 | - | - | - | - | - | - | 406 | 406 | - | 338 | 338 | - |
| Stage 2 | - | - | - | - | - | - | 374 | 387 | - | 455 | 418 | - |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1287 | - | - | 1186 | - | - | 315 | 323 | 678 | 309 | 340 | 806 |
| Stage 1 | - | - | - | - | - | - | 626 | 601 | - | 681 | 644 | - |
| Stage 2 | - | - | - | - | - | - | 651 | 613 | - | 589 | 594 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1287 | - | - | 1186 | - | - | 271 | 306 | 678 | 250 | 322 | 806 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 271 | 306 | - | 250 | 322 | - |
| Stage 1 | - | - | - | - | - | - | 618 | 593 | - | 672 | 617 | - |
| Stage 2 | - | - | - | - | - | - | 566 | 587 | - | 497 | 586 | - |
| Approach | EB | | | WB | | | NB | | SB | | | |
| HCM Control Delay, s | 0.3 | | | 1.2 | | | 15.6 | | 23.1 | | | |
| HCM LOS | | | | | | | C | | C | | | |
| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | | |
| Capacity (veh/h) | 463 | 1287 | - | - | 1186 | - | - | 348 | | | | |
| HCM Lane V/C Ratio | 0.27 | 0.014 | - | - | 0.042 | - | - | 0.437 | | | | |
| HCM Control Delay (s) | 15.6 | 7.8 | - | - | 8.2 | - | - | 23.1 | | | | |
| HCM Lane LOS | C | A | - | - | A | - | - | C | | | | |
| HCM 95th %tile Q(veh) | 1.1 | 0 | - | - | 0.1 | - | - | 2.1 | | | | |

| Intersection | | | | | | | | | | | | | | | | | | | |
|--------------------------|-------|--------|------|-------|--------|------|-------|--------|-------|-------|-------|-------|--|--|--|--|--|--|--|
| Int Delay, s/veh 0.8 | | | | | | | | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | | | | | |
| Lane Configurations | + | + | + | + | + | + | + | + | + | + | + | + | | | | | | | |
| Traffic Vol, veh/h | 33 | 355 | 0 | 0 | 226 | 4 | 0 | 0 | 0 | 2 | 0 | 21 | | | | | | | |
| Future Vol, veh/h | 33 | 355 | 0 | 0 | 226 | 4 | 0 | 0 | 0 | 2 | 0 | 21 | | | | | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | | | | | | | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | | | | | | | |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - | | | | | | | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | | | | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | | | | | | | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | | | | | | |
| Mvmt Flow | 36 | 386 | 0 | 0 | 246 | 4 | 0 | 0 | 0 | 2 | 0 | 23 | | | | | | | |
| Major/Minor | | | | | | | | | | | | | | | | | | | |
| Major1 | | Major2 | | | Minor1 | | | Minor2 | | | | | | | | | | | |
| Conflicting Flow All | 250 | 0 | 0 | 386 | 0 | 0 | 718 | 708 | 386 | 706 | 706 | 248 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 458 | 458 | - | 248 | 248 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 260 | 250 | - | 458 | 458 | - | | | | | | | |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | | | | | | | |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - | | | | | | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - | | | | | | | |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | | | | | | | |
| Pot Cap-1 Maneuver | 1316 | - | - | 1172 | - | - | 344 | 360 | 662 | 351 | 361 | 791 | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 583 | 567 | - | 756 | 701 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 745 | 700 | - | 583 | 567 | - | | | | | | | |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - | | | | | | | |
| Mov Cap-1 Maneuver | 1316 | - | - | 1172 | - | - | 325 | 347 | 662 | 342 | 348 | 791 | | | | | | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 325 | 347 | - | 342 | 348 | - | | | | | | | |
| Stage 1 | - | - | - | - | - | - | 563 | 547 | - | 730 | 701 | - | | | | | | | |
| Stage 2 | - | - | - | - | - | - | 724 | 700 | - | 563 | 547 | - | | | | | | | |
| Approach | | | | | | | | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | | | | | | | | |
| HCM Control Delay, s | 0.7 | | 0 | | | 0 | | | 10.3 | | | | | | | | | | |
| HCM LOS | A | | | | | | B | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | | | | | | | | | | | | | | | | | | |
| Capacity (veh/h) | - | 1316 | - | - | 1172 | - | - | - | 710 | - | - | - | | | | | | | |
| HCM Lane V/C Ratio | - | 0.027 | - | - | - | - | - | - | 0.035 | - | - | - | | | | | | | |
| HCM Control Delay (s) | 0 | 7.8 | 0 | - | 0 | - | - | - | 10.3 | - | - | - | | | | | | | |
| HCM Lane LOS | A | A | A | - | A | - | - | - | B | - | - | - | | | | | | | |
| HCM 95th %tile Q(veh) | - | 0.1 | - | - | 0 | - | - | - | 0.1 | - | - | - | | | | | | | |

Intersection

Intersection Delay, s/veh 20.1
Intersection LOS C

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 16 | 69 | 56 | 12 | 43 | 55 | 43 | 300 | 20 | 88 | 365 | 25 |
| Future Vol, veh/h | 16 | 69 | 56 | 12 | 43 | 55 | 43 | 300 | 20 | 88 | 365 | 25 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 17 | 75 | 61 | 13 | 47 | 60 | 47 | 326 | 22 | 96 | 397 | 27 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 12.1 | | | 11.5 | | | 17.9 | | | 26.1 | | |
| HCM LOS | B | | | B | | | C | | | D | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 12% | 11% | 11% | 18% |
| Vol Thru, % | 83% | 49% | 39% | 76% |
| Vol Right, % | 6% | 40% | 50% | 5% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 363 | 141 | 110 | 478 |
| LT Vol | 43 | 16 | 12 | 88 |
| Through Vol | 300 | 69 | 43 | 365 |
| RT Vol | 20 | 56 | 55 | 25 |
| Lane Flow Rate | 395 | 153 | 120 | 520 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.628 | 0.279 | 0.219 | 0.788 |
| Departure Headway (Hd) | 5.733 | 6.543 | 6.591 | 5.57 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 635 | 550 | 545 | 655 |
| Service Time | 3.733 | 4.569 | 4.62 | 3.57 |
| HCM Lane V/C Ratio | 0.622 | 0.278 | 0.22 | 0.794 |
| HCM Control Delay | 17.9 | 12.1 | 11.5 | 26.1 |
| HCM Lane LOS | C | B | B | D |
| HCM 95th-tile Q | 4.4 | 1.1 | 0.8 | 7.7 |

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|------|-------|-------|
| Int Delay, s/veh | 0.5 | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 0 | 125 | 85 | 7 | 12 | 0 |
| Future Vol, veh/h | 0 | 125 | 85 | 7 | 12 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | - | 0 | 0 | - | 0 | - |
| Grade, % | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 136 | 92 | 8 | 13 | 0 |
| Major/Minor | Major1 | Major2 | Minor2 | | | |
| Conflicting Flow All | 100 | 0 | - | 0 | 232 | 96 |
| Stage 1 | - | - | - | - | 96 | - |
| Stage 2 | - | - | - | - | 136 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1493 | - | - | - | 756 | 960 |
| Stage 1 | - | - | - | - | 928 | - |
| Stage 2 | - | - | - | - | 890 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1493 | - | - | - | 756 | 960 |
| Mov Cap-2 Maneuver | - | - | - | - | 756 | - |
| Stage 1 | - | - | - | - | 928 | - |
| Stage 2 | - | - | - | - | 890 | - |
| Approach | EB | WB | SB | | | |
| HCM Control Delay, s | 0 | 0 | 9.8 | | | |
| HCM LOS | | | A | | | |
| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | 1493 | - | - | - | 756 | |
| HCM Lane V/C Ratio | - | - | - | - | 0.017 | |
| HCM Control Delay (s) | 0 | - | - | - | 9.8 | |
| HCM Lane LOS | A | - | - | - | A | |
| HCM 95th %tile Q(veh) | 0 | - | - | - | 0.1 | |

LANE SUMMARY

 Site: St-Jean / Morris Village Access PM (short-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|-------------------------------------|--------------|------|-------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | Cap. | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV % | veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: Morris Village Access | | | | | | | | | | | | | |
| Lane 1 ^d | 108 | 3.0 | 1114 | 0.097 | 100 | 11.6 | LOS B | 0.5 | 4.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 22 | 3.0 | 1114 | 0.020 | 100 | 4.9 | LOS A | 0.1 | 0.8 | Short | 60 | 0.0 | NA |
| Approach | 129 | 3.0 | | 0.097 | | 10.5 | LOS B | 0.5 | 4.0 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 212 | 3.0 | 1074 | 0.197 | 100 | 5.6 | LOS A | 1.1 | 8.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 212 | 3.0 | | 0.197 | | 5.6 | LOS A | 1.1 | 8.9 | | | | |
| West: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 490 | 3.0 | 1153 | 0.425 | 100 | 3.9 | LOS A | 3.2 | 25.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 490 | 3.0 | | 0.425 | | 3.9 | LOS A | 3.2 | 25.0 | | | | |
| Intersection | 832 | 3.0 | | 0.425 | | 5.4 | LOS A | 3.2 | 25.0 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Dr Corbeil PM (short-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 357 | 3.0 | 779 | 0.458 | 100 | 7.7 | LOS A | 3.0 | 23.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 357 | 3.0 | | 0.458 | | 7.7 | LOS A | 3.0 | 23.8 | | | | |
| East: Dr. Corbeil | | | | | | | | | | | | | |
| Lane 1 ^d | 277 | 3.0 | 874 | 0.317 | 100 | 7.6 | LOS A | 2.0 | 15.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 277 | 3.0 | | 0.317 | | 7.6 | LOS A | 2.0 | 15.8 | | | | |
| North: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 491 | 3.0 | 1022 | 0.481 | 100 | 8.8 | LOS A | 3.9 | 30.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 491 | 3.0 | | 0.481 | | 8.8 | LOS A | 3.9 | 30.7 | | | | |
| Intersection | 1125 | 3.0 | | 0.481 | | 8.2 | LOS A | 3.9 | 30.7 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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Appendix D-1

Forecast Medium-Term Traffic Analysis

Appendix D-2



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | WBL | WBR | NBT | NBR | SBL | SBT |
| Traffic Volume (vph) | 19 | 83 | 859 | 7 | 33 | 358 |
| Future Volume (vph) | 19 | 83 | 859 | 7 | 33 | 358 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | | 0.0 | 30.0 | |
| Storage Lanes | 1 | 0 | | 0 | 1 | |
| Taper Length (m) | 7.5 | | | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 0.891 | | 0.999 | | | |
| Flt Protected | 0.991 | | | | 0.950 | |
| Satd. Flow (prot) | 1420 | 0 | 1743 | 0 | 1530 | 1681 |
| Flt Permitted | 0.991 | | | | 0.232 | |
| Satd. Flow (perm) | 1420 | 0 | 1743 | 0 | 374 | 1681 |
| Right Turn on Red | | Yes | | Yes | | |
| Satd. Flow (RTOR) | 90 | | 1 | | | |
| Link Speed (k/h) | 50 | | 50 | | | 50 |
| Link Distance (m) | 196.2 | | 531.3 | | 401.7 | |
| Travel Time (s) | 14.1 | | 38.3 | | 28.9 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 40% | 13% | 9% | 0% | 18% | 13% |
| Adj. Flow (vph) | 21 | 90 | 934 | 8 | 36 | 389 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 111 | 0 | 942 | 0 | 36 | 389 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Right | Left | Left |
| Median Width(m) | 3.6 | | 3.6 | | | 3.6 |
| Link Offset(m) | 0.0 | | 0.0 | | | 0.0 |
| Crosswalk Width(m) | 4.8 | | 4.8 | | | 4.8 |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | | 15 | 25 | |
| Number of Detectors | 1 | | 2 | | 1 | 2 |
| Detector Template | Left | | Thru | | Left | Thru |
| Leading Detector (m) | 2.0 | | 10.0 | | 2.0 | 10.0 |
| Trailing Detector (m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | | 0.6 | | 2.0 | 0.6 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 2 Position(m) | | | 9.4 | | | 9.4 |
| Detector 2 Size(m) | | | 0.6 | | | 0.6 |
| Detector 2 Type | | | Cl+Ex | | Cl+Ex | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | 0.0 | | | 0.0 |
| Turn Type | Perm | | NA | | Perm | NA |
| Protected Phases | | | 2 | | | 6 |



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|-------------------------|-------|-----|-------|-----|-------|-------|
| Permitted Phases | 8 | | | | 6 | |
| Detector Phase | 8 | | 2 | | 6 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Minimum Split (s) | 23.0 | | 23.0 | | 23.0 | 23.0 |
| Total Split (s) | 23.0 | | 97.0 | | 97.0 | 97.0 |
| Total Split (%) | 19.2% | | 80.8% | | 80.8% | 80.8% |
| Maximum Green (s) | 18.0 | | 92.0 | | 92.0 | 92.0 |
| Yellow Time (s) | 3.5 | | 3.5 | | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | | 1.5 | | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Lead/Lag | | | | | | |
| Lead-Lag Optimize? | | | | | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | 3.0 |
| Recall Mode | None | | Min | | Min | Min |
| Walk Time (s) | 7.0 | | 7.0 | | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | | 11.0 | | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | | 0 | | 0 | 0 |
| Act Effect Green (s) | 7.5 | | 47.2 | | 47.2 | 47.2 |
| Actuated g/C Ratio | 0.12 | | 0.78 | | 0.78 | 0.78 |
| v/c Ratio | 0.44 | | 0.69 | | 0.12 | 0.30 |
| Control Delay | 16.4 | | 8.6 | | 4.1 | 3.8 |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Delay | 16.4 | | 8.6 | | 4.1 | 3.8 |
| LOS | B | | A | | A | A |
| Approach Delay | 16.4 | | 8.6 | | 3.8 | |
| Approach LOS | B | | A | | | A |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 60.6

Natural Cycle: 70

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.69

Intersection Signal Delay: 7.8

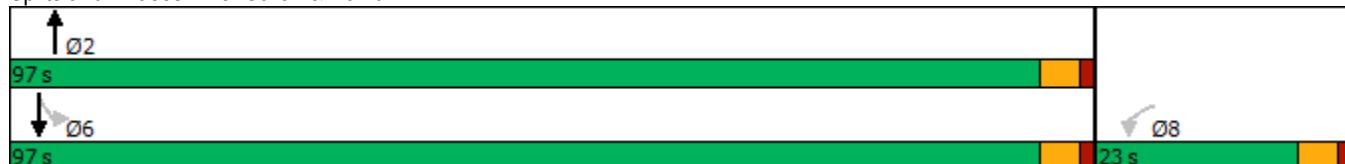
Intersection LOS: A

Intersection Capacity Utilization 60.1%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 5: Caron & David





| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↗ | ↖ | ↖ | ↘ | ↗ |
| Traffic Volume (vph) | 715 | 41 | 18 | 1986 | 120 | 10 |
| Future Volume (vph) | 715 | 41 | 18 | 1986 | 120 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 3438 | 1524 | 1703 | 3574 | 1770 | 1346 |
| Flt Permitted | | | 0.292 | | 0.950 | |
| Satd. Flow (perm) | 3438 | 1524 | 523 | 3574 | 1770 | 1346 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 45 | | | 11 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 5% | 6% | 6% | 1% | 2% | 20% |
| Adj. Flow (vph) | 777 | 45 | 20 | 2159 | 130 | 11 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 777 | 45 | 20 | 2159 | 130 | 11 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|-------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 56.0 | 56.0 | 21.0 | 77.0 | 26.0 | 26.0 |
| Total Split (%) | 54.4% | 54.4% | 20.4% | 74.8% | 25.2% | 25.2% |
| Maximum Green (s) | 49.8 | 49.8 | 14.8 | 70.8 | 20.8 | 20.8 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 59.2 | 59.2 | 63.9 | 63.9 | 21.0 | 21.0 |
| Actuated g/C Ratio | 0.61 | 0.61 | 0.66 | 0.66 | 0.22 | 0.22 |
| v/c Ratio | 0.37 | 0.05 | 0.05 | 0.91 | 0.34 | 0.04 |
| Control Delay | 10.5 | 3.2 | 5.4 | 20.7 | 37.0 | 17.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 10.5 | 3.2 | 5.4 | 20.7 | 37.0 | 17.4 |
| LOS | B | A | A | C | D | B |
| Approach Delay | 10.1 | | | 20.6 | 35.5 | |
| Approach LOS | B | | | C | D | |

Intersection Summary

Area Type: Other

Cycle Length: 103

Actuated Cycle Length: 96.4

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.91

Intersection Signal Delay: 18.5

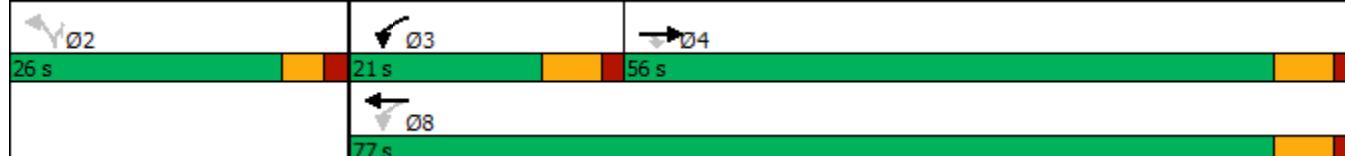
Intersection LOS: B

Intersection Capacity Utilization 71.0%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 6 | 169 | 136 | 51 | 260 | 8 | 314 | 15 | 92 | 2 | 5 | 11 |
| Future Volume (vph) | 6 | 169 | 136 | 51 | 260 | 8 | 314 | 15 | 92 | 2 | 5 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.996 | | | 0.871 | | | 0.894 | |
| Flt Protected | | 0.998 | | | 0.992 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1843 | 1568 | 0 | 1868 | 0 | 1719 | 1443 | 0 | 1805 | 1604 | 0 |
| Flt Permitted | | 0.984 | | | 0.934 | | 0.746 | | | 0.682 | | |
| Satd. Flow (perm) | 0 | 1817 | 1568 | 0 | 1759 | 0 | 1350 | 1443 | 0 | 1296 | 1604 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 148 | | | 3 | | 100 | | | 12 | | |
| Link Speed (k/h) | | 50 | | | 50 | | 50 | | | 50 | | |
| Link Distance (m) | | 549.0 | | | 622.7 | | 441.7 | | | 187.4 | | |
| Travel Time (s) | | 39.5 | | | 44.8 | | 31.8 | | | 13.5 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 3% | 3% | 3% | 0% | 0% | 5% | 13% | 15% | 0% | 20% | 0% |
| Adj. Flow (vph) | 7 | 184 | 148 | 55 | 283 | 9 | 341 | 16 | 100 | 2 | 5 | 12 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 191 | 148 | 0 | 347 | 0 | 341 | 116 | 0 | 2 | 17 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | 4.8 | | | 4.8 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 33.0 | | 27.0 | 27.0 | | 27.0 | 27.0 | |
| Total Split (%) | 38.3% | 38.3% | 38.3% | 16.7% | 55.0% | | 45.0% | 45.0% | | 45.0% | 45.0% | |
| Maximum Green (s) | 18.0 | 18.0 | 18.0 | 5.0 | 28.0 | | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 18.0 | 18.0 | | 28.0 | | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Actuated g/C Ratio | | 0.30 | 0.30 | | 0.47 | | 0.37 | 0.37 | | 0.37 | 0.37 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|------|------|-----|------|-----|------|------|-----|------|------|-----|-----|
| v/c Ratio | 0.35 | 0.26 | | 0.42 | | 0.69 | 0.20 | | 0.00 | 0.03 | | |
| Control Delay | 18.7 | 4.7 | | 12.4 | | 25.2 | 5.2 | | 12.0 | 8.3 | | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | 18.7 | 4.7 | | 12.4 | | 25.2 | 5.2 | | 12.0 | 8.3 | | |
| LOS | B | A | | B | | C | A | | B | A | | |
| Approach Delay | 12.6 | | | 12.4 | | | 20.1 | | | 8.7 | | |
| Approach LOS | B | | | B | | | C | | | A | | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.69

Intersection Signal Delay: 15.4

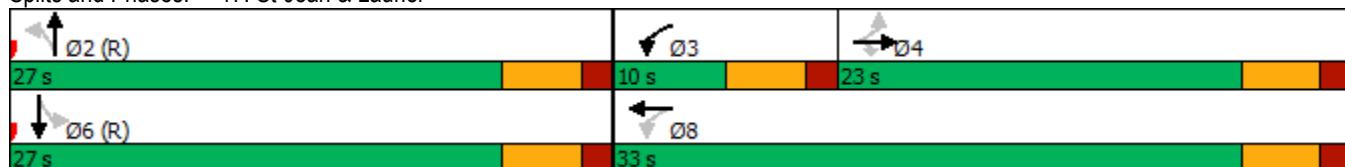
Intersection LOS: B

Intersection Capacity Utilization 62.8%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|----------------------------|--------|-------|-------|-------|--------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 80 | 80 | 88 | 858 | 323 | 54 |
| Future Volume (vph) | 80 | 80 | 88 | 858 | 323 | 54 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | 40.0 | | 0.0 | |
| Storage Lanes | 1 | 0 | 1 | | 0 | |
| Taper Length (m) | 7.5 | | 7.5 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 0.932 | | | 0.981 | | |
| Flt Protected | 0.976 | | 0.950 | | | |
| Satd. Flow (prot) | 1608 | 0 | 1597 | 1743 | 1837 | 0 |
| Flt Permitted | 0.976 | | 0.506 | | | |
| Satd. Flow (perm) | 1608 | 0 | 851 | 1743 | 1837 | 0 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | 36 | | | 21 | | |
| Link Speed (k/h) | 50 | | | 50 | 50 | |
| Link Distance (m) | 1482.6 | | | 401.7 | 1080.0 | |
| Travel Time (s) | 106.7 | | | 28.9 | 77.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 13% | 13% | 9% | 0% | 10% |
| Adj. Flow (vph) | 87 | 87 | 96 | 933 | 351 | 59 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 174 | 0 | 96 | 933 | 410 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | | 3.6 | 3.6 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 4.8 | | | 4.8 | 4.8 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | 25 | | 15 | |
| Number of Detectors | 1 | | 1 | 2 | 2 | |
| Detector Template | Left | | Left | Thru | Thru | |
| Leading Detector (m) | 2.0 | | 2.0 | 10.0 | 10.0 | |
| Trailing Detector (m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Position(m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Size(m) | 2.0 | | 2.0 | 0.6 | 0.6 | |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex | |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Queue (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Delay (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 2 Position(m) | | | | 9.4 | 9.4 | |
| Detector 2 Size(m) | | | | 0.6 | 0.6 | |
| Detector 2 Type | | | Cl+Ex | Cl+Ex | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | | 0.0 | 0.0 | |
| Turn Type | Prot | | Perm | NA | NA | |
| Protected Phases | 4 | | | 2 | 6 | |



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|-----|-------|-------|-------|-----|
| Permitted Phases | | | 2 | | | |
| Detector Phase | 4 | | 2 | 2 | 6 | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 23.0 | | 23.0 | 23.0 | 23.0 | |
| Total Split (s) | 24.0 | | 96.0 | 96.0 | 96.0 | |
| Total Split (%) | 20.0% | | 80.0% | 80.0% | 80.0% | |
| Maximum Green (s) | 19.0 | | 91.0 | 91.0 | 91.0 | |
| Yellow Time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | | 1.5 | 1.5 | 1.5 | |
| Lost Time Adjust (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.0 | | 5.0 | 5.0 | 5.0 | |
| Lead/Lag | | | | | | |
| Lead-Lag Optimize? | | | | | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | |
| Recall Mode | None | | Min | Min | Min | |
| Walk Time (s) | 7.0 | | 7.0 | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | | 11.0 | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | | 0 | 0 | 0 | |
| Act Effect Green (s) | 11.8 | | 48.0 | 48.0 | 48.0 | |
| Actuated g/C Ratio | 0.17 | | 0.68 | 0.68 | 0.68 | |
| v/c Ratio | 0.58 | | 0.17 | 0.78 | 0.33 | |
| Control Delay | 31.8 | | 5.1 | 13.8 | 5.3 | |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Delay | 31.8 | | 5.1 | 13.8 | 5.3 | |
| LOS | C | | A | B | A | |
| Approach Delay | 31.8 | | | 13.0 | 5.3 | |
| Approach LOS | C | | | B | A | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 70.3

Natural Cycle: 65

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.78

Intersection Signal Delay: 13.1

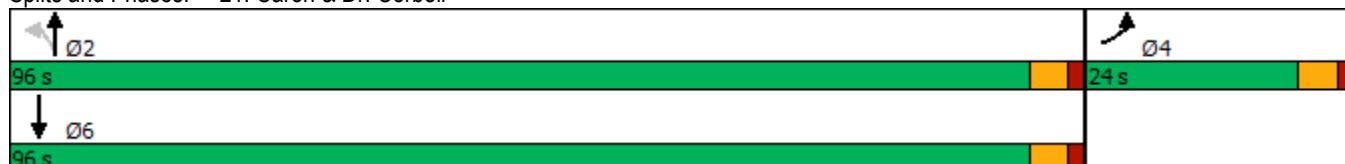
Intersection LOS: B

Intersection Capacity Utilization 62.8%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 21: Caron & Dr. Corbeil



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 69 | 38 | 83 | 37 | 119 | 165 | 158 | 631 | 12 | 53 | 295 | 30 |
| Future Volume (vph) | 69 | 38 | 83 | 37 | 119 | 165 | 158 | 631 | 12 | 53 | 295 | 30 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 35.0 | | 125.0 | 30.0 | | 120.0 | 120.0 | | 0.0 | 120.0 | | 40.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 0 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.997 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 1857 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.385 | | | 0.730 | | | 0.504 | | | 0.293 | | |
| Satd. Flow (perm) | 717 | 1863 | 1583 | 1360 | 1863 | 1583 | 939 | 1857 | 0 | 546 | 1863 | 1583 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 90 | | | 179 | | | 1 | | | 109 |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 289.2 | | | 367.4 | | | 197.4 | | | 531.3 | |
| Travel Time (s) | | 20.8 | | | 26.5 | | | 14.2 | | | 38.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 75 | 41 | 90 | 40 | 129 | 179 | 172 | 686 | 13 | 58 | 321 | 33 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 75 | 41 | 90 | 40 | 129 | 179 | 172 | 699 | 0 | 58 | 321 | 33 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 3.6 | | | 3.6 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 5 | 2 | | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | | 6 | | 6 |

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|-------|-------|-------|-------|-------|-------|-------|------|------|-------|-------|
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 10.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 10.0 | 23.0 | 23.0 |
| Total Split (s) | 11.0 | 36.0 | 36.0 | 25.0 | 25.0 | 25.0 | 12.0 | 74.0 | | 10.0 | 72.0 | 72.0 |
| Total Split (%) | 9.2% | 30.0% | 30.0% | 20.8% | 20.8% | 20.8% | 10.0% | 61.7% | | 8.3% | 60.0% | 60.0% |
| Maximum Green (s) | 6.0 | 31.0 | 31.0 | 20.0 | 20.0 | 20.0 | 7.0 | 69.0 | | 5.0 | 67.0 | 67.0 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | Lead | Lag | | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | None | Max | | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 7.0 | | | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | | 11.0 | | | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | | | 0 | 0 |
| Act Effect Green (s) | 21.5 | 21.5 | 21.5 | 13.0 | 13.0 | 13.0 | 77.0 | 71.6 | | 72.4 | 67.3 | 67.3 |
| Actuated g/C Ratio | 0.19 | 0.19 | 0.19 | 0.12 | 0.12 | 0.12 | 0.69 | 0.65 | | 0.65 | 0.61 | 0.61 |
| v/c Ratio | 0.38 | 0.11 | 0.24 | 0.25 | 0.59 | 0.52 | 0.24 | 0.58 | | 0.14 | 0.28 | 0.03 |
| Control Delay | 42.2 | 36.1 | 9.0 | 49.1 | 58.6 | 12.4 | 6.9 | 15.9 | | 7.0 | 12.3 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 42.2 | 36.1 | 9.0 | 49.1 | 58.6 | 12.4 | 6.9 | 15.9 | | 7.0 | 12.3 | 0.1 |
| LOS | D | D | A | D | E | B | A | B | | A | B | A |
| Approach Delay | | | | 26.5 | | | | | 14.1 | | | 10.6 |
| Approach LOS | | | | C | | C | | B | | | | B |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 110.9

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.59

Intersection Signal Delay: 18.4

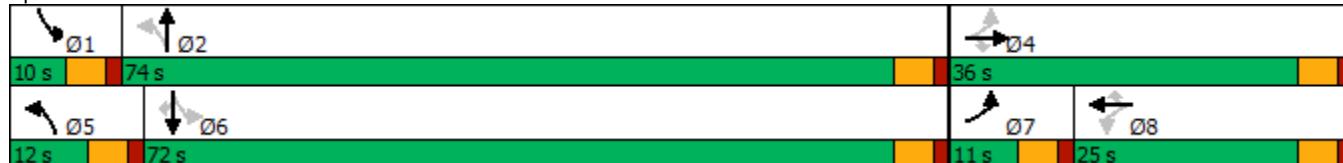
Intersection LOS: B

Intersection Capacity Utilization 61.1%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 33: Caron & Street No.1



Intersection

Intersection Delay, s/veh 13.6

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 422 | 30 | 16 | 181 | 4 |
| Future Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 422 | 30 | 16 | 181 | 4 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 6 | 0 | 14 | 6 | 0 | 5 | 3 | 10 | 0 | 1 | 25 |
| Mvmt Flow | 4 | 36 | 39 | 15 | 34 | 14 | 24 | 459 | 33 | 17 | 197 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 9.3 | | | 9.7 | | | 16.2 | | | 10 | | |
| HCM LOS | A | | | A | | | C | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 5% | 5% | 24% | 8% |
| Vol Thru, % | 89% | 45% | 53% | 90% |
| Vol Right, % | 6% | 49% | 22% | 2% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 474 | 73 | 58 | 201 |
| LT Vol | 22 | 4 | 14 | 16 |
| Through Vol | 422 | 33 | 31 | 181 |
| RT Vol | 30 | 36 | 13 | 4 |
| Lane Flow Rate | 515 | 79 | 63 | 218 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.659 | 0.121 | 0.104 | 0.296 |
| Departure Headway (Hd) | 4.603 | 5.495 | 5.963 | 4.875 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 778 | 656 | 605 | 730 |
| Service Time | 2.668 | 3.497 | 3.965 | 2.958 |
| HCM Lane V/C Ratio | 0.662 | 0.12 | 0.104 | 0.299 |
| HCM Control Delay | 16.2 | 9.3 | 9.7 | 10 |
| HCM Lane LOS | C | A | A | A |
| HCM 95th-tile Q | 5 | 0.4 | 0.3 | 1.2 |

Intersection

Intersection Delay, s/veh 8.8

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Traffic Vol, veh/h | 11 | 10 | 37 | 7 | 63 | 9 | 158 | 57 | 3 | 6 | 36 | 75 |
| Future Vol, veh/h | 11 | 10 | 37 | 7 | 63 | 9 | 158 | 57 | 3 | 6 | 36 | 75 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 22 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 33 | 0 | 4 | 0 |
| Mvmt Flow | 12 | 11 | 40 | 8 | 68 | 10 | 172 | 62 | 3 | 7 | 39 | 82 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 8.2 | | | 8.5 | | | 9.6 | | | 7.9 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 72% | 100% | 0% | 9% | 5% |
| Vol Thru, % | 26% | 0% | 21% | 80% | 31% |
| Vol Right, % | 1% | 0% | 79% | 11% | 64% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 218 | 11 | 47 | 79 | 117 |
| LT Vol | 158 | 11 | 0 | 7 | 6 |
| Through Vol | 57 | 0 | 10 | 63 | 36 |
| RT Vol | 3 | 0 | 37 | 9 | 75 |
| Lane Flow Rate | 237 | 12 | 51 | 86 | 127 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.301 | 0.021 | 0.069 | 0.116 | 0.147 |
| Departure Headway (Hd) | 4.572 | 6.297 | 4.86 | 4.861 | 4.165 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 787 | 568 | 736 | 737 | 860 |
| Service Time | 2.598 | 4.035 | 2.598 | 2.897 | 2.194 |
| HCM Lane V/C Ratio | 0.301 | 0.021 | 0.069 | 0.117 | 0.148 |
| HCM Control Delay | 9.6 | 9.2 | 8 | 8.5 | 7.9 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 1.3 | 0.1 | 0.2 | 0.4 | 0.5 |

Intersection

Intersection Delay, s/veh 8.3

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | | ↑ | ↑ | | ↔ | ↔ | | ↑ | ↑ | |
| Traffic Vol, veh/h | 15 | 8 | 0 | 15 | 19 | 204 | 0 | 5 | 0 | 27 | 20 | 12 |
| Future Vol, veh/h | 15 | 8 | 0 | 15 | 19 | 204 | 0 | 5 | 0 | 27 | 20 | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 |
| Mvmt Flow | 16 | 9 | 0 | 16 | 21 | 222 | 0 | 5 | 0 | 29 | 22 | 13 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | WB | | | NB | | SB | | | | |
| Opposing Approach | WB | | EB | | | SB | | NB | | | | |
| Opposing Lanes | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Left | SB | | NB | | | EB | | WB | | | | |
| Conflicting Lanes Left | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Right | NB | | SB | | | WB | | EB | | | | |
| Conflicting Lanes Right | 2 | | 2 | | | 2 | | 2 | | | | |
| HCM Control Delay | 8 | | 8.3 | | | 7.1 | | 8.4 | | | | |
| HCM LOS | A | | A | | | A | | A | | | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 57% | 0% |
| Vol Thru, % | 100% | 100% | 0% | 100% | 0% | 9% | 43% | 0% |
| Vol Right, % | 0% | 0% | 0% | 0% | 0% | 91% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 3 | 3 | 15 | 8 | 15 | 223 | 47 | 12 |
| LT Vol | 0 | 0 | 15 | 0 | 15 | 0 | 27 | 0 |
| Through Vol | 3 | 3 | 0 | 8 | 0 | 19 | 20 | 0 |
| RT Vol | 0 | 0 | 0 | 0 | 0 | 204 | 0 | 12 |
| Lane Flow Rate | 3 | 3 | 16 | 9 | 16 | 242 | 51 | 13 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.004 | 0.003 | 0.024 | 0.012 | 0.023 | 0.269 | 0.078 | 0.016 |
| Departure Headway (Hd) | 5.187 | 3.479 | 5.366 | 4.864 | 5.13 | 3.988 | 5.513 | 4.419 |
| Convergence, Y/N | Yes |
| Cap | 694 | 1034 | 670 | 739 | 690 | 887 | 653 | 814 |
| Service Time | 2.891 | 1.183 | 3.072 | 2.571 | 2.915 | 1.773 | 3.214 | 2.121 |
| HCM Lane V/C Ratio | 0.004 | 0.003 | 0.024 | 0.012 | 0.023 | 0.273 | 0.078 | 0.016 |
| HCM Control Delay | 7.9 | 6.2 | 8.2 | 7.6 | 8 | 8.3 | 8.7 | 7.2 |
| HCM Lane LOS | A | A | A | A | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.1 | 0 | 0.1 | 1.1 | 0.3 | 0 |

| Intersection | | | | | | | | | | | | |
|--------------------------|-------|--------|-------|------|--------|-------|------|--------|-------|------|------|------|
| Int Delay, s/veh | 2.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↖ | ↗ | | ↖ | ↗ | | ↖ | ↗ | | ↖ | ↗ | |
| Traffic Vol, veh/h | 9 | 23 | 6 | 37 | 229 | 30 | 7 | 3 | 25 | 11 | 1 | 1 |
| Future Vol, veh/h | 9 | 23 | 6 | 37 | 229 | 30 | 7 | 3 | 25 | 11 | 1 | 1 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 22 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 10 | 25 | 7 | 40 | 249 | 33 | 8 | 3 | 27 | 12 | 1 | 1 |
| Major/Minor | | | | | | | | | | | | |
| Major1 | | Major2 | | | Minor1 | | | Minor2 | | | | |
| Conflicting Flow All | 282 | 0 | 0 | 32 | 0 | 0 | 396 | 411 | 29 | 410 | 398 | 266 |
| Stage 1 | - | - | - | - | - | - | 49 | 49 | - | 346 | 346 | - |
| Stage 2 | - | - | - | - | - | - | 347 | 362 | - | 64 | 52 | - |
| Critical Hdwy | 4.32 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.398 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1174 | - | - | 1593 | - | - | 568 | 534 | 1052 | 556 | 543 | 778 |
| Stage 1 | - | - | - | - | - | - | 969 | 858 | - | 674 | 639 | - |
| Stage 2 | - | - | - | - | - | - | 673 | 629 | - | 952 | 856 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1174 | - | - | 1593 | - | - | 552 | 516 | 1052 | 525 | 525 | 778 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 552 | 516 | - | 525 | 525 | - |
| Stage 1 | - | - | - | - | - | - | 960 | 850 | - | 668 | 623 | - |
| Stage 2 | - | - | - | - | - | - | 654 | 613 | - | 916 | 848 | - |
| Approach | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | |
| HCM Control Delay, s | 1.9 | | 0.9 | | | 9.6 | | | 11.9 | | | |
| HCM LOS | A | | | | | | B | | | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | |
| Capacity (veh/h) | 828 | | 1174 | - | - | 1593 | - | - | 538 | | | |
| HCM Lane V/C Ratio | 0.046 | | 0.008 | - | - | 0.025 | - | - | 0.026 | | | |
| HCM Control Delay (s) | 9.6 | | 8.1 | - | - | 7.3 | - | - | 11.9 | | | |
| HCM Lane LOS | A | | A | - | - | A | - | - | B | | | |
| HCM 95th %tile Q(veh) | 0.1 | | 0 | - | - | 0.1 | - | - | 0.1 | | | |

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|------|-------|-------|
| Int Delay, s/veh | 1.6 | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 18 | 126 | 336 | 51 | 17 | 53 |
| Future Vol, veh/h | 18 | 126 | 336 | 51 | 17 | 53 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | - | 0 | 0 | - | 0 | - |
| Grade, % | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 137 | 365 | 55 | 18 | 58 |
| Major/Minor | Major1 | Major2 | Minor2 | | | |
| Conflicting Flow All | 420 | 0 | - | 0 | 570 | 393 |
| Stage 1 | - | - | - | - | 393 | - |
| Stage 2 | - | - | - | - | 177 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1139 | - | - | - | 483 | 656 |
| Stage 1 | - | - | - | - | 682 | - |
| Stage 2 | - | - | - | - | 854 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1139 | - | - | - | 474 | 656 |
| Mov Cap-2 Maneuver | - | - | - | - | 474 | - |
| Stage 1 | - | - | - | - | 669 | - |
| Stage 2 | - | - | - | - | 854 | - |
| Approach | EB | WB | SB | | | |
| HCM Control Delay, s | 1 | 0 | 11.9 | | | |
| HCM LOS | | | B | | | |
| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | 1139 | - | - | - | 600 | |
| HCM Lane V/C Ratio | 0.017 | - | - | - | 0.127 | |
| HCM Control Delay (s) | 8.2 | 0 | - | - | 11.9 | |
| HCM Lane LOS | A | A | - | - | B | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | - | 0.4 | |

LANE SUMMARY

Site: Poupart / Site Access AM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 66 | 3.0 | 796 | 0.083 | 100 | 10.2 | LOS B | 0.4 | 3.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 66 | 3.0 | | 0.083 | | 10.2 | LOS B | 0.4 | 3.2 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 835 | 3.0 | 1005 | 0.831 | 100 | 7.1 | LOS A | 13.0 | 101.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 835 | 3.0 | | 0.831 | | 7.1 | LOS A | 13.0 | 101.0 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 167 | 3.0 | 367 | 0.457 | 100 | 16.9 | LOS B | 3.3 | 26.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 167 | 3.0 | | 0.457 | | 16.9 | LOS B | 3.3 | 26.0 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 329 | 3.0 | 1084 | 0.304 | 100 | 5.3 | LOS A | 2.2 | 17.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 329 | 3.0 | | 0.304 | | 5.3 | LOS A | 2.2 | 17.3 | | | | |
| Intersection | 1398 | 3.0 | | 0.831 | | 8.0 | LOS A | 13.0 | 101.0 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: Poupart Extension AM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| East: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 1009 | 3.0 | 1102 | 0.915 | 100 | 5.7 | LOS A | 33.5 | 260.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 1009 | 3.0 | | 0.915 | | 5.7 | LOS A | 33.5 | 260.9 | | | | |
| North: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 108 | 3.0 | 422 | 0.255 | 100 | 15.7 | LOS B | 1.6 | 12.4 | Full | 500 | 0.0 | 0.0 |
| Approach | 108 | 3.0 | | 0.255 | | 15.7 | LOS B | 1.6 | 12.4 | | | | |
| West: Poupart Extension | | | | | | | | | | | | | |
| Lane 1 ^d | 266 | 3.0 | 1004 | 0.265 | 100 | 5.5 | LOS A | 1.8 | 13.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 266 | 3.0 | | 0.265 | | 5.5 | LOS A | 1.8 | 13.8 | | | | |
| Intersection | 1383 | 3.0 | | 0.915 | | 6.4 | LOS A | 33.5 | 260.9 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Dr Corbeil AM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 286 | 3.0 | 995 | 0.287 | 100 | 5.2 | LOS A | 1.8 | 13.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 286 | 3.0 | | 0.287 | | 5.2 | LOS A | 1.8 | 13.8 | | | | |
| East: Dr. Corbeil | | | | | | | | | | | | | |
| Lane 1 ^d | 385 | 3.0 | 875 | 0.440 | 100 | 8.1 | LOS A | 3.0 | 23.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 385 | 3.0 | | 0.440 | | 8.1 | LOS A | 3.0 | 23.2 | | | | |
| North: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 246 | 3.0 | 978 | 0.251 | 100 | 7.5 | LOS A | 1.5 | 12.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 246 | 3.0 | | 0.251 | | 7.5 | LOS A | 1.5 | 12.0 | | | | |
| Intersection | 916 | 3.0 | | 0.440 | | 7.1 | LOS A | 3.0 | 23.2 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Morris Village Access AM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|-------------------------------------|--------------|------|-------|-----------|------------|---------------|------------------|-----------------------|--------------|-------------|---------------|-------------|----------------|
| | Demand Flows | | Cap. | Deg. Satn | Lane Util. | Average Delay | Level of Service | 95% Back of Queue Veh | Queue Dist m | Lane Config | Lane Length m | Cap. Adj. % | Prob. Block. % |
| | Total veh/h | HV % | veh/h | v/c | % | sec | | | m | | | | |
| South: Morris Village Access | | | | | | | | | | | | | |
| Lane 1 ^d | 526 | 3.0 | 1259 | 0.418 | 100 | 11.2 | LOS B | 2.9 | 22.7 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 102 | 3.0 | 1259 | 0.081 | 100 | 4.3 | LOS A | 0.4 | 3.2 | Short | 60 | 0.0 | NA |
| Approach | 628 | 3.0 | | 0.418 | | 10.1 | LOS B | 2.9 | 22.7 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 327 | 3.0 | 716 | 0.457 | 100 | 9.4 | LOS A | 3.2 | 25.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 327 | 3.0 | | 0.457 | | 9.4 | LOS A | 3.2 | 25.3 | | | | |
| West: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 330 | 3.0 | 1159 | 0.285 | 100 | 3.8 | LOS A | 2.0 | 15.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 330 | 3.0 | | 0.285 | | 3.8 | LOS A | 2.0 | 15.7 | | | | |
| Intersection | 1286 | 3.0 | | 0.457 | | 8.3 | LOS A | 3.2 | 25.3 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: St-Jean / Poupart AM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 299 | 3.0 | 837 | 0.357 | 100 | 9.4 | LOS A | 2.3 | 17.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 299 | 3.0 | | 0.357 | | 9.4 | LOS A | 2.3 | 17.9 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 816 | 3.0 | 874 | 0.935 | 100 | 23.3 | LOS C | 24.6 | 191.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 816 | 3.0 | | 0.935 | | 23.3 | LOS C | 24.6 | 191.9 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 249 | 3.0 | 314 | 0.794 | 100 | 38.6 | LOS D | 8.6 | 67.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 249 | 3.0 | | 0.794 | | 38.6 | LOS D | 8.6 | 67.3 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 300 | 3.0 | 722 | 0.415 | 100 | 8.7 | LOS A | 2.8 | 21.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 300 | 3.0 | | 0.415 | | 8.7 | LOS A | 2.8 | 21.6 | | | | |
| Intersection | 1664 | 3.0 | | 0.935 | | 20.4 | LOS C | 24.6 | 191.9 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 13 | 66 | 669 | 19 | 96 | 970 |
| Future Volume (vph) | 13 | 66 | 669 | 19 | 96 | 970 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | | 0.0 | 30.0 | |
| Storage Lanes | 1 | 0 | | 0 | 1 | |
| Taper Length (m) | 7.5 | | | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 0.887 | | 0.996 | | | |
| Flt Protected | 0.992 | | | | 0.950 | |
| Satd. Flow (prot) | 1672 | 0 | 1874 | 0 | 1671 | 1881 |
| Flt Permitted | 0.992 | | | | 0.335 | |
| Satd. Flow (perm) | 1672 | 0 | 1874 | 0 | 589 | 1881 |
| Right Turn on Red | | Yes | | Yes | | |
| Satd. Flow (RTOR) | 72 | | 4 | | | |
| Link Speed (k/h) | 50 | | 50 | | | 50 |
| Link Distance (m) | 196.2 | | 558.9 | | 401.7 | |
| Travel Time (s) | 14.1 | | 40.2 | | 28.9 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 8% | 1% |
| Adj. Flow (vph) | 14 | 72 | 727 | 21 | 104 | 1054 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 86 | 0 | 748 | 0 | 104 | 1054 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Right | Left | Left |
| Median Width(m) | 3.6 | | 3.6 | | | 3.6 |
| Link Offset(m) | 0.0 | | 0.0 | | | 0.0 |
| Crosswalk Width(m) | 4.8 | | 4.8 | | | 4.8 |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | | 15 | 25 | |
| Number of Detectors | 1 | | 2 | | 1 | 2 |
| Detector Template | Left | | Thru | | Left | Thru |
| Leading Detector (m) | 2.0 | | 10.0 | | 2.0 | 10.0 |
| Trailing Detector (m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | | 0.6 | | 2.0 | 0.6 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 2 Position(m) | | | 9.4 | | | 9.4 |
| Detector 2 Size(m) | | | 0.6 | | | 0.6 |
| Detector 2 Type | | | Cl+Ex | | Cl+Ex | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | 0.0 | | | 0.0 |
| Turn Type | Perm | | NA | | Perm | NA |
| Protected Phases | | | 2 | | | 6 |



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|-------------------------|-------|-----|-------|-----|-------|-------|
| Permitted Phases | 8 | | | | 6 | |
| Detector Phase | 8 | | 2 | | 6 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Minimum Split (s) | 23.0 | | 23.0 | | 23.0 | 23.0 |
| Total Split (s) | 23.0 | | 97.0 | | 97.0 | 97.0 |
| Total Split (%) | 19.2% | | 80.8% | | 80.8% | 80.8% |
| Maximum Green (s) | 18.0 | | 92.0 | | 92.0 | 92.0 |
| Yellow Time (s) | 3.5 | | 3.5 | | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | | 1.5 | | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Lead/Lag | | | | | | |
| Lead-Lag Optimize? | | | | | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | 3.0 |
| Recall Mode | None | | Min | | Min | Min |
| Walk Time (s) | 7.0 | | 7.0 | | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | | 11.0 | | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | | 0 | | 0 | 0 |
| Act Effect Green (s) | 7.3 | | 49.4 | | 49.4 | 49.4 |
| Actuated g/C Ratio | 0.12 | | 0.80 | | 0.80 | 0.80 |
| v/c Ratio | 0.33 | | 0.50 | | 0.22 | 0.70 |
| Control Delay | 15.4 | | 4.7 | | 4.1 | 7.9 |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Delay | 15.4 | | 4.7 | | 4.1 | 7.9 |
| LOS | B | | A | | A | A |
| Approach Delay | 15.4 | | 4.7 | | 7.6 | |
| Approach LOS | B | | A | | | A |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 62

Natural Cycle: 70

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.70

Intersection Signal Delay: 6.8

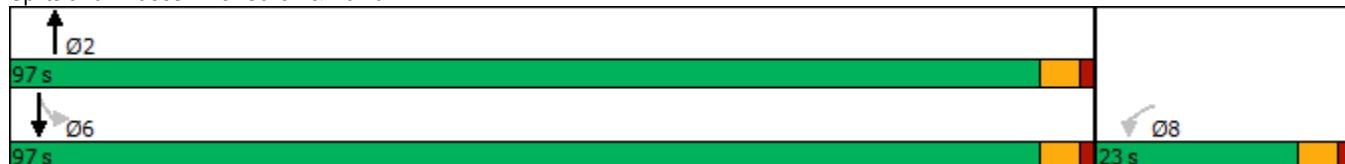
Intersection LOS: A

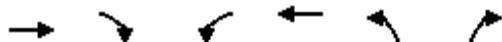
Intersection Capacity Utilization 64.2%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 5: Caron & David





| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 2066 | 208 | 66 | 1103 | 73 | 109 |
| Future Volume (vph) | 2066 | 208 | 66 | 1103 | 73 | 109 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 3505 | 1599 | 1752 | 3539 | 1805 | 1615 |
| Flt Permitted | | | 0.053 | | 0.950 | |
| Satd. Flow (perm) | 3505 | 1599 | 98 | 3539 | 1805 | 1615 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 194 | | | 81 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 3% | 1% | 3% | 2% | 0% | 0% |
| Adj. Flow (vph) | 2246 | 226 | 72 | 1199 | 79 | 118 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 2246 | 226 | 72 | 1199 | 79 | 118 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|-------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 75.0 | 75.0 | 11.2 | 86.2 | 23.8 | 23.8 |
| Total Split (%) | 68.2% | 68.2% | 10.2% | 78.4% | 21.6% | 21.6% |
| Maximum Green (s) | 68.8 | 68.8 | 5.0 | 80.0 | 18.6 | 18.6 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 69.0 | 69.0 | 77.7 | 77.7 | 18.6 | 18.6 |
| Actuated g/C Ratio | 0.64 | 0.64 | 0.72 | 0.72 | 0.17 | 0.17 |
| v/c Ratio | 1.00 | 0.21 | 0.49 | 0.47 | 0.25 | 0.34 |
| Control Delay | 40.3 | 2.3 | 20.4 | 7.0 | 42.1 | 18.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.3 | 2.3 | 20.4 | 7.0 | 42.1 | 18.3 |
| LOS | D | A | C | A | D | B |
| Approach Delay | 36.8 | | | 7.8 | 27.9 | |
| Approach LOS | D | | | A | C | |

Intersection Summary

Area Type: Other

Cycle Length: 110

Actuated Cycle Length: 107.8

Natural Cycle: 110

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 1.00

Intersection Signal Delay: 27.0

Intersection LOS: C

Intersection Capacity Utilization 73.4%

ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 9 | 405 | 345 | 89 | 340 | 14 | 227 | 13 | 106 | 20 | 11 | 17 |
| Future Volume (vph) | 9 | 405 | 345 | 89 | 340 | 14 | 227 | 13 | 106 | 20 | 11 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.996 | | | 0.866 | | | 0.910 | |
| Flt Protected | | 0.999 | | | 0.990 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1898 | 1568 | 0 | 1869 | 0 | 1752 | 1645 | 0 | 1805 | 1729 | 0 |
| Flt Permitted | | 0.987 | | | 0.582 | | 0.738 | | | 0.674 | | |
| Satd. Flow (perm) | 0 | 1875 | 1568 | 0 | 1099 | 0 | 1361 | 1645 | 0 | 1281 | 1729 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 173 | | | 4 | | | 115 | | | 18 | |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 549.0 | | | 622.7 | | | 441.7 | | | 187.4 | |
| Travel Time (s) | | 39.5 | | | 44.8 | | | 31.8 | | | 13.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 3% | 0% | 0% | 7% | 3% | 0% | 0% | 0% | 0% | 0% |
| Adj. Flow (vph) | 10 | 440 | 375 | 97 | 370 | 15 | 247 | 14 | 115 | 22 | 12 | 18 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 450 | 375 | 0 | 482 | 0 | 247 | 129 | 0 | 22 | 30 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.1 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 25.9 | 25.9 | 25.9 | 10.1 | 36.0 | | 24.0 | 24.0 | | 24.0 | 24.0 | |
| Total Split (%) | 43.2% | 43.2% | 43.2% | 16.8% | 60.0% | | 40.0% | 40.0% | | 40.0% | 40.0% | |
| Maximum Green (s) | 20.9 | 20.9 | 20.9 | 5.1 | 31.0 | | 19.0 | 19.0 | | 19.0 | 19.0 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 20.9 | 20.9 | | 31.0 | | 19.0 | 19.0 | | 19.0 | 19.0 | |
| Actuated g/C Ratio | | 0.35 | 0.35 | | 0.52 | | 0.32 | 0.32 | | 0.32 | 0.32 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|------|------|-----|------|-----|------|------|-----|------|------|-----|-----|
| v/c Ratio | 0.69 | 0.57 | | 0.76 | | 0.57 | 0.22 | | 0.05 | 0.05 | | |
| Control Delay | 23.4 | 12.3 | | 20.5 | | 23.5 | 5.5 | | 14.8 | 9.5 | | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | 23.4 | 12.3 | | 20.5 | | 23.5 | 5.5 | | 14.8 | 9.5 | | |
| LOS | C | B | | C | | C | A | | B | A | | |
| Approach Delay | 18.4 | | | 20.5 | | | 17.3 | | | 11.7 | | |
| Approach LOS | B | | | C | | | B | | | B | | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.76

Intersection Signal Delay: 18.5

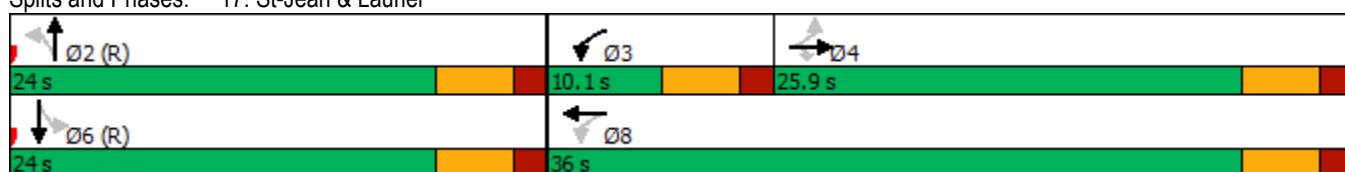
Intersection LOS: B

Intersection Capacity Utilization 77.2%

ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|----------------------------|--------|-------|-------|-------|--------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 104 | 131 | 106 | 646 | 958 | 105 |
| Future Volume (vph) | 104 | 131 | 106 | 646 | 958 | 105 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | 40.0 | | 0.0 | |
| Storage Lanes | 1 | 0 | 1 | | 0 | |
| Taper Length (m) | 7.5 | | 7.5 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 0.925 | | | 0.987 | | |
| Flt Protected | 0.978 | | 0.950 | | | |
| Satd. Flow (prot) | 1719 | 0 | 1805 | 1900 | 1875 | 0 |
| Flt Permitted | 0.978 | | 0.053 | | | |
| Satd. Flow (perm) | 1719 | 0 | 101 | 1900 | 1875 | 0 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | 44 | | | 10 | | |
| Link Speed (k/h) | 50 | | | 50 | 50 | |
| Link Distance (m) | 1482.6 | | | 401.7 | 1080.0 | |
| Travel Time (s) | 106.7 | | | 28.9 | 77.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 0% |
| Adj. Flow (vph) | 113 | 142 | 115 | 702 | 1041 | 114 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 255 | 0 | 115 | 702 | 1155 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | | 3.6 | 3.6 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 4.8 | | | 4.8 | 4.8 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | 25 | | 15 | |
| Number of Detectors | 1 | | 1 | 2 | 2 | |
| Detector Template | Left | | Left | Thru | Thru | |
| Leading Detector (m) | 2.0 | | 2.0 | 10.0 | 10.0 | |
| Trailing Detector (m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Position(m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Size(m) | 2.0 | | 2.0 | 0.6 | 0.6 | |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex | |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Queue (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Delay (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 2 Position(m) | | | | 9.4 | 9.4 | |
| Detector 2 Size(m) | | | | 0.6 | 0.6 | |
| Detector 2 Type | | | Cl+Ex | Cl+Ex | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | | 0.0 | 0.0 | |
| Turn Type | Perm | pm+pt | | NA | NA | |
| Protected Phases | | | 5 | 2 | 6 | |



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|------|------|-------|-------|-----|
| Permitted Phases | 4 | | 2 | | | |
| Detector Phase | 4 | | 5 | 2 | 6 | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | 5.0 | | |
| Minimum Split (s) | 23.0 | | 10.0 | 23.0 | 23.0 | |
| Total Split (s) | 23.0 | | 11.2 | 97.0 | 85.8 | |
| Total Split (%) | 19.2% | | 9.3% | 80.8% | 71.5% | |
| Maximum Green (s) | 18.0 | | 6.2 | 92.0 | 80.8 | |
| Yellow Time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | | 1.5 | 1.5 | 1.5 | |
| Lost Time Adjust (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.0 | | 5.0 | 5.0 | 5.0 | |
| Lead/Lag | | Lead | | Lag | | |
| Lead-Lag Optimize? | | Yes | | Yes | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | | |
| Recall Mode | None | | None | Min | Min | |
| Walk Time (s) | 7.0 | | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | | | 0 | 0 | |
| Act Effect Green (s) | 16.7 | | 82.1 | 82.1 | 70.6 | |
| Actuated g/C Ratio | 0.15 | | 0.75 | 0.75 | 0.65 | |
| v/c Ratio | 0.85 | | 0.66 | 0.49 | 0.95 | |
| Control Delay | 64.4 | | 35.7 | 6.6 | 34.1 | |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Delay | 64.4 | | 35.7 | 6.6 | 34.1 | |
| LOS | E | | D | A | C | |
| Approach Delay | 64.4 | | | 10.7 | 34.1 | |
| Approach LOS | E | | | B | C | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 109.1

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.95

Intersection Signal Delay: 29.0 Intersection LOS: C

Intersection Capacity Utilization 89.0% ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 21: Caron & Dr. Corbeil



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 49 | 126 | 180 | 24 | 78 | 109 | 136 | 531 | 39 | 174 | 731 | 77 |
| Future Volume (vph) | 49 | 126 | 180 | 24 | 78 | 109 | 136 | 531 | 39 | 174 | 731 | 77 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 35.0 | | 125.0 | 30.0 | | 120.0 | 120.0 | | 0.0 | 120.0 | | 40.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 0 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.990 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 1844 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.460 | | | 0.669 | | | 0.161 | | | 0.253 | | |
| Satd. Flow (perm) | 857 | 1863 | 1583 | 1246 | 1863 | 1583 | 300 | 1844 | 0 | 471 | 1863 | 1583 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 196 | | | 145 | | | 5 | | | 145 |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 179.3 | | | 276.0 | | | 177.7 | | | 558.9 | |
| Travel Time (s) | | 12.9 | | | 19.9 | | | 12.8 | | | 40.2 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 53 | 137 | 196 | 26 | 85 | 118 | 148 | 577 | 42 | 189 | 795 | 84 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 53 | 137 | 196 | 26 | 85 | 118 | 148 | 619 | 0 | 189 | 795 | 84 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 3.6 | | | 3.6 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 5 | 2 | | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | | 6 | | 6 |

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-------|-------|-------|
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 10.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 10.0 | 23.0 | 23.0 |
| Total Split (s) | 10.0 | 33.0 | 33.0 | 23.0 | 23.0 | 23.0 | 10.0 | 45.0 | | 12.0 | 47.0 | 47.0 |
| Total Split (%) | 11.1% | 36.7% | 36.7% | 25.6% | 25.6% | 25.6% | 11.1% | 50.0% | | 13.3% | 52.2% | 52.2% |
| Maximum Green (s) | 5.0 | 28.0 | 28.0 | 18.0 | 18.0 | 18.0 | 5.0 | 40.0 | | 7.0 | 42.0 | 42.0 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | Lead | Lag | | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Max | | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 15.1 | 15.1 | 15.1 | 9.5 | 9.5 | 9.5 | 45.5 | 40.4 | | 49.1 | 42.3 | 42.3 |
| Actuated g/C Ratio | 0.19 | 0.19 | 0.19 | 0.12 | 0.12 | 0.12 | 0.59 | 0.52 | | 0.63 | 0.55 | 0.55 |
| v/c Ratio | 0.23 | 0.38 | 0.42 | 0.17 | 0.37 | 0.37 | 0.55 | 0.64 | | 0.46 | 0.78 | 0.09 |
| Control Delay | 27.1 | 29.3 | 7.0 | 34.8 | 37.5 | 7.4 | 14.9 | 18.6 | | 9.6 | 22.8 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.1 | 29.3 | 7.0 | 34.8 | 37.5 | 7.4 | 14.9 | 18.6 | | 9.6 | 22.8 | 0.6 |
| LOS | C | C | A | C | D | A | B | B | | A | C | A |
| Approach Delay | | 17.7 | | | 21.7 | | | 17.9 | | | 18.7 | |
| Approach LOS | | B | | | C | | | B | | | B | |

Intersection Summary

Area Type: Other

Cycle Length: 90

Actuated Cycle Length: 77.5

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.78

Intersection Signal Delay: 18.6

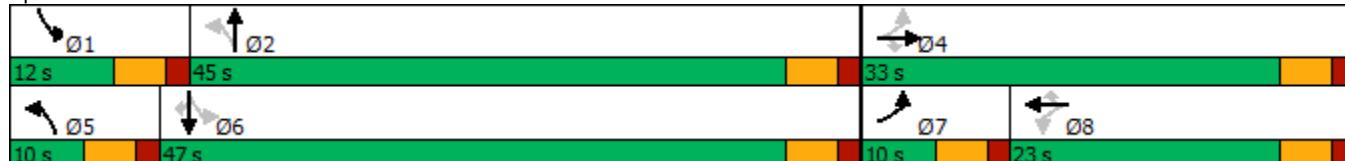
Intersection LOS: B

Intersection Capacity Utilization 73.5%

ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 33: Caron & Street No.1



Intersection

Intersection Delay, s/veh 20.9

Intersection LOS C

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 334 | 28 | 33 | 457 | 9 |
| Future Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 334 | 28 | 33 | 457 | 9 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 6 | 3 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 0 |
| Mvmt Flow | 17 | 39 | 52 | 34 | 47 | 18 | 64 | 363 | 30 | 36 | 497 | 10 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | EB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 11.3 | | | 11.3 | | | 19.6 | | | 25.7 | | |
| HCM LOS | B | | | B | | | C | | | D | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 14% | 16% | 34% | 7% |
| Vol Thru, % | 79% | 36% | 47% | 92% |
| Vol Right, % | 7% | 48% | 19% | 2% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 421 | 100 | 91 | 499 |
| LT Vol | 59 | 16 | 31 | 33 |
| Through Vol | 334 | 36 | 43 | 457 |
| RT Vol | 28 | 48 | 17 | 9 |
| Lane Flow Rate | 458 | 109 | 99 | 542 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.687 | 0.198 | 0.184 | 0.795 |
| Departure Headway (Hd) | 5.403 | 6.543 | 6.681 | 5.275 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 664 | 543 | 532 | 683 |
| Service Time | 3.468 | 4.638 | 4.779 | 3.337 |
| HCM Lane V/C Ratio | 0.69 | 0.201 | 0.186 | 0.794 |
| HCM Control Delay | 19.6 | 11.3 | 11.3 | 25.7 |
| HCM Lane LOS | C | B | B | D |
| HCM 95th-tile Q | 5.4 | 0.7 | 0.7 | 8 |

Intersection

Intersection Delay, s/veh 10.2

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ |
| Traffic Vol, veh/h | 123 | 55 | 173 | 9 | 24 | 17 | 86 | 68 | 14 | 22 | 71 | 99 |
| Future Vol, veh/h | 123 | 55 | 173 | 9 | 24 | 17 | 86 | 68 | 14 | 22 | 71 | 99 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Mvmt Flow | 134 | 60 | 188 | 10 | 26 | 18 | 93 | 74 | 15 | 24 | 77 | 108 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 10.5 | | | 9.1 | | | 10.3 | | | 10 | | |
| HCM LOS | B | | | A | | | B | | | A | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 51% | 100% | 0% | 18% | 11% |
| Vol Thru, % | 40% | 0% | 24% | 48% | 37% |
| Vol Right, % | 8% | 0% | 76% | 34% | 52% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 168 | 123 | 228 | 50 | 192 |
| LT Vol | 86 | 123 | 0 | 9 | 22 |
| Through Vol | 68 | 0 | 55 | 24 | 71 |
| RT Vol | 14 | 0 | 173 | 17 | 99 |
| Lane Flow Rate | 183 | 134 | 248 | 54 | 209 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.267 | 0.224 | 0.343 | 0.085 | 0.284 |
| Departure Headway (Hd) | 5.264 | 6.023 | 4.982 | 5.614 | 4.905 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 674 | 590 | 714 | 642 | 724 |
| Service Time | 3.362 | 3.82 | 2.778 | 3.614 | 3 |
| HCM Lane V/C Ratio | 0.272 | 0.227 | 0.347 | 0.084 | 0.289 |
| HCM Control Delay | 10.3 | 10.6 | 10.4 | 9.1 | 10 |
| HCM Lane LOS | B | B | B | A | A |
| HCM 95th-tile Q | 1.1 | 0.9 | 1.5 | 0.3 | 1.2 |

Intersection

Intersection Delay, s/veh 8.5

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | 3 | 12 | 22 | 122 | 0 | 49 | 22 | 45 | 68 | 21 |
| Traffic Vol, veh/h | 17 | 31 | 3 | 12 | 22 | 122 | 0 | 49 | 22 | 45 | 68 | 21 |
| Future Vol, veh/h | 17 | 31 | 3 | 12 | 22 | 122 | 0 | 49 | 22 | 45 | 68 | 21 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 19 |
| Mvmt Flow | 18 | 34 | 3 | 13 | 24 | 133 | 0 | 53 | 24 | 49 | 74 | 23 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 2 | | | 2 | | | 2 | | | 2 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 2 | | | 2 | | | 2 | | | 2 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 2 | | | 2 | | | 2 | | | 2 | | |
| HCM Control Delay | 8.3 | | | 8.4 | | | 8 | | | 8.9 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 40% | 0% |
| Vol Thru, % | 100% | 43% | 0% | 91% | 0% | 15% | 60% | 0% |
| Vol Right, % | 0% | 57% | 0% | 9% | 0% | 85% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 33 | 38 | 17 | 34 | 12 | 144 | 113 | 21 |
| LT Vol | 0 | 0 | 17 | 0 | 12 | 0 | 45 | 0 |
| Through Vol | 33 | 16 | 0 | 31 | 0 | 22 | 68 | 0 |
| RT Vol | 0 | 22 | 0 | 3 | 0 | 122 | 0 | 21 |
| Lane Flow Rate | 36 | 42 | 18 | 37 | 13 | 157 | 123 | 23 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.051 | 0.055 | 0.029 | 0.053 | 0.02 | 0.197 | 0.181 | 0.028 |
| Departure Headway (Hd) | 5.218 | 4.78 | 5.724 | 5.159 | 5.626 | 4.528 | 5.309 | 4.423 |
| Convergence, Y/N | Yes |
| Cap | 686 | 749 | 626 | 694 | 637 | 794 | 676 | 809 |
| Service Time | 2.95 | 2.512 | 3.452 | 2.887 | 3.349 | 2.251 | 3.039 | 2.153 |
| HCM Lane V/C Ratio | 0.052 | 0.056 | 0.029 | 0.053 | 0.02 | 0.198 | 0.182 | 0.028 |
| HCM Control Delay | 8.2 | 7.8 | 8.6 | 8.2 | 8.5 | 8.4 | 9.2 | 7.3 |
| HCM Lane LOS | A | A | A | A | A | A | A | A |
| HCM 95th-tile Q | 0.2 | 0.2 | 0.1 | 0.2 | 0.1 | 0.7 | 0.7 | 0.1 |

| Intersection | | | | | | | | | | | | |
|--------------------------|--------|-------|--------|------|--------|------|--------|-------|------|------|------|------|
| Int Delay, s/veh | 7.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↑ | ↑ | | ↑ | ↑ | | ↔ | ↔ | | ↔ | ↔ | |
| Traffic Vol, veh/h | 66 | 175 | 22 | 52 | 78 | 80 | 25 | 13 | 83 | 88 | 13 | 53 |
| Future Vol, veh/h | 66 | 175 | 22 | 52 | 78 | 80 | 25 | 13 | 83 | 88 | 13 | 53 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 72 | 190 | 24 | 57 | 85 | 87 | 27 | 14 | 90 | 96 | 14 | 58 |
| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | |
| Conflicting Flow All | 172 | 0 | 0 | 214 | 0 | 0 | 625 | 632 | 202 | 641 | 601 | 129 |
| Stage 1 | - | - | - | - | - | - | 346 | 346 | - | 243 | 243 | - |
| Stage 2 | - | - | - | - | - | - | 279 | 286 | - | 398 | 358 | - |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1417 | - | - | 1368 | - | - | 400 | 400 | 844 | 390 | 417 | 926 |
| Stage 1 | - | - | - | - | - | - | 674 | 639 | - | 765 | 708 | - |
| Stage 2 | - | - | - | - | - | - | 732 | 679 | - | 632 | 631 | - |
| Platoon blocked, % | - | - | - | - | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1417 | - | - | 1368 | - | - | 339 | 364 | 844 | 315 | 379 | 926 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 339 | 364 | - | 315 | 379 | - |
| Stage 1 | - | - | - | - | - | - | 640 | 606 | - | 726 | 678 | - |
| Stage 2 | - | - | - | - | - | - | 644 | 650 | - | 523 | 599 | - |
| Approach | EB | | | WB | | | NB | | SB | | | |
| HCM Control Delay, s | 1.9 | | | 1.9 | | | 13 | | 19.4 | | | |
| HCM LOS | | | | | | | B | | C | | | |
| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | | |
| Capacity (veh/h) | 582 | 1417 | - | - | 1368 | - | - | 415 | | | | |
| HCM Lane V/C Ratio | 0.226 | 0.051 | - | - | 0.041 | - | - | 0.403 | | | | |
| HCM Control Delay (s) | 13 | 7.7 | - | - | 7.7 | - | - | 19.4 | | | | |
| HCM Lane LOS | B | A | - | - | A | - | - | C | | | | |
| HCM 95th %tile Q(veh) | 0.9 | 0.2 | - | - | 0.1 | - | - | 1.9 | | | | |

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|------|-------|-------|
| Int Delay, s/veh | 2.4 | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 58 | 361 | 239 | 35 | 54 | 38 |
| Future Vol, veh/h | 58 | 361 | 239 | 35 | 54 | 38 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | - | 0 | 0 | - | 0 | - |
| Grade, % | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 63 | 392 | 260 | 38 | 59 | 41 |
| Major/Minor | Major1 | Major2 | Minor2 | | | |
| Conflicting Flow All | 298 | 0 | - | 0 | 797 | 279 |
| Stage 1 | - | - | - | - | 279 | - |
| Stage 2 | - | - | - | - | 518 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1263 | - | - | - | 356 | 760 |
| Stage 1 | - | - | - | - | 768 | - |
| Stage 2 | - | - | - | - | 598 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1263 | - | - | - | 333 | 760 |
| Mov Cap-2 Maneuver | - | - | - | - | 333 | - |
| Stage 1 | - | - | - | - | 719 | - |
| Stage 2 | - | - | - | - | 598 | - |
| Approach | EB | WB | SB | | | |
| HCM Control Delay, s | 1.1 | 0 | 15.8 | | | |
| HCM LOS | | | C | | | |
| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | 1263 | - | - | - | 434 | |
| HCM Lane V/C Ratio | 0.05 | - | - | - | 0.23 | |
| HCM Control Delay (s) | 8 | 0 | - | - | 15.8 | |
| HCM Lane LOS | A | A | - | - | C | |
| HCM 95th %tile Q(veh) | 0.2 | - | - | - | 0.9 | |

LANE SUMMARY

Site: Poupart / Site Access PM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 48 | 3.0 | 246 | 0.195 | 100 | 20.4 | LOS C | 1.3 | 9.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 48 | 3.0 | | 0.195 | | 20.4 | LOS C | 1.3 | 9.8 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 607 | 3.0 | 896 | 0.677 | 100 | 7.8 | LOS A | 7.4 | 57.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 607 | 3.0 | | 0.677 | | 7.8 | LOS A | 7.4 | 57.8 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 120 | 3.0 | 544 | 0.220 | 100 | 10.4 | LOS B | 1.3 | 10.1 | Full | 500 | 0.0 | 0.0 |
| Approach | 120 | 3.0 | | 0.220 | | 10.4 | LOS B | 1.3 | 10.1 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 1117 | 3.0 | 1072 | 1.043 | 100 | 34.1 | LOS F | 96.1 | 748.6 | Full | 500 | 0.0 | 18.6 |
| Approach | 1117 | 3.0 | | 1.043 | | 34.1 | LOS C | 96.1 | 748.6 | | | | |
| Intersection | 1891 | 3.0 | | 1.043 | | 23.8 | LOS C | 96.1 | 748.6 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: Poupart Extension PM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| East: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 684 | 3.0 | 1097 | 0.623 | 100 | 4.6 | LOS A | 8.0 | 62.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 684 | 3.0 | | 0.623 | | 4.6 | LOS A | 8.0 | 62.6 | | | | |
| North: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 297 | 3.0 | 670 | 0.443 | 100 | 14.6 | LOS B | 2.9 | 22.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 297 | 3.0 | | 0.443 | | 14.6 | LOS B | 2.9 | 22.9 | | | | |
| West: Poupart Extension | | | | | | | | | | | | | |
| Lane 1 ^d | 835 | 3.0 | 808 | 1.033 | 100 | 45.5 | LOS F | 39.3 | 306.1 | Full | 500 | 0.0 | 0.0 |
| Approach | 835 | 3.0 | | 1.033 | | 45.5 | LOS D | 39.3 | 306.1 | | | | |
| Intersection | 1815 | 3.0 | | 1.033 | | 25.1 | LOS C | 39.3 | 306.1 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Dr Corbeil PM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. % | Block. % |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 427 | 3.0 | 769 | 0.556 | 100 | 9.0 | LOS A | 4.6 | 36.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 427 | 3.0 | | 0.556 | | 9.0 | LOS A | 4.6 | 36.0 | | | | |
| East: Dr. Corbeil | | | | | | | | | | | | | |
| Lane 1 ^d | 297 | 3.0 | 814 | 0.364 | 100 | 8.4 | LOS A | 2.4 | 18.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 297 | 3.0 | | 0.364 | | 8.4 | LOS A | 2.4 | 18.7 | | | | |
| North: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 603 | 3.0 | 996 | 0.605 | 100 | 8.7 | LOS A | 6.0 | 46.4 | Full | 500 | 0.0 | 0.0 |
| Approach | 603 | 3.0 | | 0.605 | | 8.7 | LOS A | 6.0 | 46.4 | | | | |
| Intersection | 1327 | 3.0 | | 0.605 | | 8.7 | LOS A | 6.0 | 46.4 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Morris Village Access PM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------|-----|------|-------|---------|----------|-------------|-------|-------|--------|--------|-------|--------|
| | Demand Flows | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. | |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| South: Morris Village Access | | | | | | | | | | | | | |
| Lane 1 ^d | 346 | 3.0 | 1011 | 0.342 | 100 | 12.2 | LOS B | 2.5 | 19.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 52 | 3.0 | 1011 | 0.052 | 100 | 5.1 | LOS A | 0.3 | 2.4 | Short | 60 | 0.0 | NA |
| Approach | 398 | 3.0 | | 0.342 | | 11.3 | LOS B | 2.5 | 19.4 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 342 | 3.0 | 833 | 0.411 | 100 | 8.5 | LOS A | 2.8 | 21.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 342 | 3.0 | | 0.411 | | 8.5 | LOS A | 2.8 | 21.8 | | | | |
| West: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 911 | 3.0 | 1060 | 0.859 | 100 | 7.3 | LOS A | 16.3 | 127.4 | Full | 500 | 0.0 | 0.0 |
| Approach | 911 | 3.0 | | 0.859 | | 7.3 | LOS A | 16.3 | 127.4 | | | | |
| Intersection | 1651 | 3.0 | | 0.859 | | 8.5 | LOS A | 16.3 | 127.4 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: St-Jean / Poupart PM (Medium-term)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 551 | 3.0 | 484 | 1.138 | 100 | 98.3 | LOS F | 39.0 | 303.5 | Full | 500 | 0.0 | 0.0 |
| Approach | 551 | 3.0 | | 1.138 | | 98.3 | LOS F | 39.0 | 303.5 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 575 | 3.0 | 763 | 0.754 | 100 | 15.2 | LOS B | 9.7 | 75.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 575 | 3.0 | | 0.754 | | 15.2 | LOS B | 9.7 | 75.7 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 158 | 3.0 | 505 | 0.312 | 100 | 11.6 | LOS B | 1.9 | 15.1 | Full | 500 | 0.0 | 0.0 |
| Approach | 158 | 3.0 | | 0.312 | | 11.6 | LOS B | 1.9 | 15.1 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 941 | 3.0 | 828 | 1.137 | 100 | 83.5 | LOS F | 63.3 | 492.9 | Full | 500 | 0.0 | 4.6 |
| Approach | 941 | 3.0 | | 1.137 | | 83.5 | LOS F | 63.3 | 492.9 | | | | |
| Intersection | 2225 | 3.0 | | 1.138 | | 64.4 | LOS E | 63.3 | 492.9 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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Appendix D-3

Forecast Build-Out Traffic Analysis



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 19 | 83 | 1571 | 7 | 33 | 582 |
| Future Volume (vph) | 19 | 83 | 1571 | 7 | 33 | 582 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | | 0.0 | 30.0 | |
| Storage Lanes | 1 | 0 | | 0 | 1 | |
| Taper Length (m) | 7.5 | | | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 |
| Fr _t | 0.891 | | 0.999 | | | |
| Flt Protected | 0.991 | | | | 0.950 | |
| Satd. Flow (prot) | 1420 | 0 | 3310 | 0 | 1530 | 3195 |
| Flt Permitted | 0.991 | | | | 0.104 | |
| Satd. Flow (perm) | 1420 | 0 | 3310 | 0 | 167 | 3195 |
| Right Turn on Red | | Yes | | Yes | | |
| Satd. Flow (RTOR) | 51 | | 1 | | | |
| Link Speed (k/h) | 50 | | 50 | | | 50 |
| Link Distance (m) | 196.2 | | 531.3 | | | 401.7 |
| Travel Time (s) | 14.1 | | 38.3 | | | 28.9 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 40% | 13% | 9% | 0% | 18% | 13% |
| Adj. Flow (vph) | 21 | 90 | 1708 | 8 | 36 | 633 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 111 | 0 | 1716 | 0 | 36 | 633 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Right | Left | Left |
| Median Width(m) | 3.6 | | 3.6 | | | 3.6 |
| Link Offset(m) | 0.0 | | 0.0 | | | 0.0 |
| Crosswalk Width(m) | 4.8 | | 4.8 | | | 4.8 |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | | 15 | 25 | |
| Number of Detectors | 1 | | 2 | | 1 | 2 |
| Detector Template | Left | | Thru | | Left | Thru |
| Leading Detector (m) | 2.0 | | 10.0 | | 2.0 | 10.0 |
| Trailing Detector (m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | | 0.6 | | 2.0 | 0.6 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 2 Position(m) | | | 9.4 | | | 9.4 |
| Detector 2 Size(m) | | | 0.6 | | | 0.6 |
| Detector 2 Type | | | Cl+Ex | | Cl+Ex | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | 0.0 | | | 0.0 |
| Turn Type | Perm | | NA | | Perm | NA |
| Protected Phases | | | 2 | | | 6 |



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|-------------------------|-------|-----|-------|-----|-------|-------|
| Permitted Phases | 8 | | | | 6 | |
| Detector Phase | 8 | | 2 | | 6 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Minimum Split (s) | 23.0 | | 23.0 | | 23.0 | 23.0 |
| Total Split (s) | 25.0 | | 95.0 | | 95.0 | 95.0 |
| Total Split (%) | 20.8% | | 79.2% | | 79.2% | 79.2% |
| Maximum Green (s) | 20.0 | | 90.0 | | 90.0 | 90.0 |
| Yellow Time (s) | 3.5 | | 3.5 | | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | | 1.5 | | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Lead/Lag | | | | | | |
| Lead-Lag Optimize? | | | | | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | 3.0 |
| Recall Mode | None | | Min | | Min | Min |
| Walk Time (s) | 7.0 | | 7.0 | | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | | 11.0 | | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | | 0 | | 0 | 0 |
| Act Effect Green (s) | 9.0 | | 51.1 | | 51.1 | 51.1 |
| Actuated g/C Ratio | 0.14 | | 0.78 | | 0.78 | 0.78 |
| v/c Ratio | 0.47 | | 0.67 | | 0.28 | 0.26 |
| Control Delay | 25.0 | | 7.0 | | 10.5 | 3.6 |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Delay | 25.0 | | 7.0 | | 10.5 | 3.6 |
| LOS | C | | A | | B | A |
| Approach Delay | 25.0 | | 7.0 | | 3.9 | |
| Approach LOS | C | | A | | | A |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 65.9

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.67

Intersection Signal Delay: 7.0

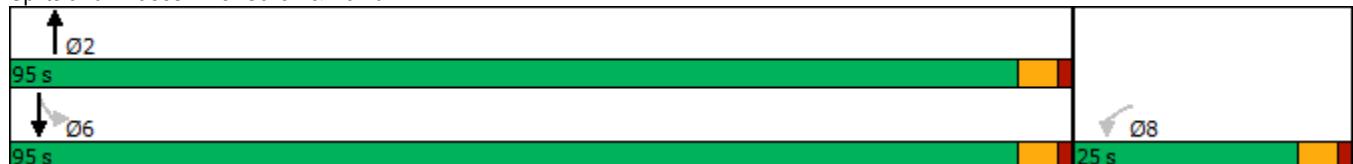
Intersection LOS: A

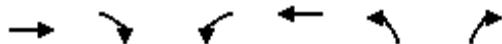
Intersection Capacity Utilization 58.2%

ICU Level of Service B

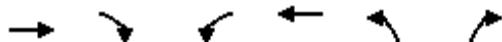
Analysis Period (min) 15

Splits and Phases: 5: Caron & David





| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↗ | ↖ | ↑↑ | ↖ | ↗ |
| Traffic Volume (vph) | 901 | 41 | 20 | 2582 | 120 | 14 |
| Future Volume (vph) | 901 | 41 | 20 | 2582 | 120 | 14 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 3438 | 1524 | 1703 | 3574 | 1770 | 1346 |
| Flt Permitted | | | 0.242 | | 0.950 | |
| Satd. Flow (perm) | 3438 | 1524 | 434 | 3574 | 1770 | 1346 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 45 | | | 15 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 5% | 6% | 6% | 1% | 2% | 20% |
| Adj. Flow (vph) | 979 | 45 | 22 | 2807 | 130 | 15 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 979 | 45 | 22 | 2807 | 130 | 15 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 85.5 | 85.5 | 11.2 | 96.7 | 23.3 | 23.3 |
| Total Split (%) | 71.3% | 71.3% | 9.3% | 80.6% | 19.4% | 19.4% |
| Maximum Green (s) | 79.3 | 79.3 | 5.0 | 90.5 | 18.1 | 18.1 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 83.8 | 83.8 | 90.5 | 90.5 | 18.1 | 18.1 |
| Actuated g/C Ratio | 0.70 | 0.70 | 0.75 | 0.75 | 0.15 | 0.15 |
| v/c Ratio | 0.41 | 0.04 | 0.06 | 1.04 | 0.49 | 0.07 |
| Control Delay | 8.8 | 2.1 | 4.0 | 45.5 | 53.7 | 19.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 8.8 | 2.1 | 4.0 | 45.5 | 53.7 | 19.9 |
| LOS | A | A | A | D | D | B |
| Approach Delay | 8.5 | | | 45.2 | 50.2 | |
| Approach LOS | A | | | D | D | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 120

Natural Cycle: 140

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 1.04

Intersection Signal Delay: 36.0

Intersection LOS: D

Intersection Capacity Utilization 87.5%

ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 6 | 170 | 153 | 72 | 260 | 8 | 360 | 15 | 163 | 2 | 5 | 11 |
| Future Volume (vph) | 6 | 170 | 153 | 72 | 260 | 8 | 360 | 15 | 163 | 2 | 5 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.997 | | | 0.862 | | | 0.894 | |
| Flt Protected | | 0.998 | | | 0.990 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1843 | 1568 | 0 | 1864 | 0 | 1719 | 1426 | 0 | 1805 | 1604 | 0 |
| Flt Permitted | | 0.983 | | | 0.902 | | 0.746 | | | 0.636 | | |
| Satd. Flow (perm) | 0 | 1815 | 1568 | 0 | 1698 | 0 | 1350 | 1426 | 0 | 1208 | 1604 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 166 | | | 3 | | 177 | | | 12 | | |
| Link Speed (k/h) | | 50 | | | 50 | | 50 | | | 50 | | |
| Link Distance (m) | | 549.0 | | | 622.7 | | 441.7 | | | 187.4 | | |
| Travel Time (s) | | 39.5 | | | 44.8 | | 31.8 | | | 13.5 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 3% | 3% | 3% | 0% | 0% | 5% | 13% | 15% | 0% | 20% | 0% |
| Adj. Flow (vph) | 7 | 185 | 166 | 78 | 283 | 9 | 391 | 16 | 177 | 2 | 5 | 12 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 192 | 166 | 0 | 370 | 0 | 391 | 193 | 0 | 2 | 17 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | 4.8 | | | 4.8 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 23.0 | 23.0 | 23.0 | 10.0 | 33.0 | | 27.0 | 27.0 | | 27.0 | 27.0 | |
| Total Split (%) | 38.3% | 38.3% | 38.3% | 16.7% | 55.0% | | 45.0% | 45.0% | | 45.0% | 45.0% | |
| Maximum Green (s) | 18.0 | 18.0 | 18.0 | 5.0 | 28.0 | | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 18.0 | 18.0 | | 28.0 | | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Actuated g/C Ratio | | 0.30 | 0.30 | | 0.47 | | 0.37 | 0.37 | | 0.37 | 0.37 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|-----|------|------|-----|------|-----|------|------|-----|------|------|-----|
| v/c Ratio | | 0.35 | 0.28 | | 0.46 | | 0.79 | 0.30 | | 0.00 | 0.03 | |
| Control Delay | | 18.7 | 4.7 | | 12.9 | | 31.5 | 4.6 | | 12.0 | 8.3 | |
| Queue Delay | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | | 18.7 | 4.7 | | 12.9 | | 31.5 | 4.6 | | 12.0 | 8.3 | |
| LOS | | B | A | | B | | C | A | | B | A | |
| Approach Delay | | 12.2 | | | 12.9 | | | 22.6 | | | 8.7 | |
| Approach LOS | | B | | | B | | C | | | | A | |

Intersection Summary

Area Type: Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 60

Control Type: Pretimed

Maximum v/c Ratio: 0.79

Intersection Signal Delay: 16.9

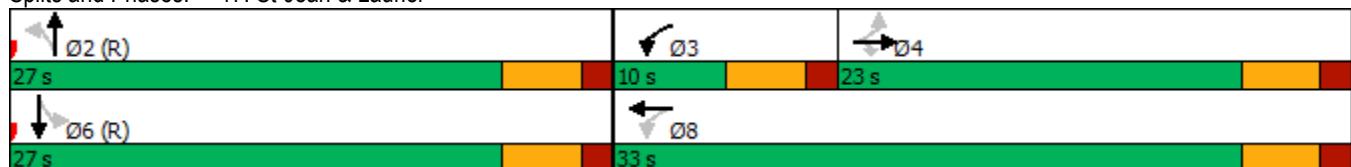
Intersection LOS: B

Intersection Capacity Utilization 66.5%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|----------------------------|--------|-------|-------|-------|--------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 85 | 84 | 102 | 1557 | 542 | 56 |
| Future Volume (vph) | 85 | 84 | 102 | 1557 | 542 | 56 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | 40.0 | | 0.0 | |
| Storage Lanes | 1 | 0 | 1 | | 0 | |
| Taper Length (m) | 7.5 | | 7.5 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 |
| Fr _t | 0.933 | | | 0.986 | | |
| Flt Protected | 0.975 | | 0.950 | | | |
| Satd. Flow (prot) | 1608 | 0 | 1597 | 3312 | 3526 | 0 |
| Flt Permitted | 0.975 | | 0.402 | | | |
| Satd. Flow (perm) | 1608 | 0 | 676 | 3312 | 3526 | 0 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | 37 | | | 24 | | |
| Link Speed (k/h) | 50 | | | 50 | 50 | |
| Link Distance (m) | 1482.6 | | | 401.7 | 1080.0 | |
| Travel Time (s) | 106.7 | | | 28.9 | 77.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 13% | 13% | 9% | 0% | 10% |
| Adj. Flow (vph) | 92 | 91 | 111 | 1692 | 589 | 61 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 183 | 0 | 111 | 1692 | 650 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | | 3.6 | 3.6 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 4.8 | | | 4.8 | 4.8 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | 25 | | 15 | |
| Number of Detectors | 1 | | 1 | 2 | 2 | |
| Detector Template | Left | | Left | Thru | Thru | |
| Leading Detector (m) | 2.0 | | 2.0 | 10.0 | 10.0 | |
| Trailing Detector (m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Position(m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Size(m) | 2.0 | | 2.0 | 0.6 | 0.6 | |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex | |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Queue (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Delay (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 2 Position(m) | | | | 9.4 | 9.4 | |
| Detector 2 Size(m) | | | | 0.6 | 0.6 | |
| Detector 2 Type | | | Cl+Ex | Cl+Ex | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | | 0.0 | 0.0 | |
| Turn Type | Prot | | Perm | NA | NA | |
| Protected Phases | 4 | | | 2 | 6 | |



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|-----|-------|-------|-------|-----|
| Permitted Phases | | | 2 | | | |
| Detector Phase | 4 | | 2 | 2 | 6 | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 23.0 | | 23.0 | 23.0 | 23.0 | |
| Total Split (s) | 28.0 | | 92.0 | 92.0 | 92.0 | |
| Total Split (%) | 23.3% | | 76.7% | 76.7% | 76.7% | |
| Maximum Green (s) | 23.0 | | 87.0 | 87.0 | 87.0 | |
| Yellow Time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | | 1.5 | 1.5 | 1.5 | |
| Lost Time Adjust (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.0 | | 5.0 | 5.0 | 5.0 | |
| Lead/Lag | | | | | | |
| Lead-Lag Optimize? | | | | | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | |
| Recall Mode | None | | Min | Min | Min | |
| Walk Time (s) | 7.0 | | 7.0 | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | | 11.0 | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | | 0 | 0 | 0 | |
| Act Effect Green (s) | 12.7 | | 49.7 | 49.7 | 49.7 | |
| Actuated g/C Ratio | 0.17 | | 0.68 | 0.68 | 0.68 | |
| v/c Ratio | 0.59 | | 0.24 | 0.75 | 0.27 | |
| Control Delay | 31.9 | | 6.5 | 10.4 | 4.8 | |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Delay | 31.9 | | 6.5 | 10.4 | 4.8 | |
| LOS | C | | A | B | A | |
| Approach Delay | 31.9 | | | 10.2 | 4.8 | |
| Approach LOS | C | | | B | A | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 72.8

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.75

Intersection Signal Delay: 10.3

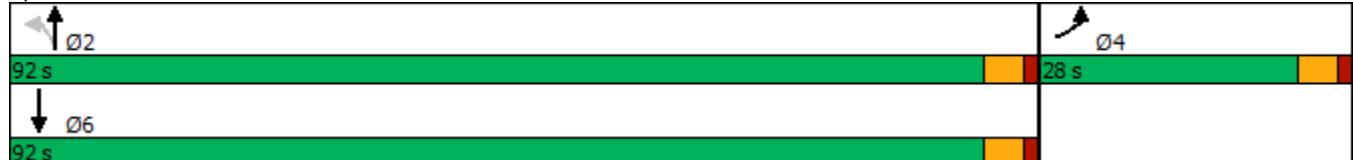
Intersection LOS: B

Intersection Capacity Utilization 61.2%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 21: Caron & Dr. Corbeil



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 100 | 76 | 137 | 74 | 238 | 331 | 309 | 1148 | 23 | 104 | 459 | 38 |
| Future Volume (vph) | 100 | 76 | 137 | 74 | 238 | 331 | 309 | 1148 | 23 | 104 | 459 | 38 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 35.0 | | 125.0 | 30.0 | | 120.0 | 120.0 | | 0.0 | 120.0 | | 40.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 0 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | 0.997 | | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 3529 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.246 | | | 0.703 | | | 0.376 | | | 0.128 | | |
| Satd. Flow (perm) | 458 | 1863 | 1583 | 1310 | 1863 | 1583 | 700 | 3529 | 0 | 238 | 3539 | 1583 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 149 | | | 215 | | 2 | | | | 155 |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | | 50 |
| Link Distance (m) | | 289.2 | | | 367.4 | | | 197.4 | | | | 531.3 |
| Travel Time (s) | | 20.8 | | | 26.5 | | | 14.2 | | | | 38.3 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 109 | 83 | 149 | 80 | 259 | 360 | 336 | 1248 | 25 | 113 | 499 | 41 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 109 | 83 | 149 | 80 | 259 | 360 | 336 | 1273 | 0 | 113 | 499 | 41 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | 3.6 | | | | 3.6 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | 0.0 | | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | 4.8 | | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | | |
| Detector 2 Size(m) | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | | |
| Detector 2 Type | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | | |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | | 6 | | 6 |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|-------|-------|-------|-------|-------|-------|-------|-----|-------|-------|-------|
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 10.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 10.0 | 23.0 | 23.0 |
| Total Split (s) | 11.0 | 44.0 | 44.0 | 33.0 | 33.0 | 33.0 | 27.0 | 61.0 | | 15.0 | 49.0 | 49.0 |
| Total Split (%) | 9.2% | 36.7% | 36.7% | 27.5% | 27.5% | 27.5% | 22.5% | 50.8% | | 12.5% | 40.8% | 40.8% |
| Maximum Green (s) | 6.0 | 39.0 | 39.0 | 28.0 | 28.0 | 28.0 | 22.0 | 56.0 | | 10.0 | 44.0 | 44.0 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | Lead | Lag | | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | None | Max | | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 31.8 | 31.8 | 31.8 | 20.8 | 20.8 | 20.8 | 69.2 | 56.2 | | 57.1 | 48.8 | 48.8 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.29 | 0.19 | 0.19 | 0.19 | 0.62 | 0.50 | | 0.51 | 0.44 | 0.44 |
| v/c Ratio | 0.54 | 0.16 | 0.27 | 0.33 | 0.75 | 0.77 | 0.57 | 0.71 | | 0.48 | 0.32 | 0.05 |
| Control Delay | 41.0 | 30.2 | 6.0 | 42.7 | 56.5 | 28.2 | 14.7 | 25.1 | | 19.9 | 22.8 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.0 | 30.2 | 6.0 | 42.7 | 56.5 | 28.2 | 14.7 | 25.1 | | 19.9 | 22.8 | 0.1 |
| LOS | D | C | A | D | E | C | B | C | | B | C | A |
| Approach Delay | | 23.0 | | | 40.4 | | | 23.0 | | | 20.9 | |
| Approach LOS | | C | | | D | | | C | | | C | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 111.3

Natural Cycle: 75

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.77

Intersection Signal Delay: 26.2

Intersection LOS: C

Intersection Capacity Utilization 73.0%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 33: Caron & Street No.1



Intersection

Intersection Delay, s/veh 20.9

Intersection LOS C

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 540 | 30 | 16 | 219 | 4 |
| Future Vol, veh/h | 4 | 33 | 36 | 14 | 31 | 13 | 22 | 540 | 30 | 16 | 219 | 4 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 6 | 0 | 14 | 6 | 0 | 5 | 3 | 10 | 0 | 1 | 25 |
| Mvmt Flow | 4 | 36 | 39 | 15 | 34 | 14 | 24 | 587 | 33 | 17 | 238 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | | 1 | | | 1 | | | 1 | |
| HCM Control Delay | 9.8 | | | 10.2 | | | 27.3 | | | 11.2 | | |
| HCM LOS | A | | | B | | | D | | | B | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 4% | 5% | 24% | 7% |
| Vol Thru, % | 91% | 45% | 53% | 92% |
| Vol Right, % | 5% | 49% | 22% | 2% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 592 | 73 | 58 | 239 |
| LT Vol | 22 | 4 | 14 | 16 |
| Through Vol | 540 | 33 | 31 | 219 |
| RT Vol | 30 | 36 | 13 | 4 |
| Lane Flow Rate | 643 | 79 | 63 | 260 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.838 | 0.131 | 0.112 | 0.372 |
| Departure Headway (Hd) | 4.687 | 5.937 | 6.413 | 5.156 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 759 | 606 | 561 | 701 |
| Service Time | 2.783 | 3.951 | 4.429 | 3.168 |
| HCM Lane V/C Ratio | 0.847 | 0.13 | 0.112 | 0.371 |
| HCM Control Delay | 27.3 | 9.8 | 10.2 | 11.2 |
| HCM Lane LOS | D | A | B | B |
| HCM 95th-tile Q | 9.5 | 0.4 | 0.4 | 1.7 |

Intersection

Intersection Delay, s/veh 9.7

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Traffic Vol, veh/h | 11 | 10 | 56 | 7 | 63 | 9 | 213 | 76 | 3 | 6 | 42 | 75 |
| Future Vol, veh/h | 11 | 10 | 56 | 7 | 63 | 9 | 213 | 76 | 3 | 6 | 42 | 75 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 22 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 33 | 0 | 4 | 0 |
| Mvmt Flow | 12 | 11 | 61 | 8 | 68 | 10 | 232 | 83 | 3 | 7 | 46 | 82 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 8.5 | | | 8.9 | | | 10.9 | | | 8.2 | | |
| HCM LOS | A | | | A | | | B | | | A | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 73% | 100% | 0% | 9% | 5% |
| Vol Thru, % | 26% | 0% | 15% | 80% | 34% |
| Vol Right, % | 1% | 0% | 85% | 11% | 61% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 292 | 11 | 66 | 79 | 123 |
| LT Vol | 213 | 11 | 0 | 7 | 6 |
| Through Vol | 76 | 0 | 10 | 63 | 42 |
| RT Vol | 3 | 0 | 56 | 9 | 75 |
| Lane Flow Rate | 317 | 12 | 72 | 86 | 134 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.41 | 0.022 | 0.1 | 0.122 | 0.161 |
| Departure Headway (Hd) | 4.65 | 6.526 | 5.042 | 5.112 | 4.346 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 771 | 547 | 707 | 698 | 822 |
| Service Time | 2.687 | 4.281 | 2.797 | 3.167 | 2.392 |
| HCM Lane V/C Ratio | 0.411 | 0.022 | 0.102 | 0.123 | 0.163 |
| HCM Control Delay | 10.9 | 9.4 | 8.4 | 8.9 | 8.2 |
| HCM Lane LOS | B | A | A | A | A |
| HCM 95th-tile Q | 2 | 0.1 | 0.3 | 0.4 | 0.6 |

Intersection

Intersection Delay, s/veh 8.4

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | 0 | 24 | 30 | 208 | 0 | 5 | 7 | 28 | 20 | 12 |
| Traffic Vol, veh/h | 15 | 13 | 0 | 24 | 30 | 208 | 0 | 5 | 7 | 28 | 20 | 12 |
| Future Vol, veh/h | 15 | 13 | 0 | 24 | 30 | 208 | 0 | 5 | 7 | 28 | 20 | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 |
| Mvmt Flow | 16 | 14 | 0 | 26 | 33 | 226 | 0 | 5 | 8 | 30 | 22 | 13 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | WB | | | NB | | SB | | | | |
| Opposing Approach | WB | | EB | | | SB | | NB | | | | |
| Opposing Lanes | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Left | SB | | NB | | | EB | | WB | | | | |
| Conflicting Lanes Left | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Right | NB | | SB | | | WB | | EB | | | | |
| Conflicting Lanes Right | 2 | | 2 | | | 2 | | 2 | | | | |
| HCM Control Delay | 8 | | 8.5 | | | 7.6 | | 8.5 | | | | |
| HCM LOS | A | | A | | | A | | A | | | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 58% | 0% |
| Vol Thru, % | 100% | 19% | 0% | 100% | 0% | 13% | 42% | 0% |
| Vol Right, % | 0% | 81% | 0% | 0% | 0% | 87% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 3 | 9 | 15 | 13 | 24 | 238 | 48 | 12 |
| LT Vol | 0 | 0 | 15 | 0 | 24 | 0 | 28 | 0 |
| Through Vol | 3 | 2 | 0 | 13 | 0 | 30 | 20 | 0 |
| RT Vol | 0 | 7 | 0 | 0 | 0 | 208 | 0 | 12 |
| Lane Flow Rate | 4 | 9 | 16 | 14 | 26 | 259 | 52 | 13 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.005 | 0.012 | 0.025 | 0.019 | 0.037 | 0.29 | 0.081 | 0.016 |
| Departure Headway (Hd) | 5.267 | 4.699 | 5.419 | 4.917 | 5.148 | 4.035 | 5.601 | 4.502 |
| Convergence, Y/N | Yes |
| Cap | 683 | 766 | 664 | 732 | 687 | 874 | 643 | 799 |
| Service Time | 2.971 | 2.402 | 3.123 | 2.621 | 2.945 | 1.831 | 3.302 | 2.204 |
| HCM Lane V/C Ratio | 0.006 | 0.012 | 0.024 | 0.019 | 0.038 | 0.296 | 0.081 | 0.016 |
| HCM Control Delay | 8 | 7.5 | 8.3 | 7.7 | 8.1 | 8.5 | 8.8 | 7.3 |
| HCM Lane LOS | A | A | A | A | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.1 | 0.1 | 0.1 | 1.2 | 0.3 | 0 |

| Intersection | | | | | | | | | | | | |
|--------------------------|-------|--------|------|------|--------|------|------|--------|-------|------|------|------|
| Int Delay, s/veh | 2.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↑ | ↑ | | ↑ | ↑ | | ↔ | ↔ | | ↔ | ↔ | |
| Traffic Vol, veh/h | 9 | 32 | 6 | 51 | 254 | 46 | 7 | 3 | 29 | 17 | 1 | 1 |
| Future Vol, veh/h | 9 | 32 | 6 | 51 | 254 | 46 | 7 | 3 | 29 | 17 | 1 | 1 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 22 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 10 | 35 | 7 | 55 | 276 | 50 | 8 | 3 | 32 | 18 | 1 | 1 |
| Major/Minor | | | | | | | | | | | | |
| Major1 | | Major2 | | | Minor1 | | | Minor2 | | | | |
| Conflicting Flow All | 326 | 0 | 0 | 42 | 0 | 0 | 471 | 495 | 39 | 487 | 473 | 301 |
| Stage 1 | - | - | - | - | - | - | 59 | 59 | - | 411 | 411 | - |
| Stage 2 | - | - | - | - | - | - | 412 | 436 | - | 76 | 62 | - |
| Critical Hdwy | 4.32 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.398 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1129 | - | - | 1580 | - | - | 506 | 479 | 1038 | 494 | 493 | 743 |
| Stage 1 | - | - | - | - | - | - | 958 | 850 | - | 622 | 598 | - |
| Stage 2 | - | - | - | - | - | - | 621 | 583 | - | 938 | 847 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1129 | - | - | 1580 | - | - | 488 | 458 | 1038 | 460 | 471 | 743 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 488 | 458 | - | 460 | 471 | - |
| Stage 1 | - | - | - | - | - | - | 949 | 842 | - | 616 | 577 | - |
| Stage 2 | - | - | - | - | - | - | 597 | 563 | - | 898 | 839 | - |
| Approach | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | |
| HCM Control Delay, s | 1.6 | | 1.1 | | | 9.8 | | | 13 | | | |
| HCM LOS | A | | | | | | B | | | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | |
| Capacity (veh/h) | 799 | 1129 | - | - | 1580 | - | - | - | 470 | | | |
| HCM Lane V/C Ratio | 0.053 | 0.009 | - | - | 0.035 | - | - | - | 0.044 | | | |
| HCM Control Delay (s) | 9.8 | 8.2 | - | - | 7.4 | - | - | - | 13 | | | |
| HCM Lane LOS | A | A | - | - | A | - | - | - | B | | | |
| HCM 95th %tile Q(veh) | 0.2 | 0 | - | - | 0.1 | - | - | - | 0.1 | | | |

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|------|-------|-------|
| Int Delay, s/veh | 2.5 | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 32 | 225 | 633 | 82 | 26 | 91 |
| Future Vol, veh/h | 32 | 225 | 633 | 82 | 26 | 91 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | - | 0 | 0 | - | 0 | - |
| Grade, % | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 35 | 245 | 688 | 89 | 28 | 99 |
| Major/Minor | Major1 | Major2 | Minor2 | | | |
| Conflicting Flow All | 777 | 0 | - | 0 | 1048 | 733 |
| Stage 1 | - | - | - | - | 733 | - |
| Stage 2 | - | - | - | - | 315 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 839 | - | - | - | 252 | 421 |
| Stage 1 | - | - | - | - | 475 | - |
| Stage 2 | - | - | - | - | 740 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 839 | - | - | - | 240 | 421 |
| Mov Cap-2 Maneuver | - | - | - | - | 240 | - |
| Stage 1 | - | - | - | - | 452 | - |
| Stage 2 | - | - | - | - | 740 | - |
| Approach | EB | WB | SB | | | |
| HCM Control Delay, s | 1.2 | 0 | 20.3 | | | |
| HCM LOS | | | C | | | |
| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | 839 | - | - | - | 361 | |
| HCM Lane V/C Ratio | 0.041 | - | - | - | 0.352 | |
| HCM Control Delay (s) | 9.5 | 0 | - | - | 20.3 | |
| HCM Lane LOS | A | A | - | - | C | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | - | 1.6 | |

LANE SUMMARY

Site: Poupart / Site Access AM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 260 | 3.0 | 678 | 0.383 | 100 | 12.4 | LOS B | 1.8 | 13.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 260 | 3.0 | | 0.383 | | 12.4 | LOS B | 1.8 | 13.6 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 746 | 3.0 | 970 | 0.769 | 100 | 9.6 | LOS A | 9.5 | 74.2 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 746 | 3.0 | 970 | 0.769 | 100 | 9.5 | LOS A | 9.5 | 74.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 1491 | 3.0 | | 0.769 | | 9.5 | LOS A | 9.5 | 74.2 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 227 | 3.0 | 275 | 0.825 | 100 | 30.8 | LOS C | 5.7 | 44.4 | Full | 500 | 0.0 | 0.0 |
| Approach | 227 | 3.0 | | 0.825 | | 30.8 | LOS C | 5.7 | 44.4 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 301 | 3.0 | 1158 | 0.259 | 100 | 5.6 | LOS A | 1.5 | 11.5 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 301 | 3.0 | 1158 | 0.259 | 100 | 4.5 | LOS A | 1.5 | 11.5 | Full | 500 | 0.0 | 0.0 |
| Approach | 601 | 3.0 | | 0.259 | | 5.1 | LOS A | 1.5 | 11.5 | | | | |
| Intersection | 2579 | 3.0 | | 0.825 | | 10.6 | LOS B | 9.5 | 74.2 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: Poupart Extension AM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| East: Poupart | | | | | | | | | | | | | |
| Lane 1 | 927 | 3.0 | 1203 | 0.770 | 100 | 4.6 | LOS A | 10.8 | 84.5 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 927 | 3.0 | 1203 | 0.770 | 100 | 4.6 | LOS A | 10.8 | 84.5 | Full | 500 | 0.0 | 0.0 |
| Approach | 1854 | 3.0 | | 0.770 | | 4.6 | LOS A | 10.8 | 84.5 | | | | |
| North: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 136 | 3.0 | 379 | 0.358 | 100 | 18.7 | LOS B | 1.6 | 12.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 136 | 3.0 | | 0.358 | | 18.7 | LOS B | 1.6 | 12.6 | | | | |
| West: Poupart Extension | | | | | | | | | | | | | |
| Lane 1 | 255 | 3.0 | 1091 | 0.234 | 100 | 5.3 | LOS A | 1.3 | 10.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 255 | 3.0 | 1091 | 0.234 | 100 | 4.8 | LOS A | 1.3 | 10.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 510 | 3.0 | | 0.234 | | 5.1 | LOS A | 1.3 | 10.0 | | | | |
| Intersection | 2500 | 3.0 | | 0.770 | | 5.5 | LOS A | 10.8 | 84.5 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Dr Corbeil AM (Ultimate)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 425 | 3.0 | 992 | 0.428 | 100 | 5.5 | LOS A | 3.1 | 24.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 425 | 3.0 | | 0.428 | | 5.5 | LOS A | 3.1 | 24.3 | | | | |
| East: Dr. Corbeil | | | | | | | | | | | | | |
| Lane 1 ^d | 390 | 3.0 | 767 | 0.509 | 100 | 10.1 | LOS B | 3.8 | 29.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 390 | 3.0 | | 0.509 | | 10.1 | LOS B | 3.8 | 29.6 | | | | |
| North: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 287 | 3.0 | 968 | 0.296 | 100 | 7.3 | LOS A | 2.0 | 15.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 287 | 3.0 | | 0.296 | | 7.3 | LOS A | 2.0 | 15.2 | | | | |
| Intersection | 1102 | 3.0 | | 0.509 | | 7.6 | LOS A | 3.8 | 29.6 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Morris Village Access AM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|-------------------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: Morris Village Access | | | | | | | | | | | | | |
| Lane 1 ^d | 887 | 3.0 | 1167 | 0.760 | 100 | 14.7 | LOS B | 10.2 | 79.7 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 145 | 3.0 | 1167 | 0.124 | 100 | 4.8 | LOS A | 0.7 | 5.1 | Short | 60 | 0.0 | NA |
| Approach | 1032 | 3.0 | | 0.760 | | 13.3 | LOS B | 10.2 | 79.7 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 167 | 3.0 | 444 | 0.377 | 100 | 13.8 | LOS B | 2.7 | 21.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 204 | 3.0 | 542 | 0.377 | 100 | 10.1 | LOS B | 2.9 | 23.0 | Short | 60 | 0.0 | NA |
| Approach | 372 | 3.0 | | 0.377 | | 11.8 | LOS B | 2.9 | 23.0 | | | | |
| West: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 252 | 3.0 | 1357 | 0.186 | 100 | 3.6 | LOS A | 1.3 | 9.8 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 297 | 3.0 | 1357 | 0.219 | 100 | 3.9 | LOS A | 1.5 | 12.0 | Full | 500 | 0.0 | 0.0 |
| Approach | 549 | 3.0 | | 0.219 | | 3.8 | LOS A | 1.5 | 12.0 | | | | |
| Intersection | 1952 | 3.0 | | 0.760 | | 10.3 | LOS B | 10.2 | 79.7 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: St-Jean / Poupart AM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 515 | 3.0 | 904 | 0.570 | 100 | 13.0 | LOS B | 4.2 | 32.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 227 | 3.0 | 937 | 0.243 | 100 | 5.5 | LOS A | 1.2 | 9.2 | Short | 60 | 0.0 | NA |
| Approach | 742 | 3.0 | | 0.570 | | 10.7 | LOS B | 4.2 | 32.4 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 604 | 3.0 | 738 | 0.818 | 100 | 20.0 | LOS C | 11.1 | 86.3 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 604 | 3.0 | 738 | 0.818 | 100 | 16.6 | LOS B | 11.1 | 86.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 1208 | 3.0 | | 0.818 | | 18.3 | LOS B | 11.1 | 86.3 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 249 | 3.0 | 253 | 0.983 | 100 | 62.1 | LOS E | 10.8 | 83.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 249 | 3.0 | | 0.983 | | 62.1 | LOS E | 10.8 | 83.8 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 | 278 | 3.0 | 801 | 0.347 | 100 | 7.9 | LOS A | 2.1 | 16.2 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 278 | 3.0 | 801 | 0.347 | 100 | 6.9 | LOS A | 2.1 | 16.2 | Full | 500 | 0.0 | 0.0 |
| Approach | 557 | 3.0 | | 0.347 | | 7.4 | LOS A | 2.1 | 16.2 | | | | |
| Intersection | 2755 | 3.0 | | 0.983 | | 18.0 | LOS B | 11.1 | 86.3 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

SIDRA INTERSECTION 6.1 | Copyright © 2000-2015 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: CASTLEGLENN CONSULTANTS | Processed: Monday, October 22, 2018 11:17:08 AM

Project: R:\CastleGlenn\Projects\Ontario Projects\Rockland\7218- Morris-Rockland Traffic Study\Sidra\Ultimate Build-out\Ultimate Build-out.sip6

| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 13 | 66 | 1137 | 19 | 96 | 1718 |
| Future Volume (vph) | 13 | 66 | 1137 | 19 | 96 | 1718 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | | 0.0 | 30.0 | |
| Storage Lanes | 1 | 0 | | 0 | 1 | |
| Taper Length (m) | 7.5 | | | | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 |
| Frt | 0.887 | | 0.997 | | | |
| Flt Protected | 0.992 | | | | 0.950 | |
| Satd. Flow (prot) | 1672 | 0 | 3564 | 0 | 1671 | 3574 |
| Flt Permitted | 0.992 | | | | 0.204 | |
| Satd. Flow (perm) | 1672 | 0 | 3564 | 0 | 359 | 3574 |
| Right Turn on Red | | Yes | | Yes | | |
| Satd. Flow (RTOR) | 72 | | 4 | | | |
| Link Speed (k/h) | 50 | | 50 | | | 50 |
| Link Distance (m) | 196.2 | | 558.9 | | 401.7 | |
| Travel Time (s) | 14.1 | | 40.2 | | 28.9 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 8% | 1% |
| Adj. Flow (vph) | 14 | 72 | 1236 | 21 | 104 | 1867 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 86 | 0 | 1257 | 0 | 104 | 1867 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Right | Left | Left |
| Median Width(m) | 3.6 | | 3.6 | | | 3.6 |
| Link Offset(m) | 0.0 | | 0.0 | | | 0.0 |
| Crosswalk Width(m) | 4.8 | | 4.8 | | | 4.8 |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | | 15 | 25 | |
| Number of Detectors | 1 | | 2 | | 1 | 2 |
| Detector Template | Left | | Thru | | Left | Thru |
| Leading Detector (m) | 2.0 | | 10.0 | | 2.0 | 10.0 |
| Trailing Detector (m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | | 0.6 | | 2.0 | 0.6 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Detector 2 Position(m) | | | 9.4 | | | 9.4 |
| Detector 2 Size(m) | | | 0.6 | | | 0.6 |
| Detector 2 Type | | | Cl+Ex | | Cl+Ex | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | 0.0 | | | 0.0 |
| Turn Type | Perm | | NA | | Perm | NA |
| Protected Phases | | | 2 | | | 6 |



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|-------------------------|-------|-----|-------|-----|-------|-------|
| Permitted Phases | 8 | | | | 6 | |
| Detector Phase | 8 | | 2 | | 6 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Minimum Split (s) | 23.0 | | 23.0 | | 23.0 | 23.0 |
| Total Split (s) | 24.0 | | 96.0 | | 96.0 | 96.0 |
| Total Split (%) | 20.0% | | 80.0% | | 80.0% | 80.0% |
| Maximum Green (s) | 19.0 | | 91.0 | | 91.0 | 91.0 |
| Yellow Time (s) | 3.5 | | 3.5 | | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | | 1.5 | | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | | 5.0 | | 5.0 | 5.0 |
| Lead/Lag | | | | | | |
| Lead-Lag Optimize? | | | | | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | 3.0 |
| Recall Mode | None | | Min | | Min | Min |
| Walk Time (s) | 7.0 | | 7.0 | | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | | 11.0 | | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | | 0 | | 0 | 0 |
| Act Effect Green (s) | 7.1 | | 50.8 | | 50.8 | 50.8 |
| Actuated g/C Ratio | 0.11 | | 0.80 | | 0.80 | 0.80 |
| v/c Ratio | 0.34 | | 0.44 | | 0.36 | 0.65 |
| Control Delay | 15.4 | | 3.5 | | 7.4 | 5.4 |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Delay | 15.4 | | 3.5 | | 7.4 | 5.4 |
| LOS | B | | A | | A | A |
| Approach Delay | 15.4 | | 3.5 | | 5.5 | |
| Approach LOS | B | | A | | | A |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 63.4

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.65

Intersection Signal Delay: 5.0

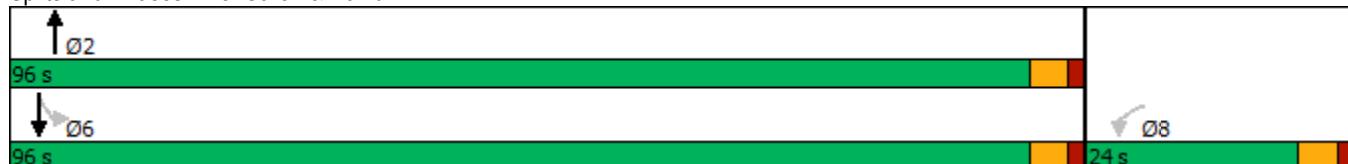
Intersection LOS: A

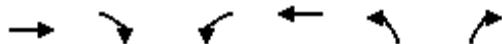
Intersection Capacity Utilization 60.6%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 5: Caron & David





| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|----------------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↗ | ↖ | ↖ | ↘ | ↖ |
| Traffic Volume (vph) | 2691 | 208 | 72 | 1495 | 73 | 112 |
| Future Volume (vph) | 2691 | 208 | 72 | 1495 | 73 | 112 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 85.0 | 125.0 | | 0.0 | 0.0 | |
| Storage Lanes | 1 | 1 | | 1 | 1 | |
| Taper Length (m) | | | 70.0 | | 7.5 | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | | 0.850 | | | 0.850 | |
| Flt Protected | | | 0.950 | | 0.950 | |
| Satd. Flow (prot) | 3505 | 1599 | 1752 | 3539 | 1805 | 1615 |
| Flt Permitted | | | 0.047 | | 0.950 | |
| Satd. Flow (perm) | 3505 | 1599 | 87 | 3539 | 1805 | 1615 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 149 | | | 67 | |
| Link Speed (k/h) | 50 | | 50 | 50 | | |
| Link Distance (m) | 470.1 | | | 337.0 | 115.6 | |
| Travel Time (s) | 33.8 | | | 24.3 | 8.3 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 3% | 1% | 3% | 2% | 0% | 0% |
| Adj. Flow (vph) | 2925 | 226 | 78 | 1625 | 79 | 122 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 2925 | 226 | 78 | 1625 | 79 | 122 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | 3.6 | 3.6 | | |
| Link Offset(m) | 0.0 | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 4.8 | | 4.8 | 4.8 | | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | | 15 | 25 | | 25 | 15 |
| Number of Detectors | 2 | 1 | 1 | 2 | 1 | 1 |
| Detector Template | Thru | Right | Left | Thru | Left | Right |
| Leading Detector (m) | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 9.4 | | 9.4 | | | |
| Detector 2 Size(m) | 0.6 | | 0.6 | | | |
| Detector 2 Type | Cl+Ex | | Cl+Ex | | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | 0.0 | | 0.0 | | | |
| Turn Type | NA | Perm | pm+pt | NA | Perm | Perm |
| Protected Phases | 4 | | 3 | 8 | | |



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|------|-------|-------|-------|
| Permitted Phases | | 4 | 8 | | 2 | 2 |
| Detector Phase | 4 | 4 | 3 | 8 | 2 | 2 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 27.2 | 27.2 | 11.2 | 27.2 | 23.2 | 23.2 |
| Total Split (s) | 85.0 | 85.0 | 11.2 | 96.2 | 23.8 | 23.8 |
| Total Split (%) | 70.8% | 70.8% | 9.3% | 80.2% | 19.8% | 19.8% |
| Maximum Green (s) | 78.8 | 78.8 | 5.0 | 90.0 | 18.6 | 18.6 |
| Yellow Time (s) | 4.6 | 4.6 | 4.6 | 4.6 | 3.3 | 3.3 |
| All-Red Time (s) | 1.6 | 1.6 | 1.6 | 1.6 | 1.9 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.2 | 6.2 | 6.2 | 6.2 | 5.2 | 5.2 |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 14.0 | 14.0 | | 14.0 | 9.0 | 9.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 78.9 | 78.9 | 87.7 | 87.7 | 18.6 | 18.6 |
| Actuated g/C Ratio | 0.67 | 0.67 | 0.74 | 0.74 | 0.16 | 0.16 |
| v/c Ratio | 1.25 | 0.20 | 0.58 | 0.62 | 0.28 | 0.39 |
| Control Delay | 136.2 | 3.3 | 30.4 | 8.3 | 47.6 | 26.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 136.2 | 3.3 | 30.4 | 8.3 | 47.6 | 26.1 |
| LOS | F | A | C | A | D | C |
| Approach Delay | 126.7 | | | 9.3 | 34.6 | |
| Approach LOS | F | | | A | C | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 117.8

Natural Cycle: 150

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 1.25

Intersection Signal Delay: 83.5

Intersection LOS: F

Intersection Capacity Utilization 90.8%

ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 12: Carmen Bergeron & CR 17



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 9 | 406 | 394 | 162 | 341 | 14 | 257 | 13 | 153 | 20 | 11 | 17 |
| Future Volume (vph) | 9 | 406 | 394 | 162 | 341 | 14 | 257 | 13 | 153 | 20 | 11 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | | 10.0 | 0.0 | | 0.0 | 20.0 | | 0.0 | 10.0 | | 0.0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 10.0 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | | | 0.850 | | 0.996 | | | 0.862 | | | 0.910 | |
| Flt Protected | | 0.999 | | | 0.985 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1898 | 1568 | 0 | 1861 | 0 | 1752 | 1638 | 0 | 1805 | 1729 | 0 |
| Flt Permitted | | 0.987 | | | 0.518 | | 0.738 | | | 0.616 | | |
| Satd. Flow (perm) | 0 | 1875 | 1568 | 0 | 978 | 0 | 1361 | 1638 | 0 | 1170 | 1729 | 0 |
| Right Turn on Red | | Yes | | | Yes | | | Yes | | | Yes | |
| Satd. Flow (RTOR) | | 202 | | | 4 | | | 166 | | | 18 | |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 549.0 | | | 622.7 | | | 441.7 | | | 187.4 | |
| Travel Time (s) | | 39.5 | | | 44.8 | | | 31.8 | | | 13.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 3% | 0% | 0% | 7% | 3% | 0% | 0% | 0% | 0% | 0% |
| Adj. Flow (vph) | 10 | 441 | 428 | 176 | 371 | 15 | 279 | 14 | 166 | 22 | 12 | 18 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 451 | 428 | 0 | 562 | 0 | 279 | 180 | 0 | 22 | 30 | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Minimum Split (s) | 23.0 | 23.0 | 23.0 | 10.1 | 23.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (s) | 36.9 | 36.9 | 36.9 | 10.1 | 47.0 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Total Split (%) | 52.7% | 52.7% | 52.7% | 14.4% | 67.1% | | 32.9% | 32.9% | | 32.9% | 32.9% | |
| Maximum Green (s) | 31.9 | 31.9 | 31.9 | 5.1 | 42.0 | | 18.0 | 18.0 | | 18.0 | 18.0 | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | | 1.5 | 1.5 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 5.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | Lag | Lag | Lag | Lead | | | | | | | | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | | | | | |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | | 11.0 | | 11.0 | 11.0 | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | 0 | |
| Act Effect Green (s) | | 31.9 | 31.9 | | 42.0 | | 18.0 | 18.0 | | 18.0 | 18.0 | |
| Actuated g/C Ratio | | 0.46 | 0.46 | | 0.60 | | 0.26 | 0.26 | | 0.26 | 0.26 | |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------|-----|------|------|-----|------|-----|------|------|-----|------|------|-----|
| v/c Ratio | | 0.53 | 0.52 | | 0.86 | | 0.80 | 0.33 | | 0.07 | 0.07 | |
| Control Delay | | 16.5 | 9.4 | | 26.5 | | 44.0 | 6.6 | | 20.6 | 12.8 | |
| Queue Delay | | 0.0 | 0.0 | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | | 16.5 | 9.4 | | 26.5 | | 44.0 | 6.6 | | 20.6 | 12.8 | |
| LOS | | B | A | | C | | D | A | | C | B | |
| Approach Delay | | 13.0 | | | 26.5 | | | 29.3 | | | 16.1 | |
| Approach LOS | | B | | | C | | | C | | | B | |

Intersection Summary

Area Type: Other

Cycle Length: 70

Actuated Cycle Length: 70

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Green

Natural Cycle: 70

Control Type: Pretimed

Maximum v/c Ratio: 0.86

Intersection Signal Delay: 20.8

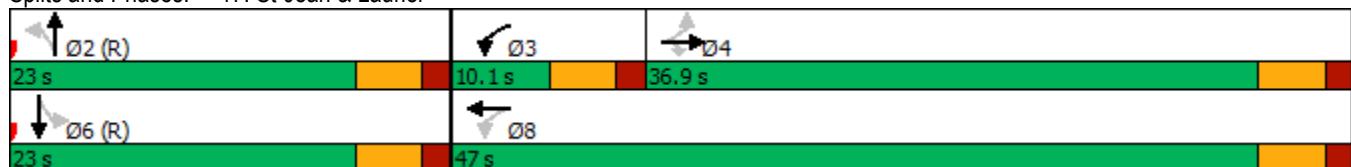
Intersection LOS: C

Intersection Capacity Utilization 83.0%

ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 17: St-Jean & Laurier



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|----------------------------|--------|-------|-------|-------|--------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 107 | 147 | 114 | 1106 | 1691 | 110 |
| Future Volume (vph) | 107 | 147 | 114 | 1106 | 1691 | 110 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 0.0 | 40.0 | | 0.0 | |
| Storage Lanes | 1 | 0 | 1 | | 0 | |
| Taper Length (m) | 7.5 | | 7.5 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 |
| Fr _t | 0.922 | | | 0.991 | | |
| Flt Protected | 0.979 | | 0.950 | | | |
| Satd. Flow (prot) | 1715 | 0 | 1805 | 3610 | 3578 | 0 |
| Flt Permitted | 0.979 | | 0.058 | | | |
| Satd. Flow (perm) | 1715 | 0 | 110 | 3610 | 3578 | 0 |
| Right Turn on Red | | Yes | | | Yes | |
| Satd. Flow (RTOR) | 51 | | | 10 | | |
| Link Speed (k/h) | 50 | | | 50 | 50 | |
| Link Distance (m) | 1482.6 | | | 401.7 | 1080.0 | |
| Travel Time (s) | 106.7 | | | 28.9 | 77.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 0% |
| Adj. Flow (vph) | 116 | 160 | 124 | 1202 | 1838 | 120 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 276 | 0 | 124 | 1202 | 1958 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.6 | | | 3.6 | 3.6 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 4.8 | | | 4.8 | 4.8 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | 15 | 25 | | 15 | |
| Number of Detectors | 1 | | 1 | 2 | 2 | |
| Detector Template | Left | | Left | Thru | Thru | |
| Leading Detector (m) | 2.0 | | 2.0 | 10.0 | 10.0 | |
| Trailing Detector (m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Position(m) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Size(m) | 2.0 | | 2.0 | 0.6 | 0.6 | |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex | |
| Detector 1 Channel | | | | | | |
| Detector 1 Extend (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Queue (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 1 Delay (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Detector 2 Position(m) | | | | 9.4 | 9.4 | |
| Detector 2 Size(m) | | | | 0.6 | 0.6 | |
| Detector 2 Type | | | Cl+Ex | Cl+Ex | | |
| Detector 2 Channel | | | | | | |
| Detector 2 Extend (s) | | | | 0.0 | 0.0 | |
| Turn Type | Perm | pm+pt | | NA | NA | |
| Protected Phases | | | 5 | 2 | 6 | |



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|------|-------|-------|-------|-----|
| Permitted Phases | 4 | | 2 | | | |
| Detector Phase | 4 | | 5 | 2 | 6 | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | | 5.0 | 5.0 | | |
| Minimum Split (s) | 23.0 | | 10.0 | 23.0 | 23.0 | |
| Total Split (s) | 28.0 | | 13.0 | 92.0 | 79.0 | |
| Total Split (%) | 23.3% | | 10.8% | 76.7% | 65.8% | |
| Maximum Green (s) | 23.0 | | 8.0 | 87.0 | 74.0 | |
| Yellow Time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | |
| All-Red Time (s) | 1.5 | | 1.5 | 1.5 | 1.5 | |
| Lost Time Adjust (s) | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.0 | | 5.0 | 5.0 | 5.0 | |
| Lead/Lag | | Lead | | Lag | | |
| Lead-Lag Optimize? | | Yes | | Yes | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | | |
| Recall Mode | None | | None | Min | Min | |
| Walk Time (s) | 7.0 | | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | 11.0 | | | 11.0 | 11.0 | |
| Pedestrian Calls (#/hr) | 0 | | | 0 | 0 | |
| Act Effect Green (s) | 18.8 | | 77.2 | 77.2 | 64.0 | |
| Actuated g/C Ratio | 0.18 | | 0.73 | 0.73 | 0.60 | |
| v/c Ratio | 0.80 | | 0.59 | 0.46 | 0.91 | |
| Control Delay | 53.8 | | 29.5 | 6.8 | 26.0 | |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | |
| Total Delay | 53.8 | | 29.5 | 6.8 | 26.0 | |
| LOS | D | | C | A | C | |
| Approach Delay | 53.8 | | | 8.9 | 26.0 | |
| Approach LOS | D | | | A | C | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 106.3

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.91

Intersection Signal Delay: 21.8

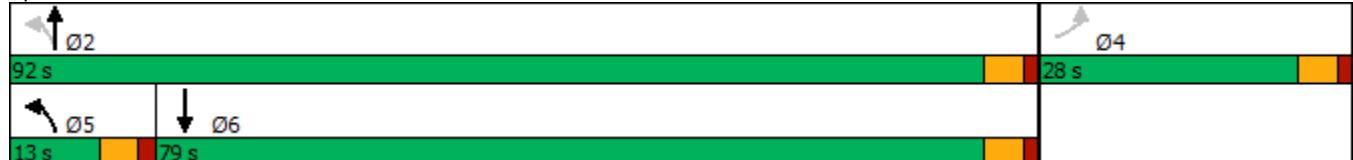
Intersection LOS: C

Intersection Capacity Utilization 84.0%

ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 21: Caron & Dr. Corbeil



| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 69 | 250 | 341 | 48 | 157 | 217 | 242 | 870 | 78 | 349 | 1275 | 108 |
| Future Volume (vph) | 69 | 250 | 341 | 48 | 157 | 217 | 242 | 870 | 78 | 349 | 1275 | 108 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 35.0 | | 125.0 | 30.0 | | 120.0 | 120.0 | | 0.0 | 120.0 | | 40.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 0 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.988 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 3497 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.365 | | | 0.592 | | | 0.105 | | | 0.119 | | |
| Satd. Flow (perm) | 680 | 1863 | 1583 | 1103 | 1863 | 1583 | 196 | 3497 | 0 | 222 | 3539 | 1583 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 284 | | | 236 | | | 10 | | | 131 |
| Link Speed (k/h) | | 50 | | | 50 | | | 50 | | | 50 | |
| Link Distance (m) | | 179.3 | | | 276.0 | | | 177.7 | | | 558.9 | |
| Travel Time (s) | | 12.9 | | | 19.9 | | | 12.8 | | | 40.2 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 75 | 272 | 371 | 52 | 171 | 236 | 263 | 946 | 85 | 379 | 1386 | 117 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 75 | 272 | 371 | 52 | 171 | 236 | 263 | 1031 | 0 | 379 | 1386 | 117 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 3.6 | | | 3.6 | | | 3.6 | | | 3.6 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 4.8 | | | 4.8 | | | 4.8 | | | 4.8 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 5 | 2 | | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | | 6 | | 6 |

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-------|-------|-------|
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 10.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 10.0 | 23.0 | | 10.0 | 23.0 | 23.0 |
| Total Split (s) | 10.0 | 33.0 | 33.0 | 23.0 | 23.0 | 23.0 | 18.0 | 41.0 | | 26.0 | 49.0 | 49.0 |
| Total Split (%) | 10.0% | 33.0% | 33.0% | 23.0% | 23.0% | 23.0% | 18.0% | 41.0% | | 26.0% | 49.0% | 49.0% |
| Maximum Green (s) | 5.0 | 28.0 | 28.0 | 18.0 | 18.0 | 18.0 | 13.0 | 36.0 | | 21.0 | 44.0 | 44.0 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | Lead | Lag | | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Max | | None | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 |
| Act Effect Green (s) | 22.0 | 22.0 | 22.0 | 14.3 | 14.3 | 14.3 | 50.3 | 38.0 | | 61.1 | 44.3 | 44.3 |
| Actuated g/C Ratio | 0.23 | 0.23 | 0.23 | 0.15 | 0.15 | 0.15 | 0.54 | 0.41 | | 0.65 | 0.47 | 0.47 |
| v/c Ratio | 0.34 | 0.62 | 0.63 | 0.31 | 0.60 | 0.54 | 0.84 | 0.72 | | 0.84 | 0.83 | 0.14 |
| Control Delay | 32.5 | 38.6 | 13.3 | 41.7 | 47.5 | 9.8 | 49.2 | 28.5 | | 38.0 | 28.1 | 2.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 32.5 | 38.6 | 13.3 | 41.7 | 47.5 | 9.8 | 49.2 | 28.5 | | 38.0 | 28.1 | 2.9 |
| LOS | C | D | B | D | D | A | D | C | | D | C | A |
| Approach Delay | | 24.9 | | | 27.5 | | | 32.7 | | | 28.5 | |
| Approach LOS | | C | | | C | | | C | | | C | |

Intersection Summary

Area Type: Other

Cycle Length: 100

Actuated Cycle Length: 93.7

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.84

Intersection Signal Delay: 29.1

Intersection LOS: C

Intersection Capacity Utilization 82.6%

ICU Level of Service E

Analysis Period (min) 15

Splits and Phases: 33: Caron & Street No.1



Intersection

Intersection Delay, s/veh 46.2

Intersection LOS E

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 410 | 28 | 33 | 578 | 9 |
| Future Vol, veh/h | 16 | 36 | 48 | 31 | 43 | 17 | 59 | 410 | 28 | 33 | 578 | 9 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 6 | 3 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 0 |
| Mvmt Flow | 17 | 39 | 52 | 34 | 47 | 18 | 64 | 446 | 30 | 36 | 628 | 10 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | | EB | | | SB | | | NB | |
| Opposing Lanes | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Left | SB | | | | NB | | | EB | | | WB | |
| Conflicting Lanes Left | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Right | NB | | | | SB | | | WB | | | EB | |
| Conflicting Lanes Right | 1 | | | | 1 | | | 1 | | | 1 | |
| HCM Control Delay | 12.4 | | | | 12.4 | | | 33.7 | | | 66.7 | |
| HCM LOS | B | | | | B | | | D | | | F | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 12% | 16% | 34% | 5% |
| Vol Thru, % | 82% | 36% | 47% | 93% |
| Vol Right, % | 6% | 48% | 19% | 1% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 497 | 100 | 91 | 620 |
| LT Vol | 59 | 16 | 31 | 33 |
| Through Vol | 410 | 36 | 43 | 578 |
| RT Vol | 28 | 48 | 17 | 9 |
| Lane Flow Rate | 540 | 109 | 99 | 674 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.856 | 0.217 | 0.201 | 1.03 |
| Departure Headway (Hd) | 5.703 | 7.331 | 7.485 | 5.504 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 627 | 492 | 483 | 654 |
| Service Time | 3.802 | 5.331 | 5.485 | 3.596 |
| HCM Lane V/C Ratio | 0.861 | 0.222 | 0.205 | 1.031 |
| HCM Control Delay | 33.7 | 12.4 | 12.4 | 66.7 |
| HCM Lane LOS | D | B | B | F |
| HCM 95th-tile Q | 9.6 | 0.8 | 0.7 | 17 |

Intersection

Intersection Delay, s/veh 11.4

Intersection LOS B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ | ↓ |
| Traffic Vol, veh/h | 123 | 55 | 232 | 9 | 24 | 17 | 121 | 79 | 14 | 22 | 71 | 99 |
| Future Vol, veh/h | 123 | 55 | 232 | 9 | 24 | 17 | 121 | 79 | 14 | 22 | 71 | 99 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Mvmt Flow | 134 | 60 | 252 | 10 | 26 | 18 | 132 | 86 | 15 | 24 | 77 | 108 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 2 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 2 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 2 | | |
| HCM Control Delay | 11.8 | | | 9.6 | | | 11.7 | | | 10.6 | | |
| HCM LOS | B | | | A | | | B | | | B | | |

| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|-------|
| Vol Left, % | 57% | 100% | 0% | 18% | 11% |
| Vol Thru, % | 37% | 0% | 19% | 48% | 37% |
| Vol Right, % | 7% | 0% | 81% | 34% | 52% |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 214 | 123 | 287 | 50 | 192 |
| LT Vol | 121 | 123 | 0 | 9 | 22 |
| Through Vol | 79 | 0 | 55 | 24 | 71 |
| RT Vol | 14 | 0 | 232 | 17 | 99 |
| Lane Flow Rate | 233 | 134 | 312 | 54 | 209 |
| Geometry Grp | 2 | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.36 | 0.234 | 0.453 | 0.089 | 0.305 |
| Departure Headway (Hd) | 5.567 | 6.304 | 5.225 | 5.923 | 5.265 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 647 | 571 | 689 | 604 | 682 |
| Service Time | 3.6 | 4.033 | 2.954 | 3.969 | 3.3 |
| HCM Lane V/C Ratio | 0.36 | 0.235 | 0.453 | 0.089 | 0.306 |
| HCM Control Delay | 11.7 | 11 | 12.2 | 9.6 | 10.6 |
| HCM Lane LOS | B | B | B | A | B |
| HCM 95th-tile Q | 1.6 | 0.9 | 2.4 | 0.3 | 1.3 |

Intersection

Intersection Delay, s/veh 8.7

Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↖ ↗ | ↖ ↗ | 3 | 18 | 29 | 125 | 0 | ↖ ↗ | 31 | 51 | 68 | 21 |
| Traffic Vol, veh/h | 17 | 42 | 3 | 18 | 29 | 125 | 0 | 49 | 31 | 51 | 68 | 21 |
| Future Vol, veh/h | 17 | 42 | 3 | 18 | 29 | 125 | 0 | 49 | 31 | 51 | 68 | 21 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, % | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 19 |
| Mvmt Flow | 18 | 46 | 3 | 20 | 32 | 136 | 0 | 53 | 34 | 55 | 74 | 23 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 1 |
| Approach | EB | | WB | | | NB | | SB | | | | |
| Opposing Approach | WB | | EB | | | SB | | NB | | | | |
| Opposing Lanes | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Left | SB | | NB | | | EB | | WB | | | | |
| Conflicting Lanes Left | 2 | | 2 | | | 2 | | 2 | | | | |
| Conflicting Approach Right | NB | | SB | | | WB | | EB | | | | |
| Conflicting Lanes Right | 2 | | 2 | | | 2 | | 2 | | | | |
| HCM Control Delay | 8.5 | | 8.6 | | | 8.1 | | 9.2 | | | | |
| HCM LOS | A | | A | | | A | | A | | | | |

| Lane | NBLn1 | NBLn2 | EBln1 | EBln2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, % | 0% | 0% | 100% | 0% | 100% | 0% | 43% | 0% |
| Vol Thru, % | 100% | 35% | 0% | 93% | 0% | 19% | 57% | 0% |
| Vol Right, % | 0% | 65% | 0% | 7% | 0% | 81% | 0% | 100% |
| Sign Control | Stop |
| Traffic Vol by Lane | 33 | 47 | 17 | 45 | 18 | 154 | 119 | 21 |
| LT Vol | 0 | 0 | 17 | 0 | 18 | 0 | 51 | 0 |
| Through Vol | 33 | 16 | 0 | 42 | 0 | 29 | 68 | 0 |
| RT Vol | 0 | 31 | 0 | 3 | 0 | 125 | 0 | 21 |
| Lane Flow Rate | 36 | 51 | 18 | 49 | 20 | 167 | 129 | 23 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.052 | 0.069 | 0.03 | 0.071 | 0.031 | 0.214 | 0.194 | 0.029 |
| Departure Headway (Hd) | 5.309 | 4.813 | 5.792 | 5.242 | 5.685 | 4.612 | 5.413 | 4.512 |
| Convergence, Y/N | Yes |
| Cap | 673 | 742 | 618 | 682 | 630 | 778 | 662 | 792 |
| Service Time | 3.051 | 2.555 | 3.531 | 2.981 | 3.417 | 2.344 | 3.152 | 2.25 |
| HCM Lane V/C Ratio | 0.053 | 0.069 | 0.029 | 0.072 | 0.032 | 0.215 | 0.195 | 0.029 |
| HCM Control Delay | 8.3 | 7.9 | 8.7 | 8.4 | 8.6 | 8.6 | 9.5 | 7.4 |
| HCM Lane LOS | A | A | A | A | A | A | A | A |
| HCM 95th-tile Q | 0.2 | 0.2 | 0.1 | 0.2 | 0.1 | 0.8 | 0.7 | 0.1 |

| Intersection | | | | | | | | | | | | | | | |
|--------------------------|--------|-------|--------|------|--------|------|--------|-------|------|------|------|------|--|--|--|
| Int Delay, s/veh | 8.9 | | | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | |
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | | | |
| Traffic Vol, veh/h | 66 | 202 | 22 | 60 | 94 | 91 | 25 | 13 | 102 | 106 | 13 | 53 | | | |
| Future Vol, veh/h | 66 | 202 | 22 | 60 | 94 | 91 | 25 | 13 | 102 | 106 | 13 | 53 | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | | | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | | | |
| Storage Length | 300 | - | - | 350 | - | - | - | - | - | - | - | - | | | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | | | |
| Heavy Vehicles, % | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Mvmt Flow | 72 | 220 | 24 | 65 | 102 | 99 | 27 | 14 | 111 | 115 | 14 | 58 | | | |
| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | | | | |
| Conflicting Flow All | 201 | 0 | 0 | 244 | 0 | 0 | 694 | 707 | 232 | 721 | 670 | 152 | | | |
| Stage 1 | - | - | - | - | - | - | 376 | 376 | - | 282 | 282 | - | | | |
| Stage 2 | - | - | - | - | - | - | 318 | 331 | - | 439 | 388 | - | | | |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | | | |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | | |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 | | | |
| Pot Cap-1 Maneuver | 1383 | - | - | 1334 | - | - | 360 | 363 | 812 | 345 | 381 | 900 | | | |
| Stage 1 | - | - | - | - | - | - | 649 | 620 | - | 729 | 681 | - | | | |
| Stage 2 | - | - | - | - | - | - | 698 | 649 | - | 601 | 612 | - | | | |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - | | | |
| Mov Cap-1 Maneuver | 1383 | - | - | 1334 | - | - | 302 | 327 | 812 | 267 | 344 | 900 | | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 302 | 327 | - | 267 | 344 | - | | | |
| Stage 1 | - | - | - | - | - | - | 615 | 588 | - | 691 | 648 | - | | | |
| Stage 2 | - | - | - | - | - | - | 608 | 617 | - | 480 | 580 | - | | | |
| Approach | EB | | | WB | | | NB | | | SB | | | | | |
| HCM Control Delay, s | 1.8 | | | 1.9 | | | 13.7 | | | 26.7 | | | | | |
| HCM LOS | | | | | | | B | | | D | | | | | |
| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | | | | | |
| Capacity (veh/h) | 564 | 1383 | - | - | 1334 | - | - | 348 | | | | | | | |
| HCM Lane V/C Ratio | 0.27 | 0.052 | - | - | 0.049 | - | - | 0.537 | | | | | | | |
| HCM Control Delay (s) | 13.7 | 7.7 | - | - | 7.8 | - | - | 26.7 | | | | | | | |
| HCM Lane LOS | B | A | - | - | A | - | - | D | | | | | | | |
| HCM 95th %tile Q(veh) | 1.1 | 0.2 | - | - | 0.2 | - | - | 3 | | | | | | | |

| Intersection | | | | | | |
|--------------------------|--------|--------|--------|------|-------|-------|
| Int Delay, s/veh | 11.1 | | | | | |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 97 | 675 | 439 | 55 | 87 | 61 |
| Future Vol, veh/h | 97 | 675 | 439 | 55 | 87 | 61 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | - | 0 | 0 | - | 0 | - |
| Grade, % | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 105 | 734 | 477 | 60 | 95 | 66 |
| Major/Minor | Major1 | Major2 | Minor2 | | | |
| Conflicting Flow All | 537 | 0 | - | 0 | 1451 | 507 |
| Stage 1 | - | - | - | - | 507 | - |
| Stage 2 | - | - | - | - | 944 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1031 | - | - | - | 144 | 566 |
| Stage 1 | - | - | - | - | 605 | - |
| Stage 2 | - | - | - | - | 378 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 1031 | - | - | - | 119 | 566 |
| Mov Cap-2 Maneuver | - | - | - | - | 119 | - |
| Stage 1 | - | - | - | - | 501 | - |
| Stage 2 | - | - | - | - | 378 | - |
| Approach | EB | WB | SB | | | |
| HCM Control Delay, s | 1.1 | 0 | 99.9 | | | |
| HCM LOS | | | F | | | |
| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 | |
| Capacity (veh/h) | 1031 | - | - | - | 176 | |
| HCM Lane V/C Ratio | 0.102 | - | - | - | 0.914 | |
| HCM Control Delay (s) | 8.9 | 0 | - | - | 99.9 | |
| HCM Lane LOS | A | A | - | - | F | |
| HCM 95th %tile Q(veh) | 0.3 | - | - | - | 6.9 | |

LANE SUMMARY

Site: Poupart / Site Access PM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 173 | 3.0 | 225 | 0.767 | 100 | 33.9 | LOS C | 4.7 | 36.4 | Full | 500 | 0.0 | 0.0 |
| Approach | 173 | 3.0 | | 0.767 | | 33.9 | LOS C | 4.7 | 36.4 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 | 540 | 3.0 | 917 | 0.589 | 100 | 8.2 | LOS A | 4.7 | 36.7 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 540 | 3.0 | 917 | 0.589 | 100 | 7.6 | LOS A | 4.7 | 36.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 1079 | 3.0 | | 0.589 | | 7.9 | LOS A | 4.7 | 36.7 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 150 | 3.0 | 416 | 0.360 | 100 | 11.5 | LOS B | 1.7 | 12.9 | Full | 500 | 0.0 | 0.0 |
| Approach | 150 | 3.0 | | 0.360 | | 11.5 | LOS B | 1.7 | 12.9 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 | 1004 | 3.0 | 1138 | 0.882 | 100 | 7.2 | LOS A | 16.2 | 126.6 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 1004 | 3.0 | 1138 | 0.882 | 100 | 6.1 | LOS A | 16.2 | 126.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 2009 | 3.0 | | 0.882 | | 6.6 | LOS A | 16.2 | 126.6 | | | | |
| Intersection | 3411 | 3.0 | | 0.882 | | 8.6 | LOS A | 16.2 | 126.6 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: Poupart Extension PM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| East: Poupart | | | | | | | | | | | | | |
| Lane 1 | 619 | 3.0 | 1197 | 0.517 | 100 | 4.4 | LOS A | 4.7 | 36.7 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 619 | 3.0 | 1197 | 0.517 | 100 | 4.4 | LOS A | 4.7 | 36.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 1238 | 3.0 | | 0.517 | | 4.4 | LOS A | 4.7 | 36.7 | | | | |
| North: Poupart | | | | | | | | | | | | | |
| Lane 1 ^d | 382 | 3.0 | 533 | 0.715 | 100 | 21.2 | LOS C | 5.0 | 39.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 382 | 3.0 | | 0.715 | | 21.2 | LOS C | 5.0 | 39.3 | | | | |
| West: Poupart Extension | | | | | | | | | | | | | |
| Lane 1 | 821 | 3.0 | 871 | 0.943 | 100 | 21.5 | LOS C | 21.6 | 168.7 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 821 | 3.0 | 871 | 0.943 | 100 | 21.3 | LOS C | 21.6 | 168.7 | Full | 500 | 0.0 | 0.0 |
| Approach | 1642 | 3.0 | | 0.943 | | 21.4 | LOS C | 21.6 | 168.7 | | | | |
| Intersection | 3262 | 3.0 | | 0.943 | | 14.9 | LOS B | 21.6 | 168.7 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Dr Corbeil PM (Ultimate)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|--------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. % | Block. % |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 518 | 3.0 | 753 | 0.689 | 100 | 11.4 | LOS B | 7.7 | 59.8 | Full | 500 | 0.0 | 0.0 |
| Approach | 518 | 3.0 | | 0.689 | | 11.4 | LOS B | 7.7 | 59.8 | | | | |
| East: Dr. Corbeil | | | | | | | | | | | | | |
| Lane 1 ^d | 311 | 3.0 | 735 | 0.423 | 100 | 9.5 | LOS A | 2.9 | 22.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 311 | 3.0 | | 0.423 | | 9.5 | LOS A | 2.9 | 22.6 | | | | |
| North: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 735 | 3.0 | 976 | 0.753 | 100 | 8.9 | LOS A | 9.7 | 75.5 | Full | 500 | 0.0 | 0.0 |
| Approach | 735 | 3.0 | | 0.753 | | 8.9 | LOS A | 9.7 | 75.5 | | | | |
| Intersection | 1564 | 3.0 | | 0.753 | | 9.9 | LOS A | 9.7 | 75.5 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 Site: St-Jean / Morris Village Access PM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|-------------------------------------|--------------|------|------------|----------|---------|-----------|----------|-------------|--------|--------|----------|--------|----------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total veh/h | HV % | Cap. veh/h | Satn v/c | Util. % | Delay sec | Service | Veh | Dist m | Config | Length m | Adj. % | Block. % |
| South: Morris Village Access | | | | | | | | | | | | | |
| Lane 1 ^d | 586 | 3.0 | 1009 | 0.581 | 100 | 14.2 | LOS B | 5.3 | 41.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 79 | 3.0 | 1009 | 0.079 | 100 | 5.5 | LOS A | 0.4 | 3.4 | Short | 60 | 0.0 | NA |
| Approach | 665 | 3.0 | | 0.581 | | 13.1 | LOS B | 5.3 | 41.4 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 225 | 3.0 | 703 | 0.320 | 100 | 12.3 | LOS B | 2.2 | 16.8 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 260 | 3.0 | 814 | 0.320 | 100 | 6.9 | LOS A | 2.3 | 17.8 | Short | 60 | 0.0 | NA |
| Approach | 485 | 3.0 | | 0.320 | | 9.4 | LOS A | 2.3 | 17.8 | | | | |
| West: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 413 | 3.0 | 1225 | 0.337 | 100 | 4.3 | LOS A | 2.4 | 19.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 945 | 3.0 | 1225 | 0.771 | 100 | 5.8 | LOS A | 10.6 | 82.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 1358 | 3.0 | | 0.771 | | 5.4 | LOS A | 10.6 | 82.6 | | | | |
| Intersection | 2508 | 3.0 | | 0.771 | | 8.2 | LOS A | 10.6 | 82.6 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

Site: St-Jean / Poupart PM (Build-out)

New Site
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|---------------------------|--------------|-----|-------|-------|-------|---------|----------|-------------|-------|--------|--------|------|--------|
| | Demand Flows | | | Deg. | Lane | Average | Level of | 95% Back of | Queue | Lane | Lane | Cap. | Prob. |
| | Total | HV | Cap. | Satn | Util. | Delay | Service | Veh | Dist | Config | Length | Adj. | Block. |
| | veh/h | % | veh/h | v/c | % | sec | | | m | | m | % | % |
| South: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 477 | 3.0 | 471 | 1.012 | 100 | 53.1 | LOS F | 18.5 | 144.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 433 | 3.0 | 559 | 0.774 | 100 | 15.1 | LOS B | 7.0 | 54.4 | Short | 60 | 0.0 | NA |
| Approach | 910 | 3.0 | | 1.012 | | 35.0 | LOS D | 18.5 | 144.0 | | | | |
| East: St-Jean | | | | | | | | | | | | | |
| Lane 1 ^d | 455 | 3.0 | 659 | 0.691 | 100 | 17.6 | LOS B | 6.9 | 54.1 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 459 | 3.0 | 664 | 0.691 | 100 | 13.5 | LOS B | 7.0 | 54.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 914 | 3.0 | | 0.691 | | 15.5 | LOS B | 7.0 | 54.3 | | | | |
| North: Site Access | | | | | | | | | | | | | |
| Lane 1 ^d | 158 | 3.0 | 358 | 0.440 | 100 | 14.7 | LOS B | 2.3 | 17.6 | Full | 500 | 0.0 | 0.0 |
| Approach | 158 | 3.0 | | 0.440 | | 14.7 | LOS B | 2.3 | 17.6 | | | | |
| West: Poupart | | | | | | | | | | | | | |
| Lane 1 | 826 | 3.0 | 862 | 0.958 | 100 | 25.2 | LOS C | 23.5 | 183.3 | Full | 500 | 0.0 | 0.0 |
| Lane 2 ^d | 826 | 3.0 | 862 | 0.958 | 100 | 24.1 | LOS C | 23.5 | 183.3 | Full | 500 | 0.0 | 0.0 |
| Approach | 1652 | 3.0 | | 0.958 | | 24.7 | LOS C | 23.5 | 183.3 | | | | |
| Intersection | 3634 | 3.0 | | 1.012 | | 24.5 | LOS C | 23.5 | 183.3 | | | | |

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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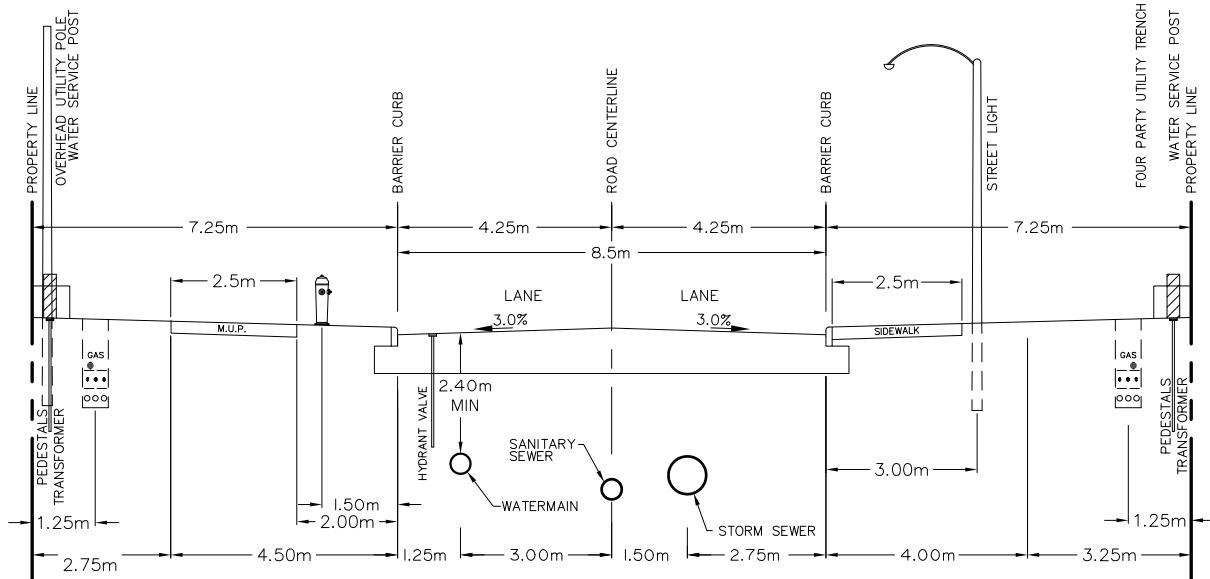
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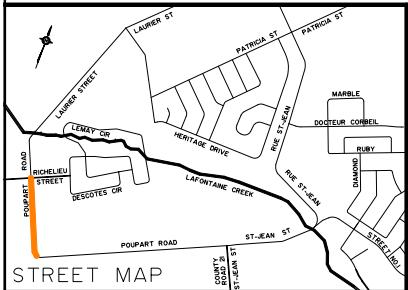
APPENDIX “C”

Typical Cross-Sections

- 180801-CS1 – Proposed undivided 23.0m R.O.W. (Poupart)
- 180801-CS2 - Proposed 30.0m divided R.O.W. (Poupart)
- 180801-CS3 - Proposed 30.0m undivided R.O.W. (St-Jean)
- 180801-CS4 - Proposed 26.0m undivided R.O.W. (Morris Village)
- 180801-CS5 - Proposed 26.0m undivided R.O.W. (St-Jean)



PROPOSED 23.0 METRE R.O.W.
POUPART AT WALMART

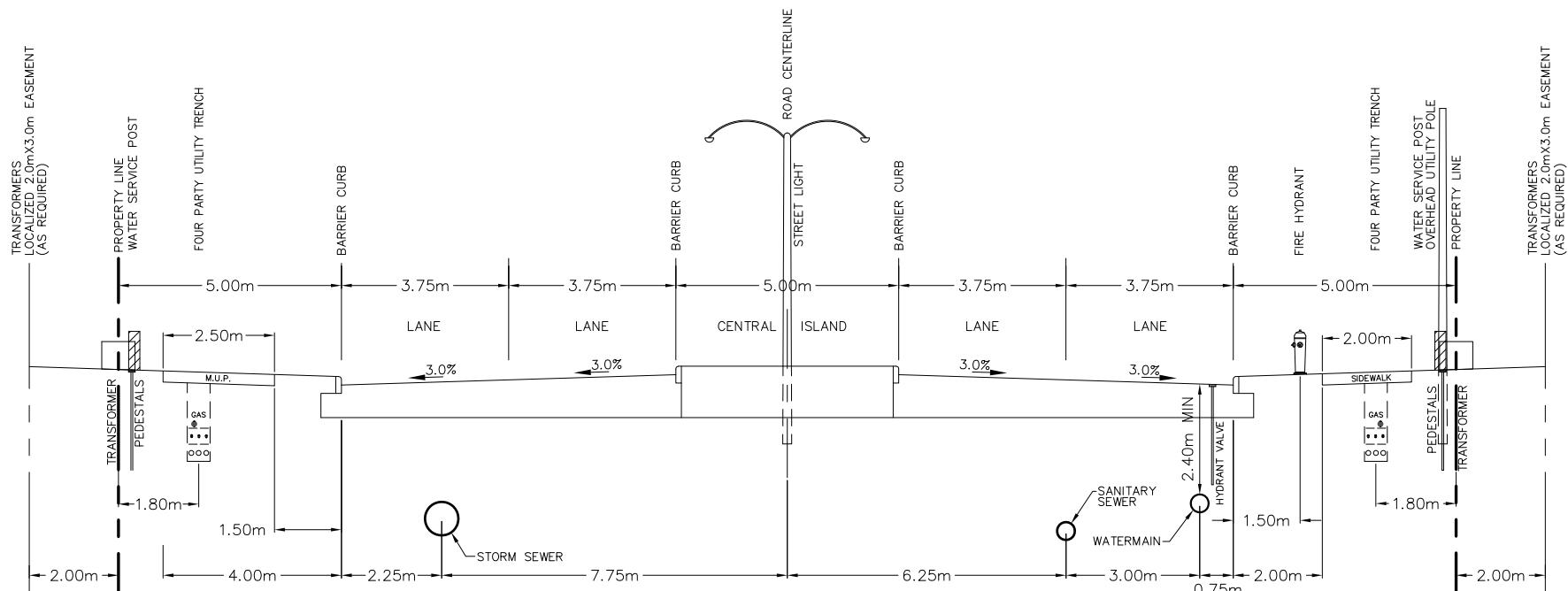


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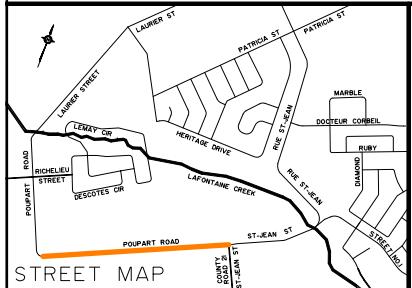
CITY OF CLARENCE-ROCKLAND
MORRIS/ROCKLAND
ROAD CROSS-SECTIONS

PLAN
PROPOSED 23.0m R.O.W.
POUPART AT WALMART

| | |
|-------------|---------------|
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| PROJECT No. | I80801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I80801-CSI |



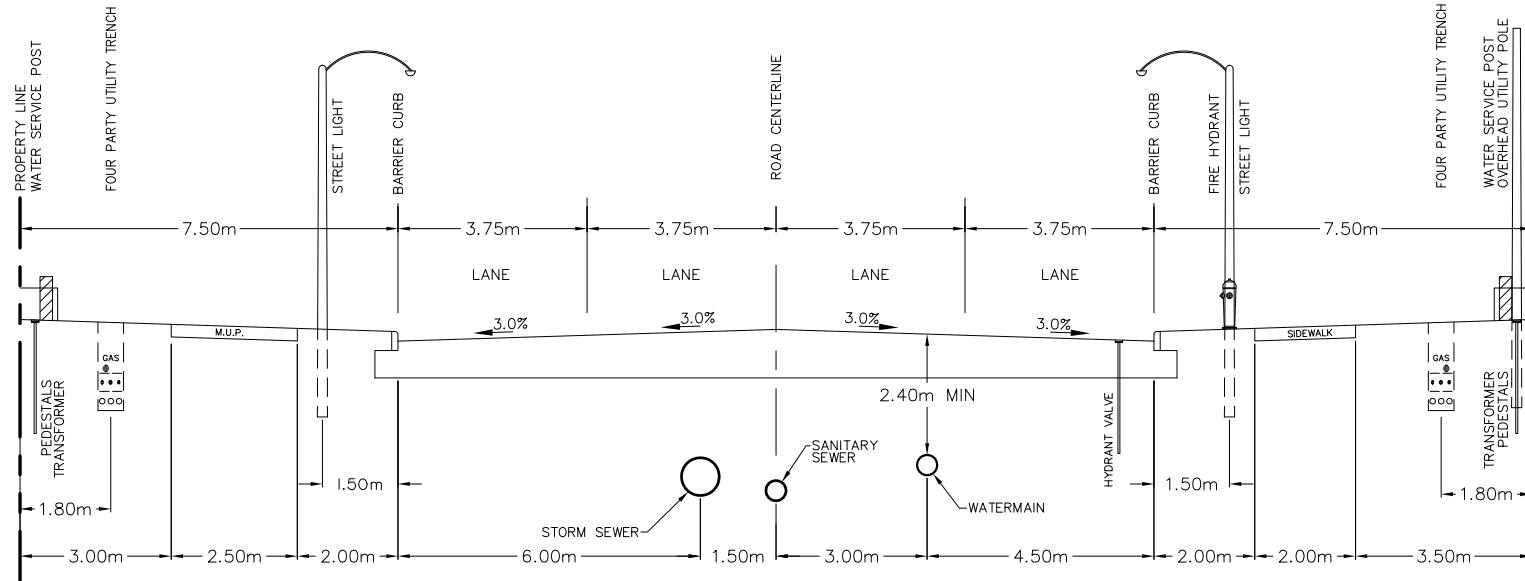
PROPOSED 30.0 METRE R.O.W.
DIVIDED



SCALE:
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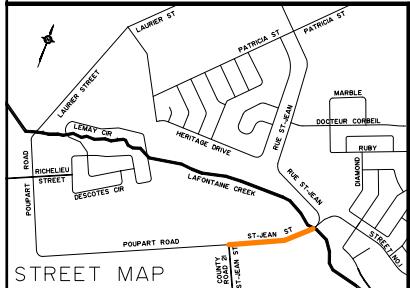
**CITY OF CLARENCE-ROCKLAND
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ROAD CROSS-SECTIONS**

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I8080I |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I8080I-CS2 |



PROPOSED 30.0 METRE R.O.W. - UNDIVIDED

ST-JEAN - HILL

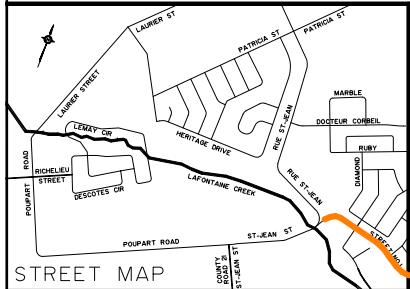
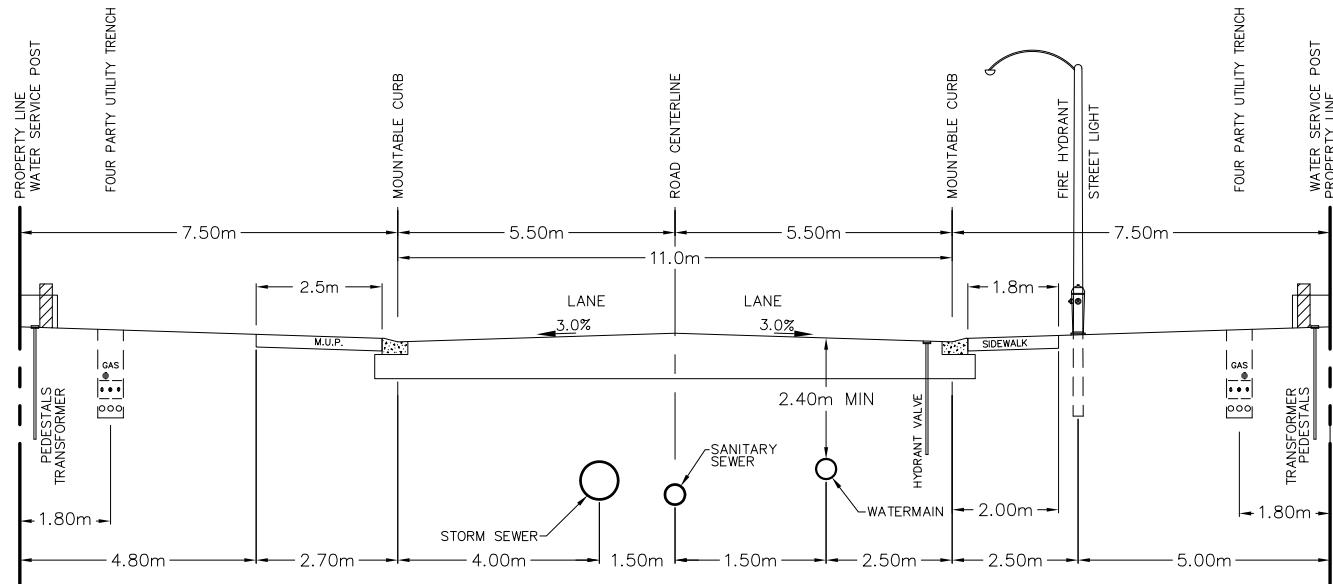


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I : 150
1.5m 0 1.5 3.0 4.5m

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MORRIS/ROCKLAND
ROAD CROSS-SECTIONS

PLAN
PROPOSED 30.0m R.O.W.
ST-JEAN HILL

| | |
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| CLIENT No. | III |
| PROJECT No. | I80801 |
| DATE | OCTOBER, 2018 |
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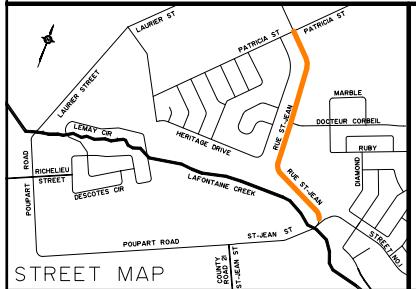
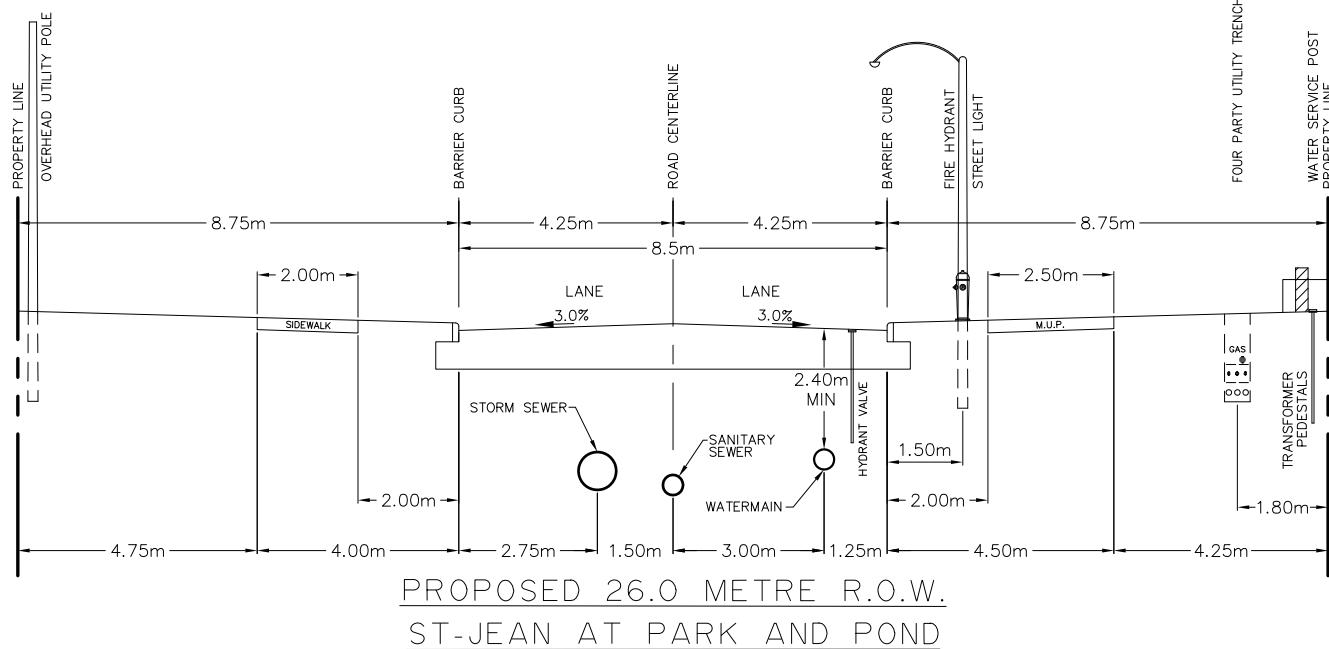


SCALE:
I : 150
1.5m 0 1.5 3.0 4.5m

CITY OF CLARENCE-ROCKLAND
MORRIS/ROCKLAND
ROAD CROSS-SECTIONS

PLAN
PROPOSED 26.0m R.O.W.
STREET No.1 (MORRIS VILLAGE)

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I80801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I80801-CS4 |



SCALE:
1 : 150
1.5m 0 1.5 3.0 4.5m

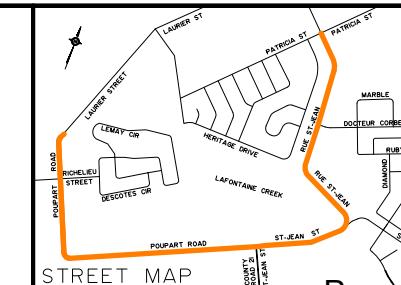
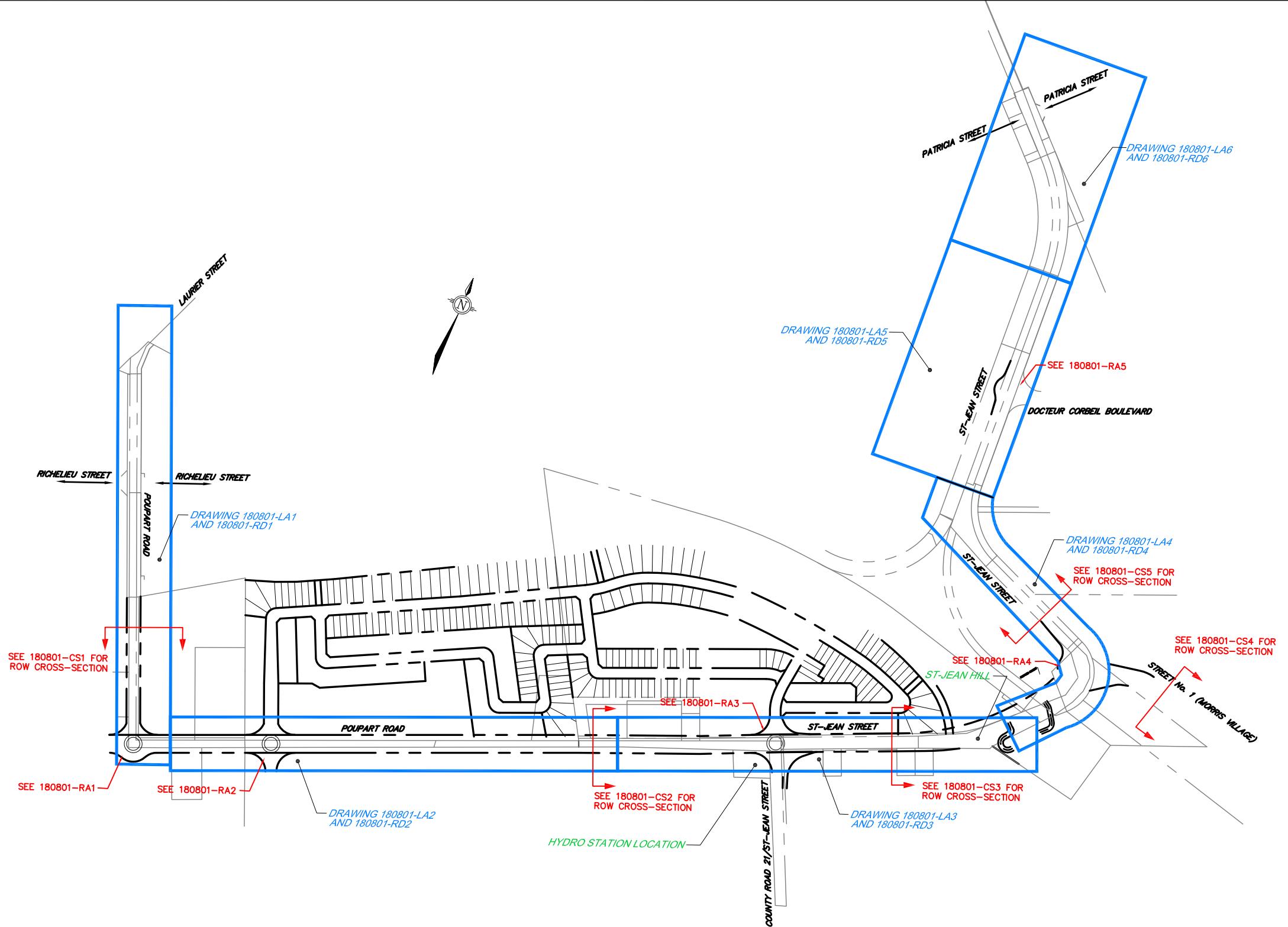
CITY OF CLARENCE-ROCKLAND
MORRIS/ROCKLAND
ROAD CROSS-SECTIONS

PLAN
PROPOSED 26.0m R.O.W.
ST-JEAN AT PARK AND POND

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I8080I |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I8080I-CS5 |

APPENDIX “D”

Reference Plan – 180801-RP1



ATREL Engineering Ltd.
Engineers - Ingénieurs

CITY OF CLARENCE-ROCKLAND
POUPART RD/ ST-JEAN ST

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | 180801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | 180801-RPI |

SCALE:
N.T.S.

PLAN
REFERENCE PLAN

APPENDIX “E”

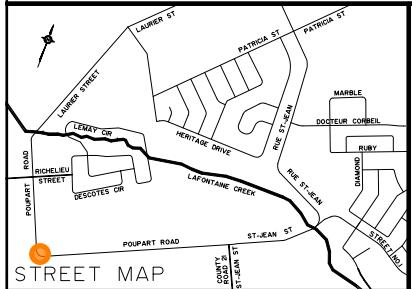
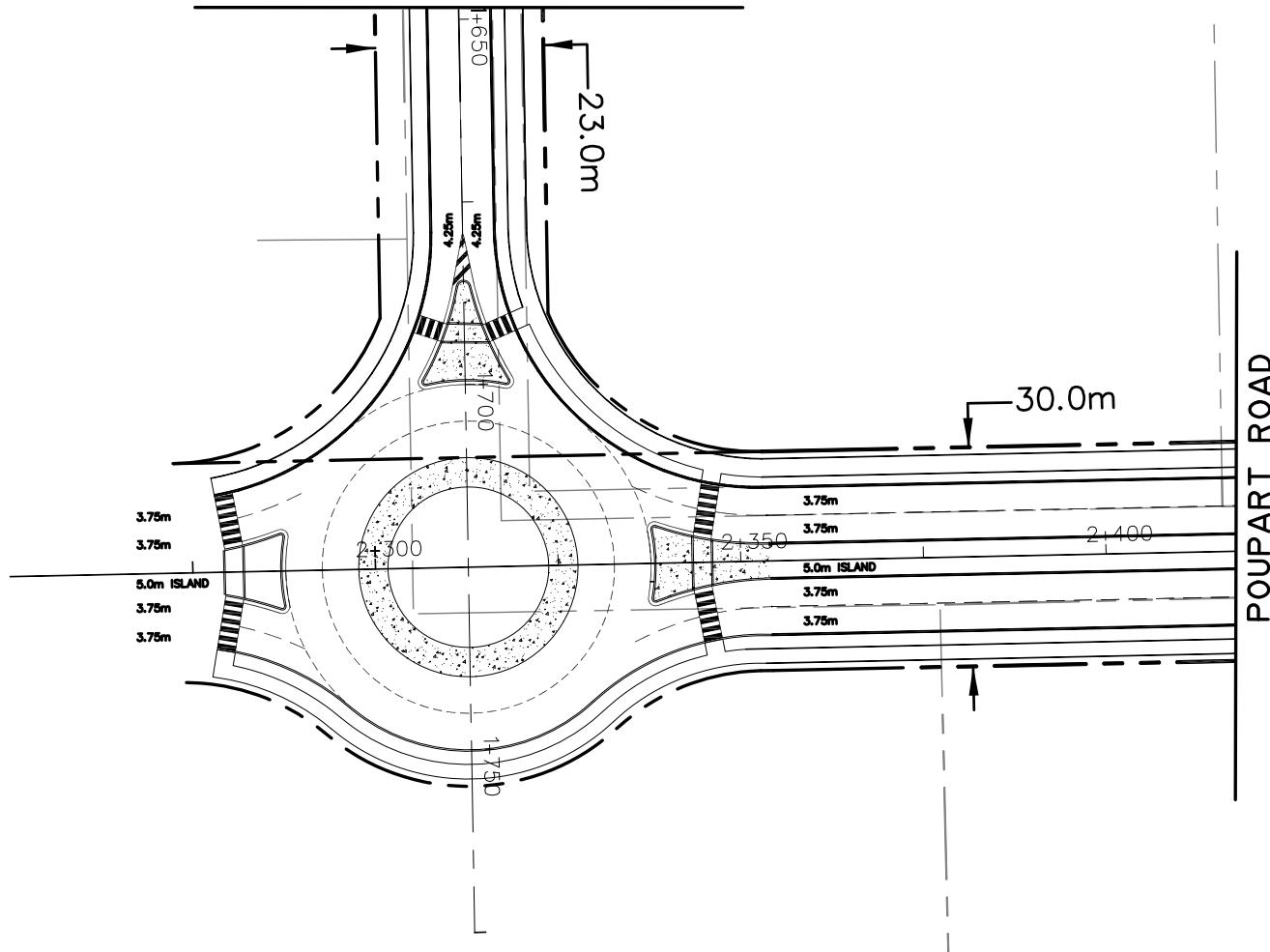
Roundabout Schematic Plans

- 180801-RA1 (Poupart)
- 180801-RA2 (Poupart/Brigil)
- 180801-RA3 (Poupart/Brigil/St-Jean)
- 180801-RA4 (St-Jean/Morris)
- 180801-RA5 (St-Jean/Dr. Corbeil)

POUPART EXTENSION



POUPART ROAD



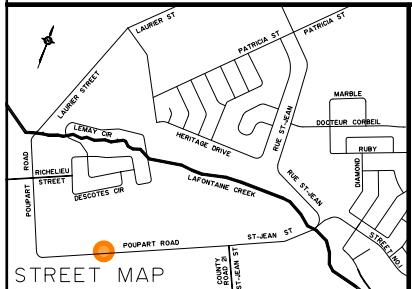
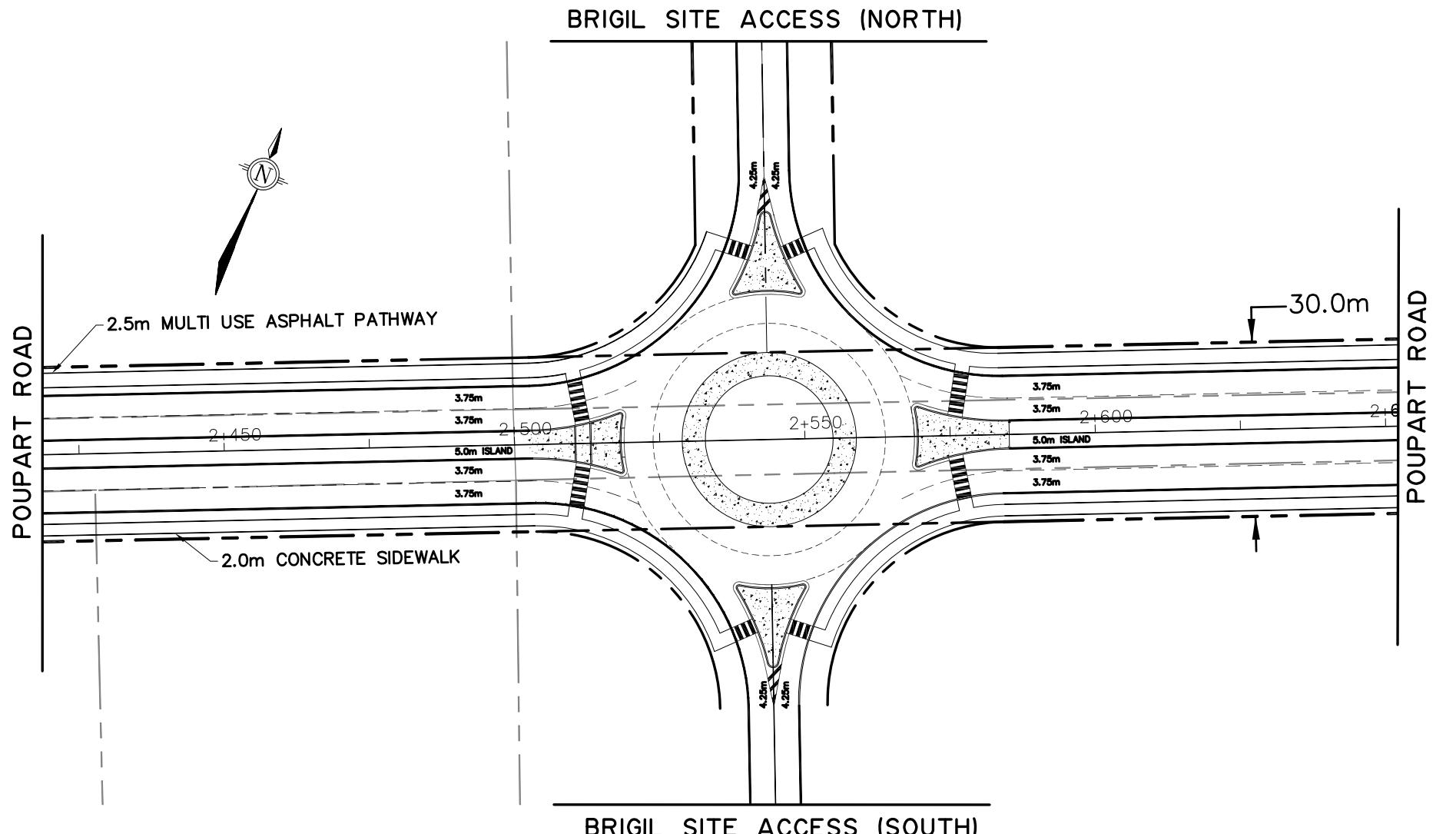
 **ATREL Engineering Ltd.**
Engineers - Ingénieurs

SCALE: 1 : 1000
10m 0 10 20 30m

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
ROUNDABOUT SCHEMATIC

PLAN
INTERSECTION AT POUPART ROAD
EXTENSION

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I80801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I80801-RAI |



 **ATREL Engineering Ltd.**
Engineers - Ingénieurs

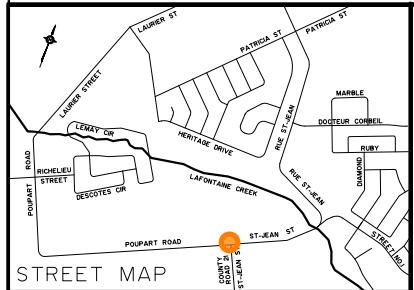
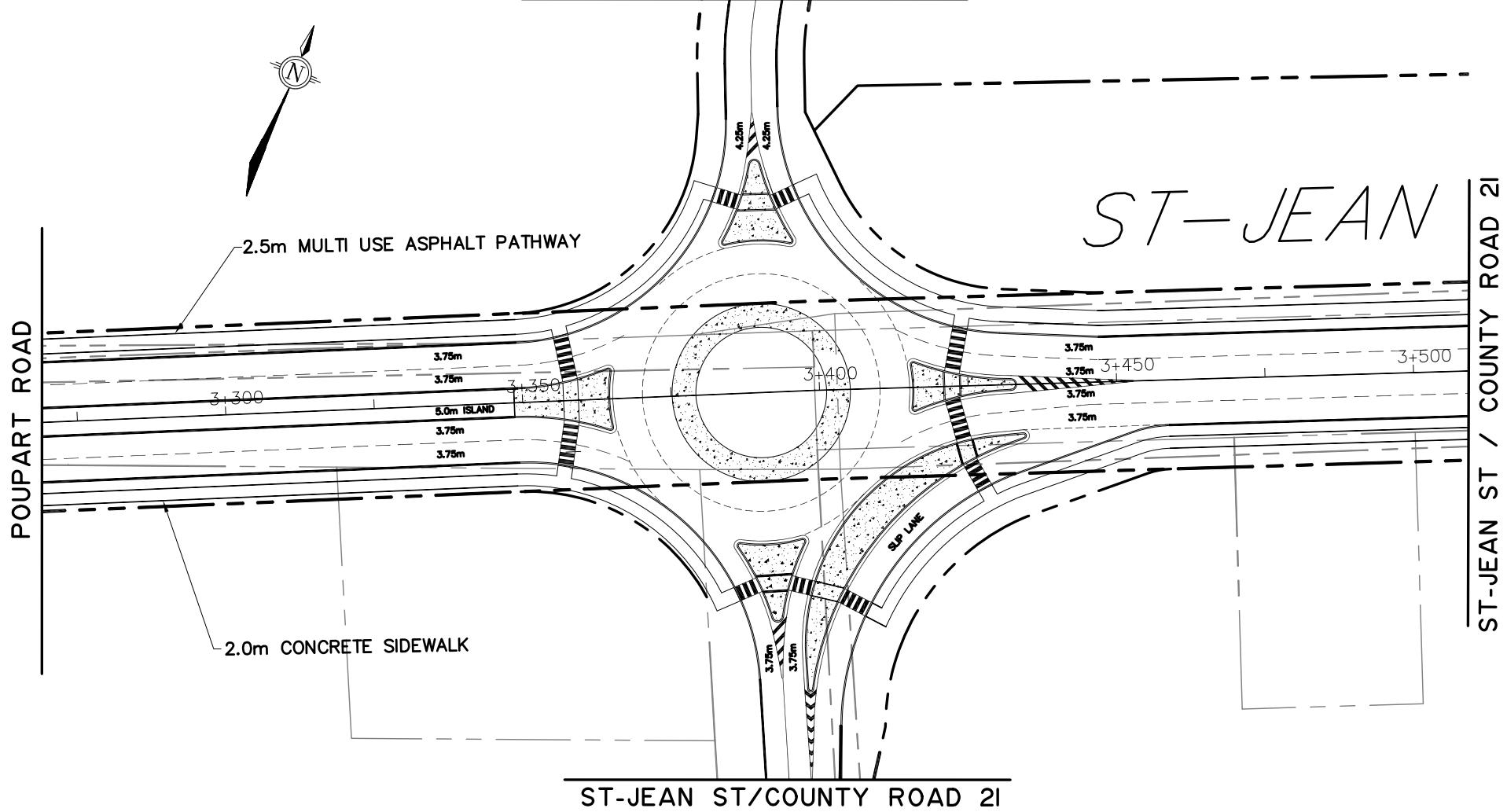
SCALE: 1 : 1000
 10m 0 10 20 30m

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
ROUNDABOUT SCHEMATIC

PLAN
INTERSECTION AT POUPART ROAD
AND BRIGIL SITE ACCESS

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I80801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I80801-RA2 |

BRIGIL SITE ACCESS (NORTH)



SCALE: 1 : 1000

A scale bar with markings at 10m, 0, 10, 20, and 30m. The 0 mark is at the left end. The 10m mark is at the center of the first black segment. The 20m mark is at the center of the second black segment. The 30m mark is at the center of the third black segment. The segments are labeled with their respective values.

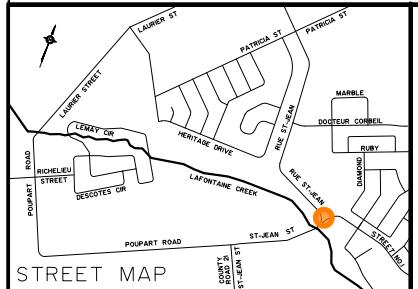
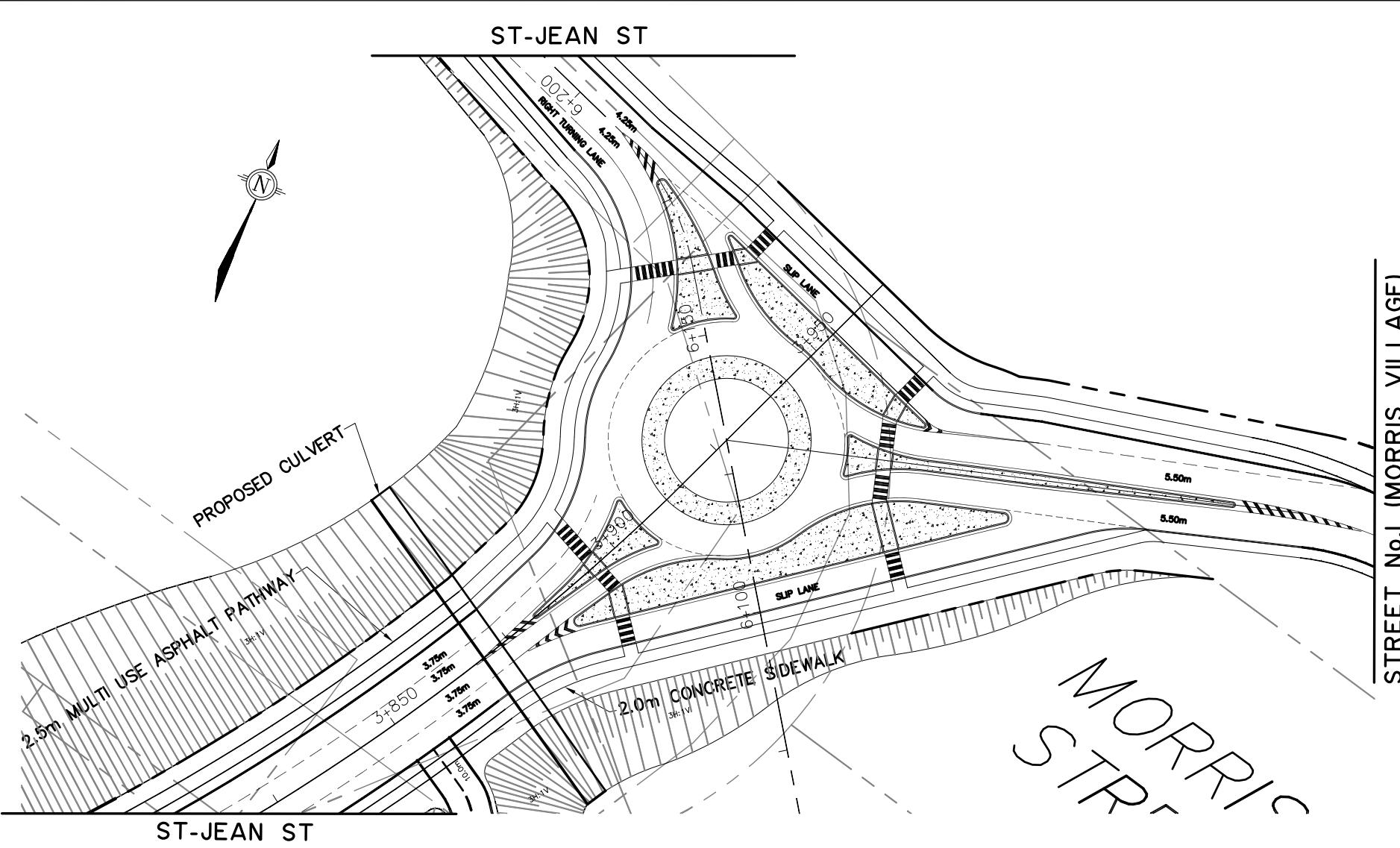
CITY OF CLARENCE-ROCKLAND

POUPART/ST-JEAN

ROUNDABOUT SCHEMATIC

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | 180801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | 180801-RA3 |

STREET No. I (MORRIS VILLAGE)



ATREL Engineering Ltd.
Engineers - Ingénieurs

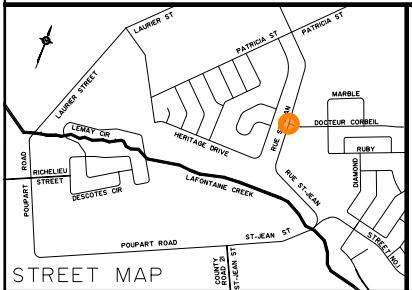
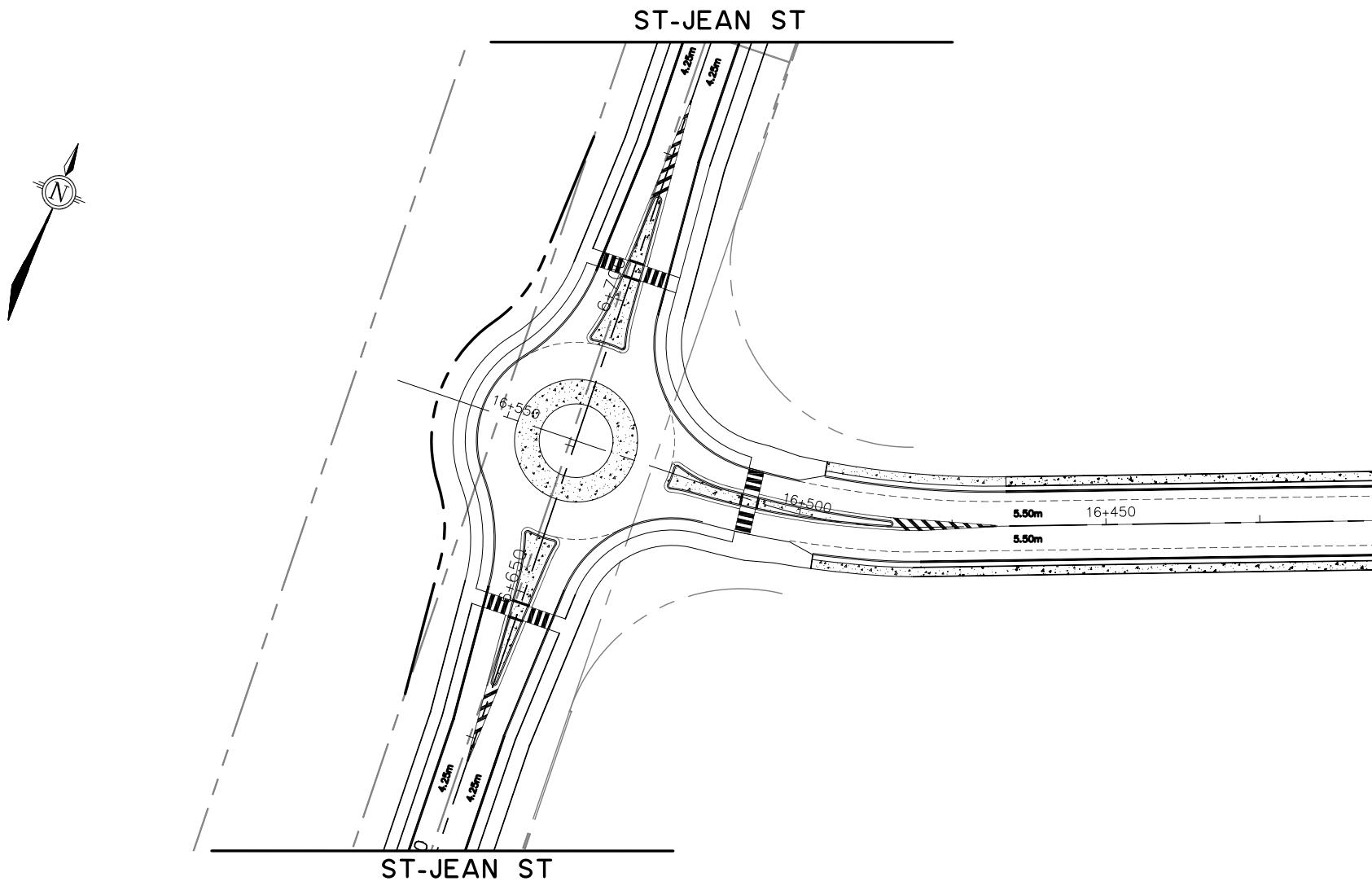
SCALE: 1 : 1000
10m 0 10 20 30m

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
ROUNABOUT SCHEMATIC

PLAN
INTERSECTION AT ST-JEAN STREET
AND STREET No. I (MORRIS VILLAGE)

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I8080I |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I8080I-RA4 |

DOCTEUR CORBEIL BOULEVARD



SCALE: 1 : 1000
 10m 0 10 20 30m

CITY OF CLARENCE-ROCKLAND
**POUPART/ST-JEAN
 ROUNDABOUT SCHEMATIC**

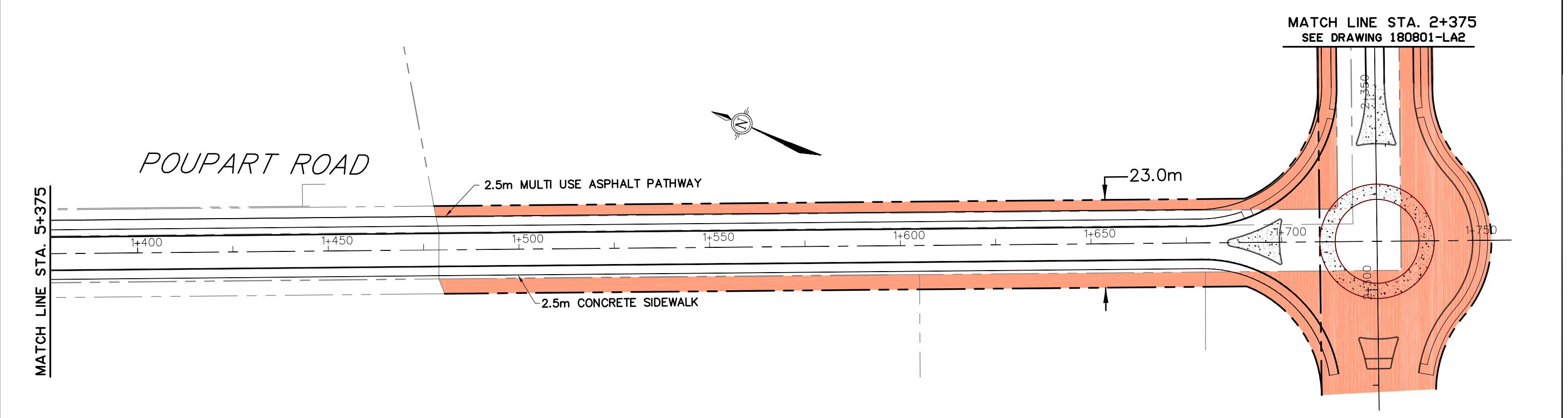
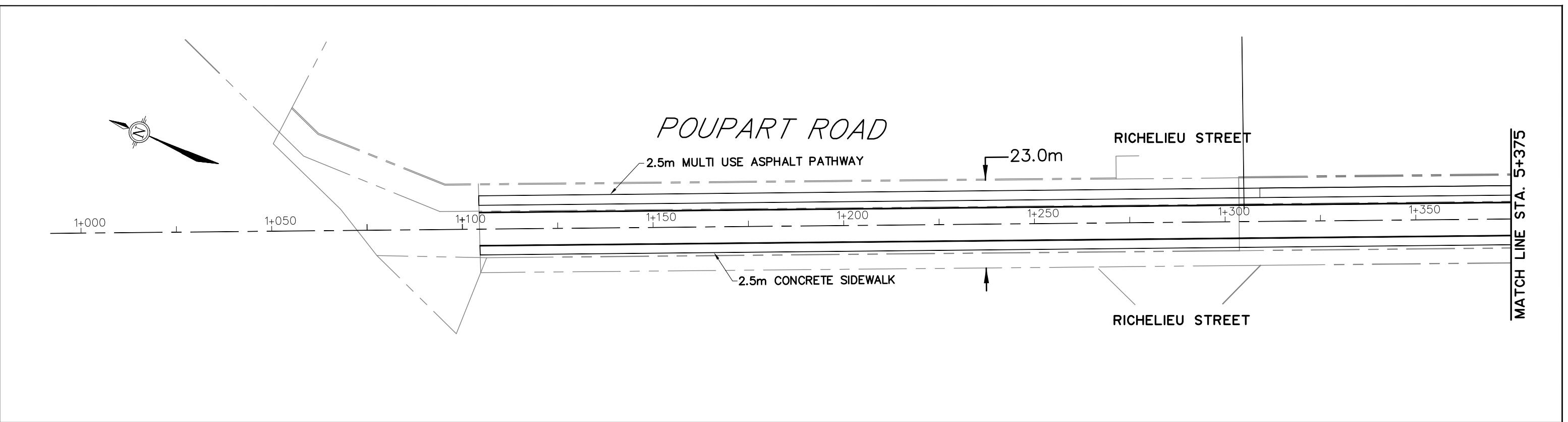
PLAN
 INTERSECTION AT ST-JEAN STREET
 AND DR CORBEIL BOULEVARD

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I8080I |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I8080I-RA5 |

APPENDIX “F”

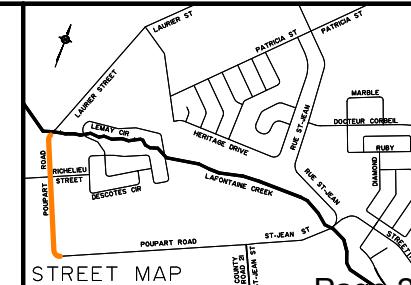
Land Acquisition Preliminary Plans

180801-LA1 (Poupart)
180801-LA2 (Poupart)
180801-LA3 (Poupart/St-Jean)
180801-LA4 (St-Jean)
180801-LA5 (St-Jean)
180801-LA6 (St-Jean)



NOTES:
1- EXACT RIGHT OF WAY (R.O.W.) WIDTH
"REQUIREMENT" TO BE SURVEYED BY OLS.

LEGEND:
LAND ACQUISITION REQUIREMENT



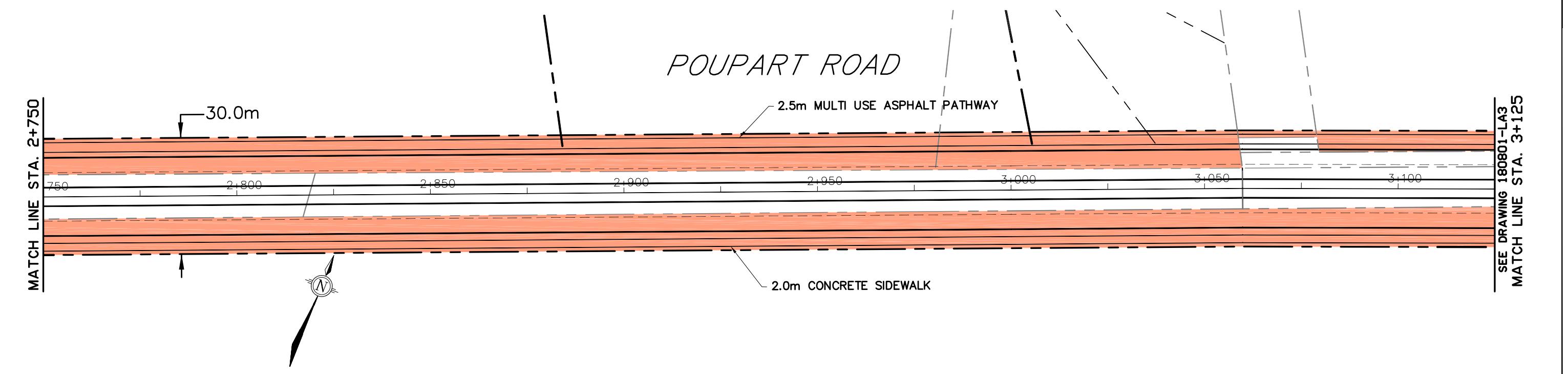
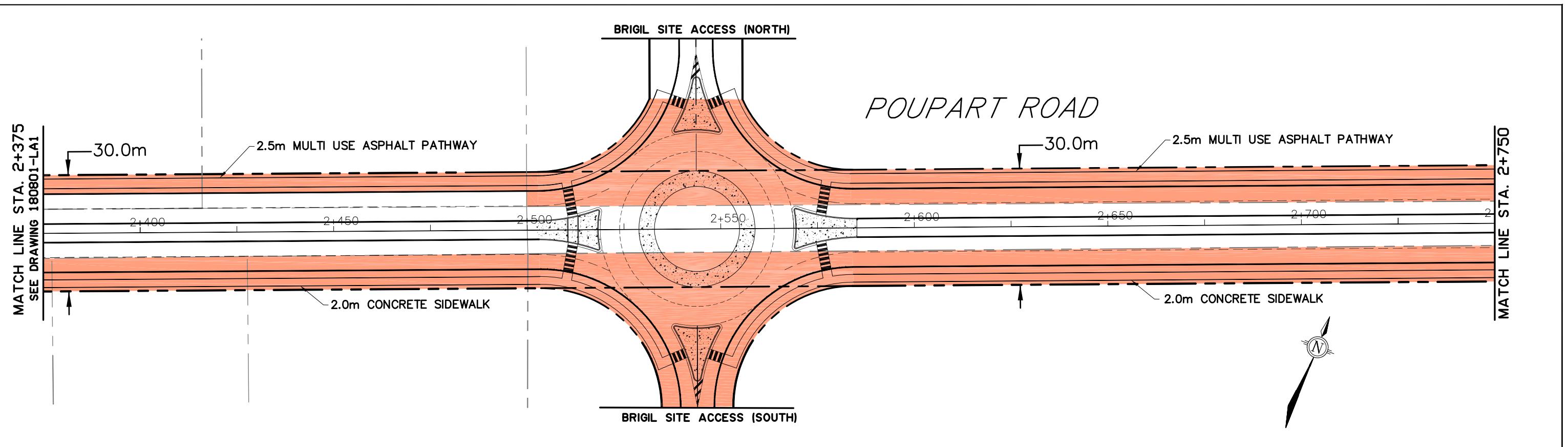
ATREL Engineering Ltd.
Engineers - Ingénieurs

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
LAND ACQUISITION PLAN

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | IB0801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | IB0801-LAI |

SCALE: 1 : 1000
10m 0 10 20 30m

PLAN
POUPART ROAD
STATION 1+000 TO STATION 2+375

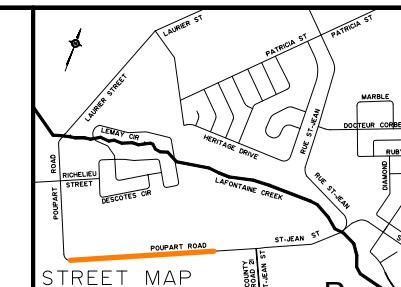


NOTES:

1- EXACT RIGHT OF WAY (R.O.W.) WIDTH
"REQUIREMENT" TO BE SURVEYED BY OLS.

LEGEND:

LAND ACQUISITION REQUIREMENT



ATREL Engineering Ltd.
Engineers - Ingénieurs

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
LAND ACQUISITION PLAN

CLIENT No.
III

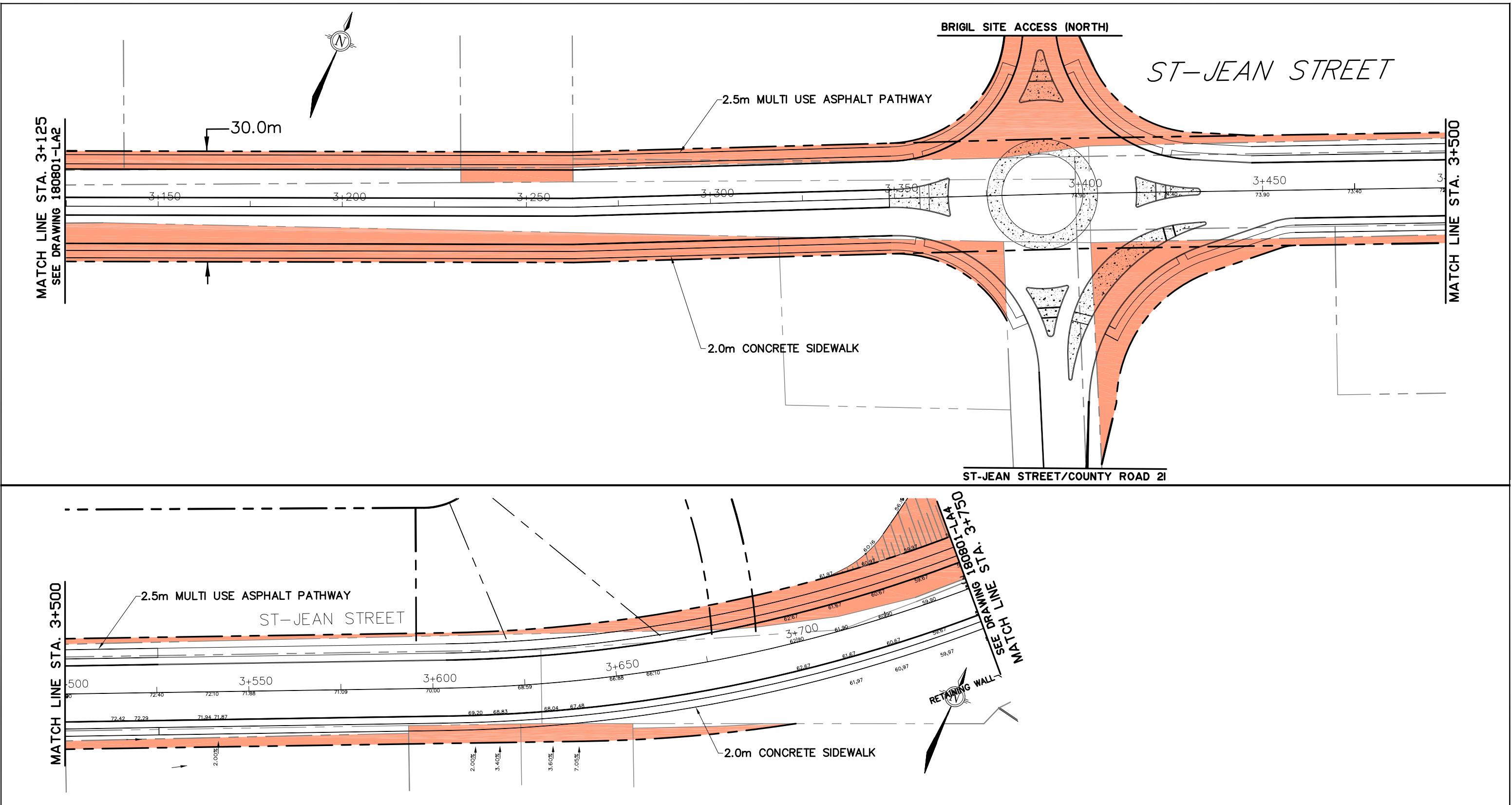
PROJECT No.
IB0801

DATE
OCTOBER, 2018

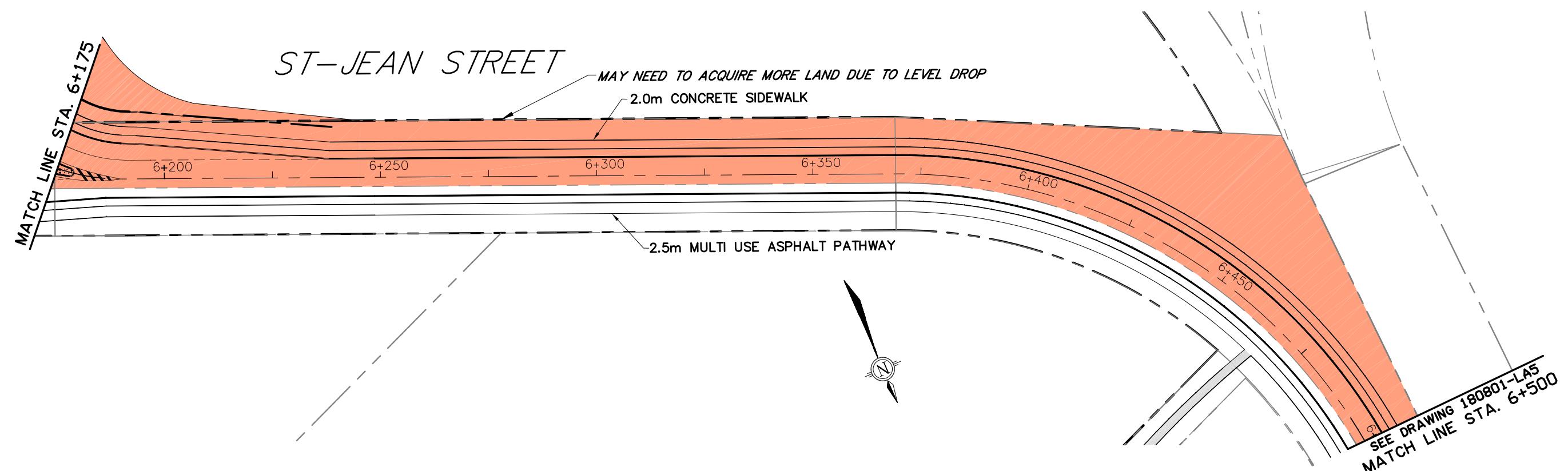
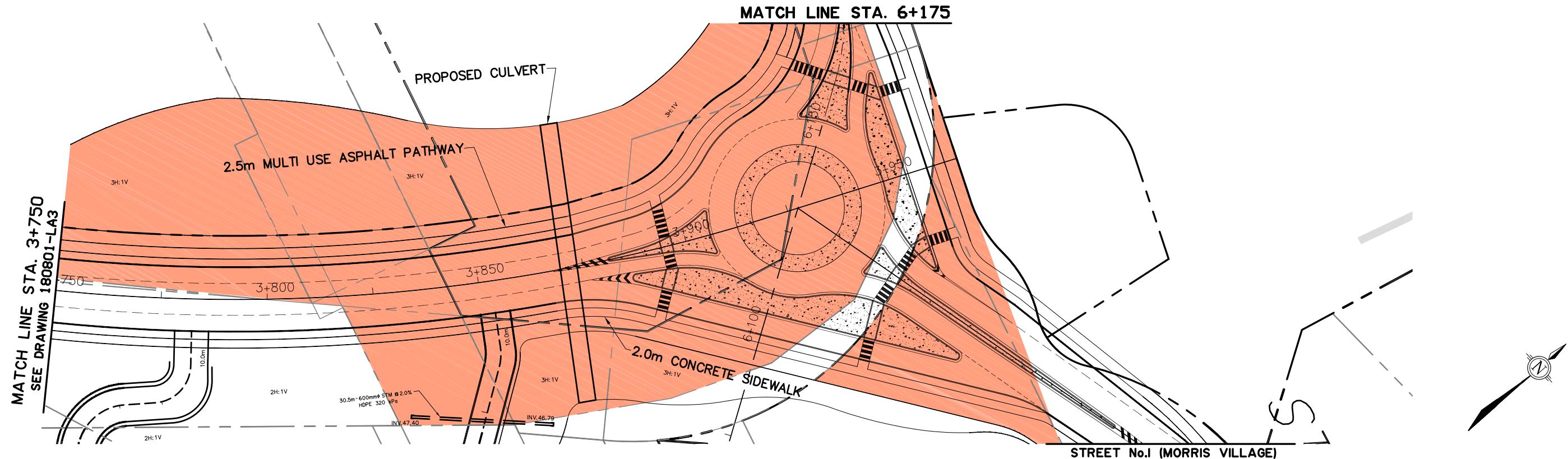
DRAWING No.
180801-LA2

SCALE:
1 : 1000
10m 0 10 20 30m

PLAN
POUPART ROAD
STATION 2+375 TO STATION 3+125



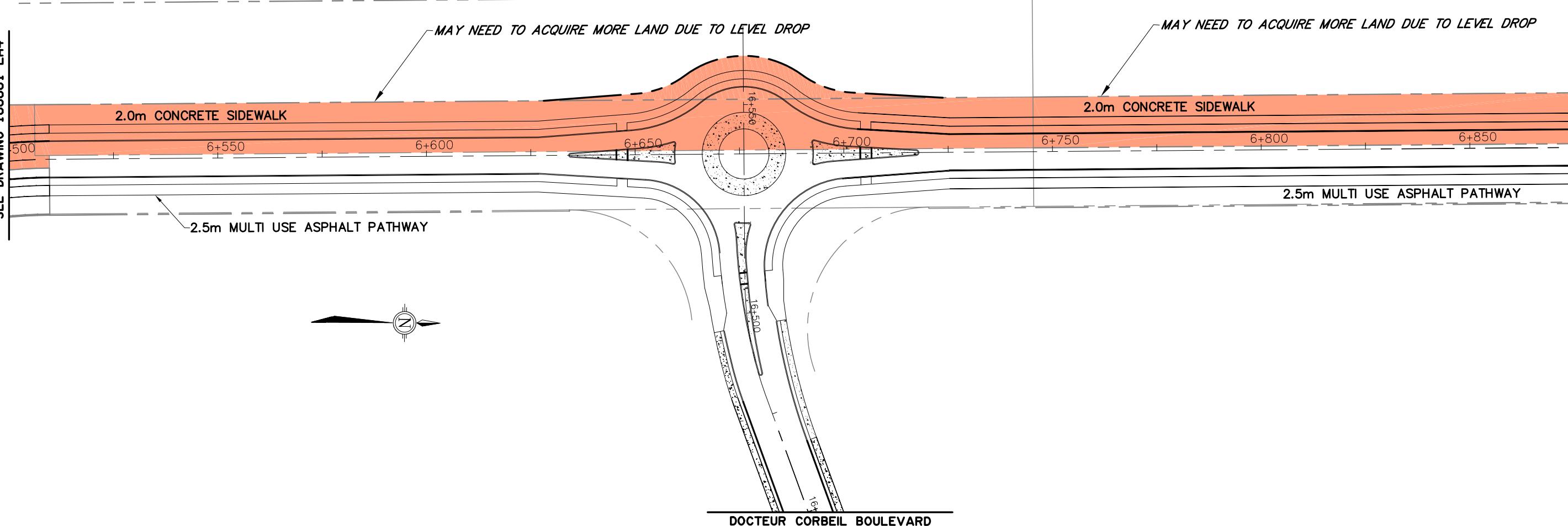
| | | | | | |
|---|--|---|---|---|----------------------------------|
| NOTES: 1- EXACT RIGHT OF WAY (R.O.W.) WIDTH "REQUIREMENT" TO BE SURVEYED BY OLS. | LEGEND:  LAND ACQUISITION REQUIREMENT |  | ATREL Engineering Ltd. Engineers - Ingénieurs | CITY OF CLARENCE-ROCKLAND POUPART/ST-JEAN LAND ACQUISITION PLAN | CLIENT No. III |
| | | | SCALE: 1 : 1000 10m 0 10 20 30m | PLAN POUPART/ST-JEAN STATION 3+125 TO STATION 3+750 | PROJECT No. 180801 |
| | | | | | DATE OCTOBER, 2018 |
| | | | | | DRAWING No. 180801-LA3 |



| | | | | | |
|---|--|---|---|---|--|
| NOTES: 1- EXACT RIGHT OF WAY (R.O.W.) WIDTH "REQUIREMENT" TO BE SURVEYED BY OLS. | LEGEND:  LAND ACQUISITION REQUIREMENT |  STREET MAP |  ATREL Engineering Ltd. Engineers - Ingénieurs | CITY OF CLARENCE-ROCKLAND POUPART/ST-JEAN LAND ACQUISITION PLAN | CLIENT No. III PROJECT No. 180801 DATE OCTOBER, 2018 DRAWING No. 180801-LA4 |
| | | | SCALE: I : 1000 10m 0 10 20 30m | PLAN ST-JEAN STREET STATION 3+750 TO STATION 6+500 | |

MATCH LINE STA. 6+500
SEE DRAWING 180801-LA4

ST-JEAN STREET

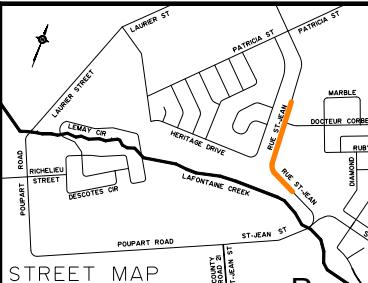


NOTES:

1- EXACT RIGHT OF WAY (R.O.W.) WIDTH
"REQUIREMENT" TO BE SURVEYED BY OLS.

LEGEND:

LAND ACQUISITION REQUIREMENT



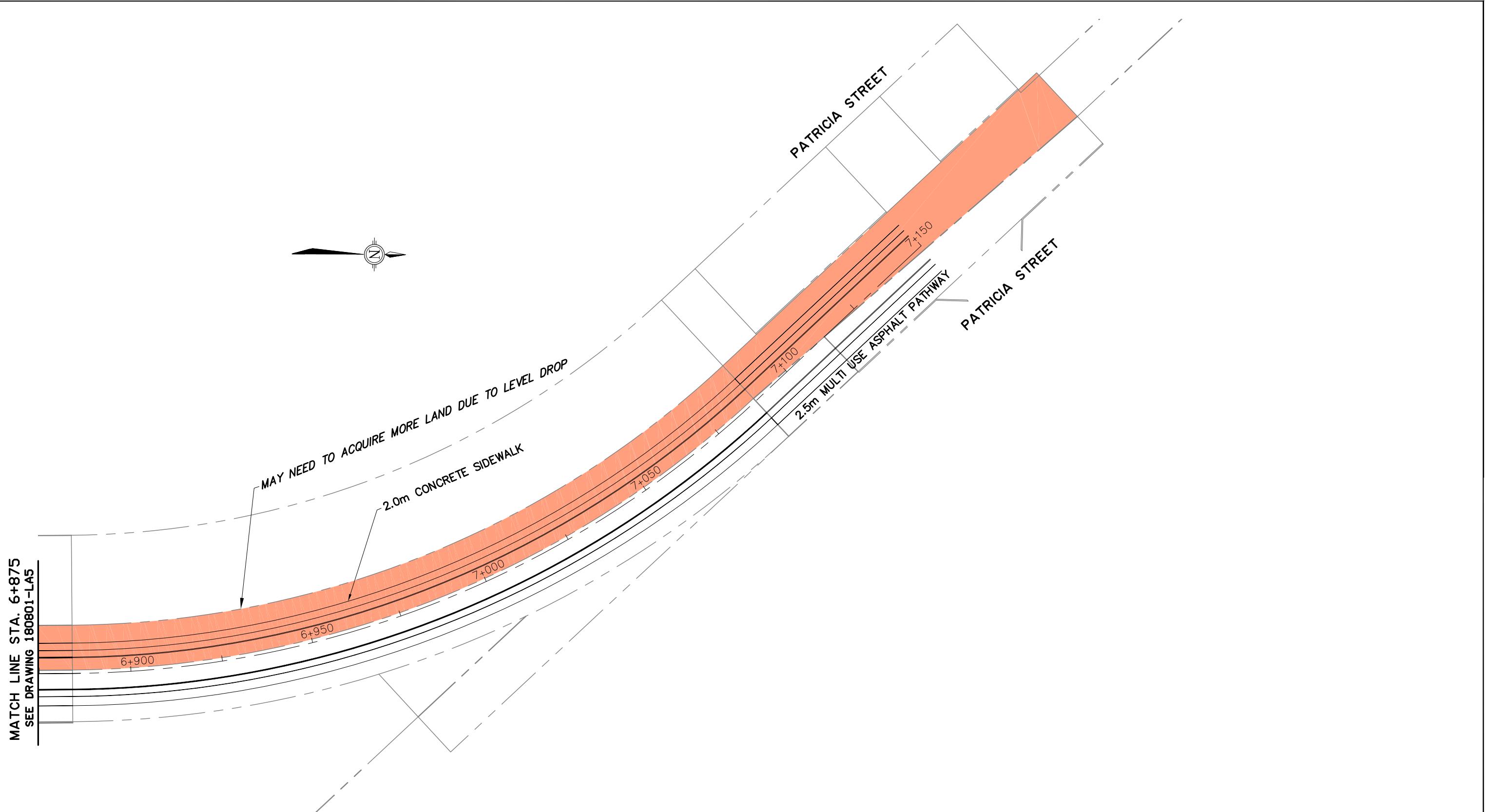
ATREL Engineering Ltd.
Engineers - Ingénieurs

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
LAND ACQUISITION PLAN

CLIENT No. III
PROJECT No. IBO801
DATE OCTOBER, 2018
DRAWING No. IBO801-LA5

SCALE: 1 : 1000
10m 0 10 20 30m

PLAN
ST-JEAN STREET
STATION 6+500 TO STATION 6+875

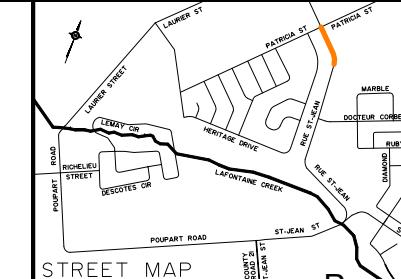


NOTES:

1- EXACT RIGHT OF WAY (R.O.W.) WIDTH
"REQUIREMENT" TO BE SURVEYED BY OLS.

LEGEND:

LAND ACQUISITION REQUIREMENT



Page 289 of 322

ATREL Engineering Ltd.
Engineers - Ingénieurs

CITY OF CLARENCE-ROCKLAND
POUPART/ST-JEAN
LAND ACQUISITION PLAN

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | IB0801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | IB0801-LA6 |

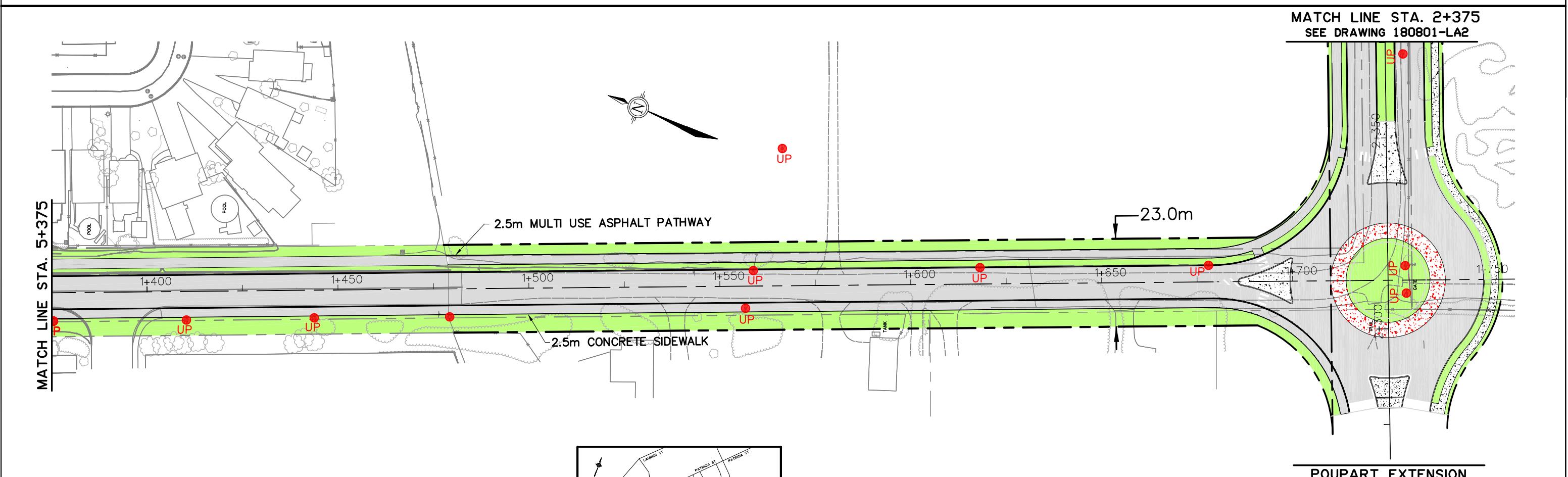
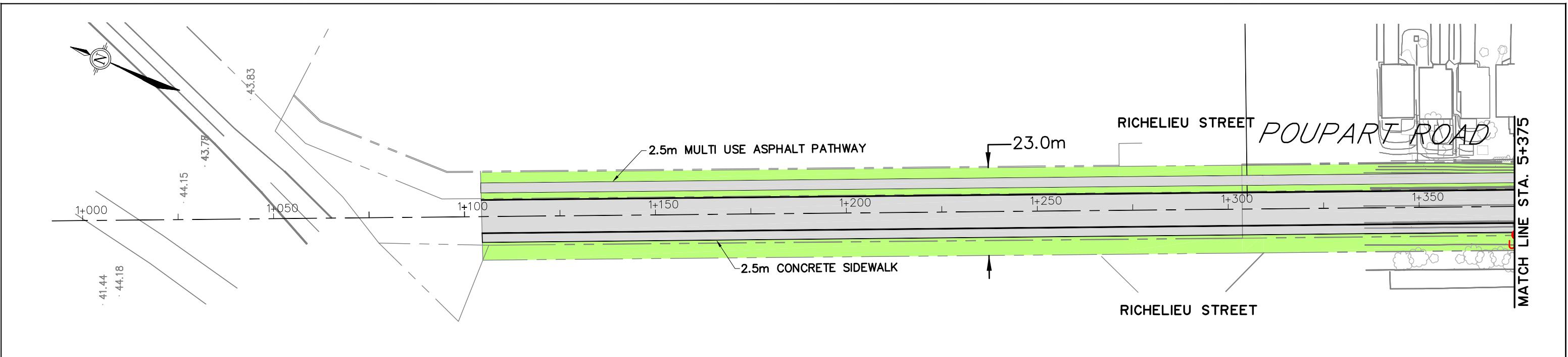
SCALE:
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PLAN
ST-JEAN STREET
STATION 6+875 TO STATION 7+150

APPENDIX “G”

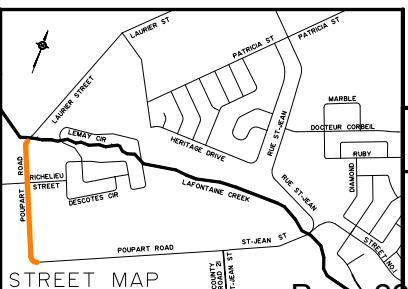
Road Schematic Plans

- 180801-RD1 (Poupart)
- 180801-RD2 (Poupart)
- 180801-RD3 (Poupart/St-Jean)
- 180801-RD4 (St-Jean)
- 180801-RD5 (St-Jean)
- 180801-RD6 (St-Jean)



LEGEND:

- GRASS AREA
 - ASPHALT AREA (ROAD AND MULTI-USE PATHWAY)
 - CONCRETE AREA
 - OTHER MATERIAL
 - UP ● UTILITY POLE



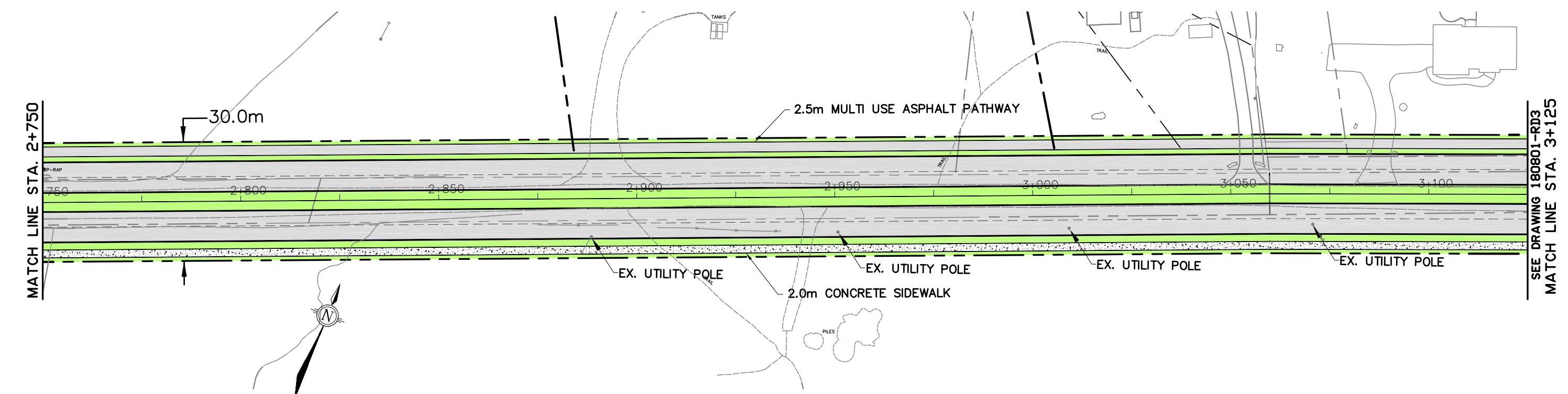
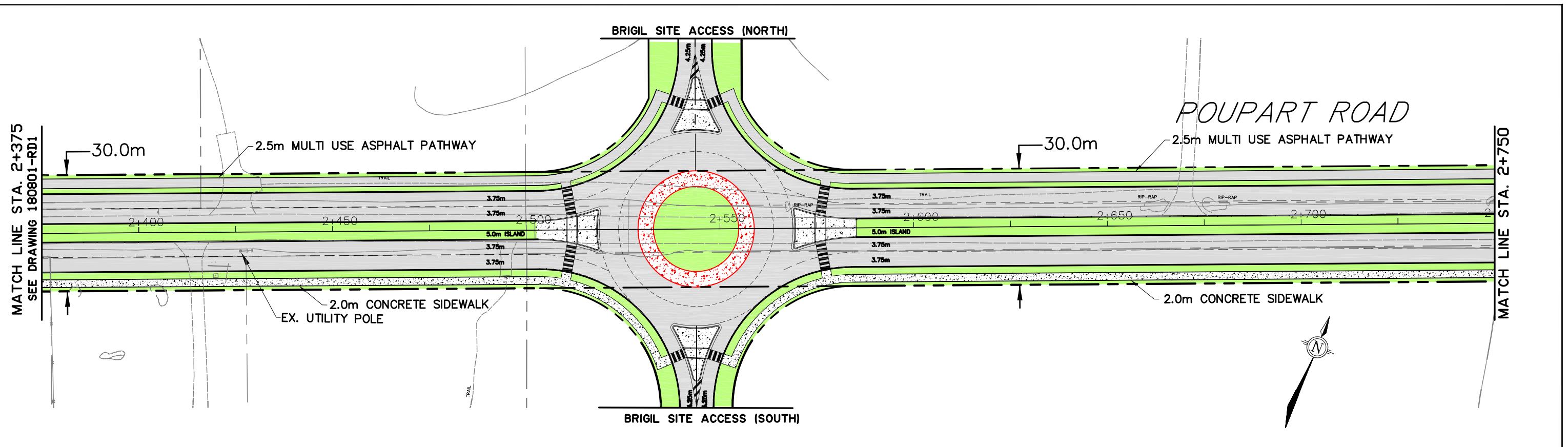
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 ATREL Engineering Ltd.
Engineers - Ingénieurs

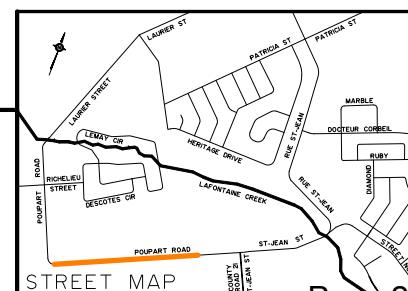
CITY OF CLARENCE-ROCKLAND
POUPART / ST-JEAN
ROAD SCHEMATIC PLAN

ENT NO. III
PROJECT No. 180801
ATE OCTOBER, 2018
AWING No.
180801-RDI



LEGEND:

- GRASS AREA
- ASPHALT AREA (ROAD AND MULTI-USE PATHWAY)
- CONCRETE AREA
- OTHER MATERIAL



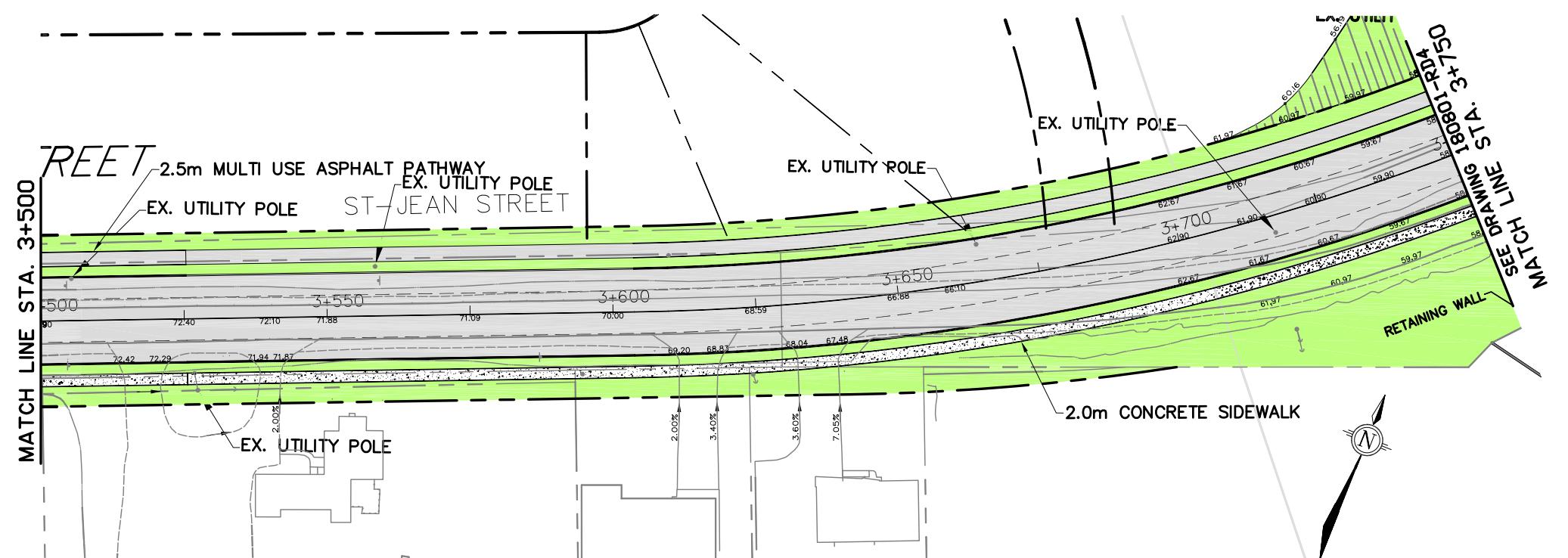
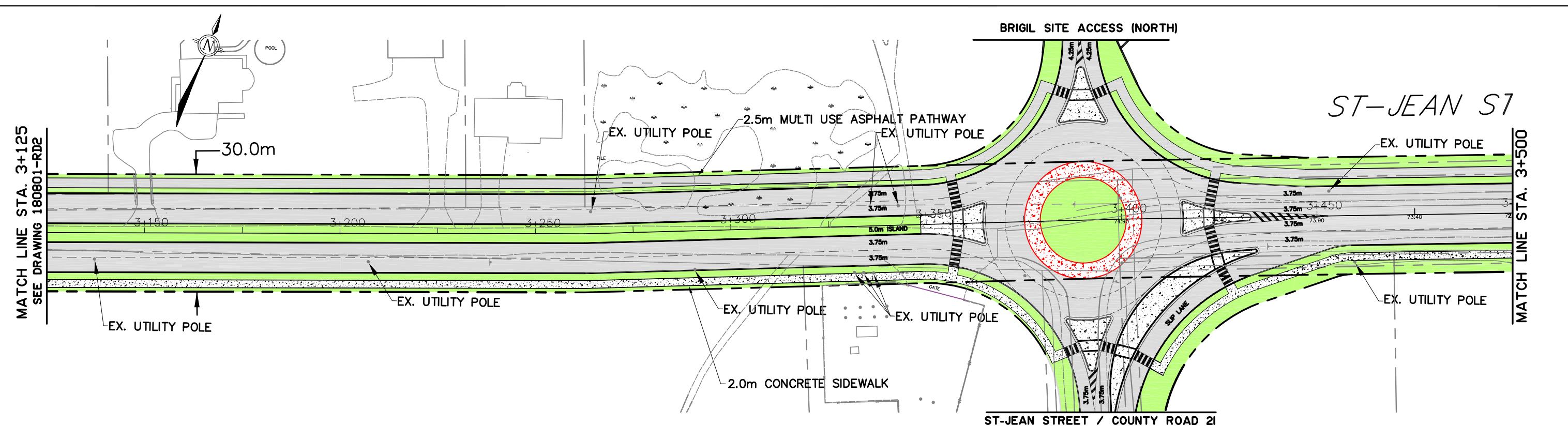
SCALE:

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10m 0 10 20 30m

ATREL Engineering Ltd
Engineers - Ingénieurs

CITY OF CLARENCE-ROCKLAND
POUPART / ST-JEAN
ROAD SCHEMATIC PLAN
PLAN
POUPART ROAD
STATION 2+375 TO STATION 3+125

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | 180801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | 180801-RD2 |



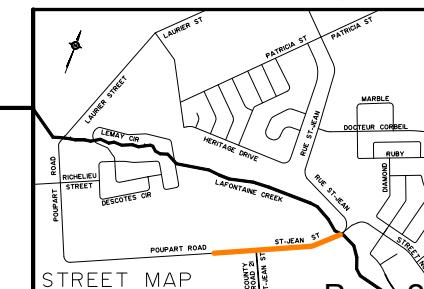
LEGEND:

GRASS AREA

ASPHALT AREA (ROAD AND MULTI-USE PATHWAY)

CONCRETE AREA

 OTHER MATERIAL



SCAL

1 : 1000



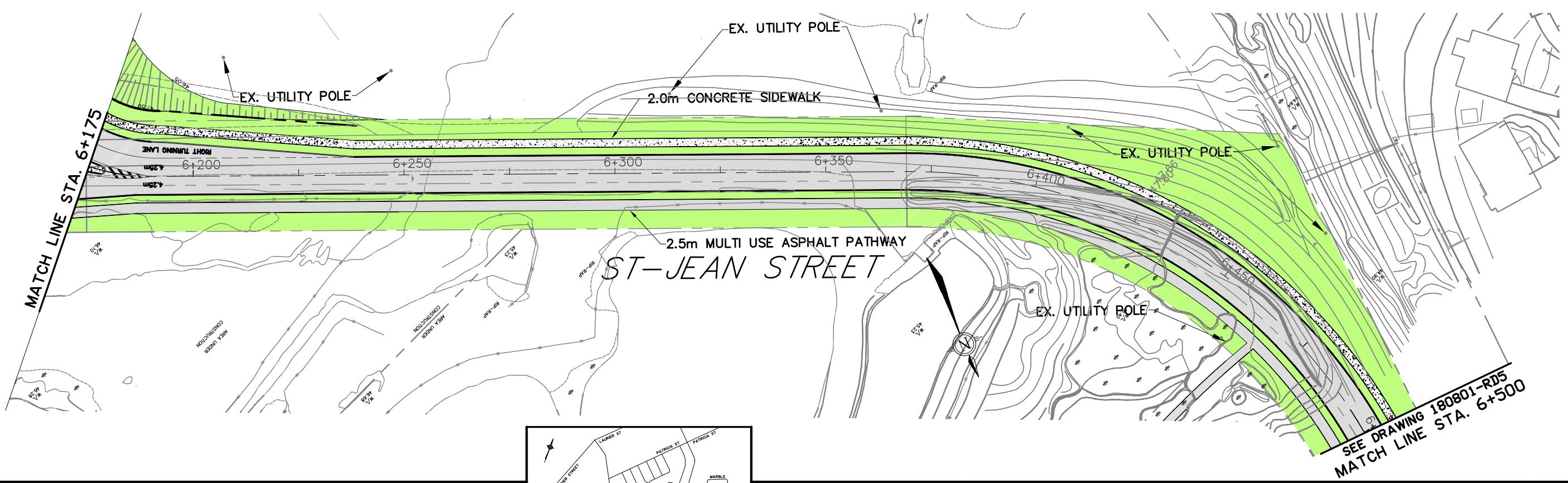
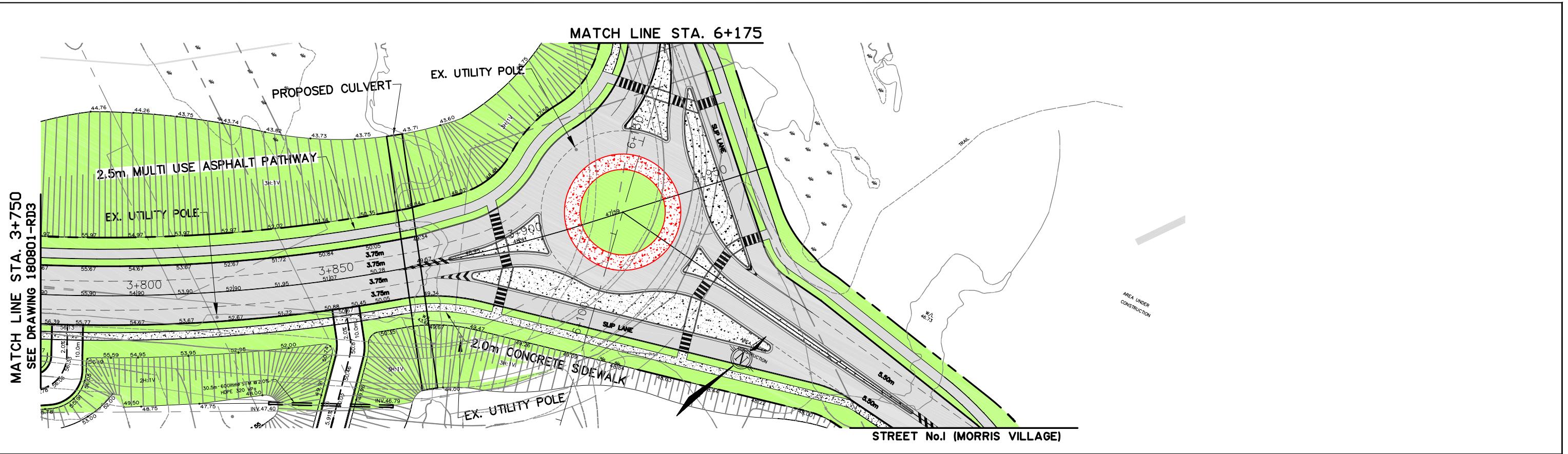
ATREL Engineering Ltd

Engineers - Ingénieurs

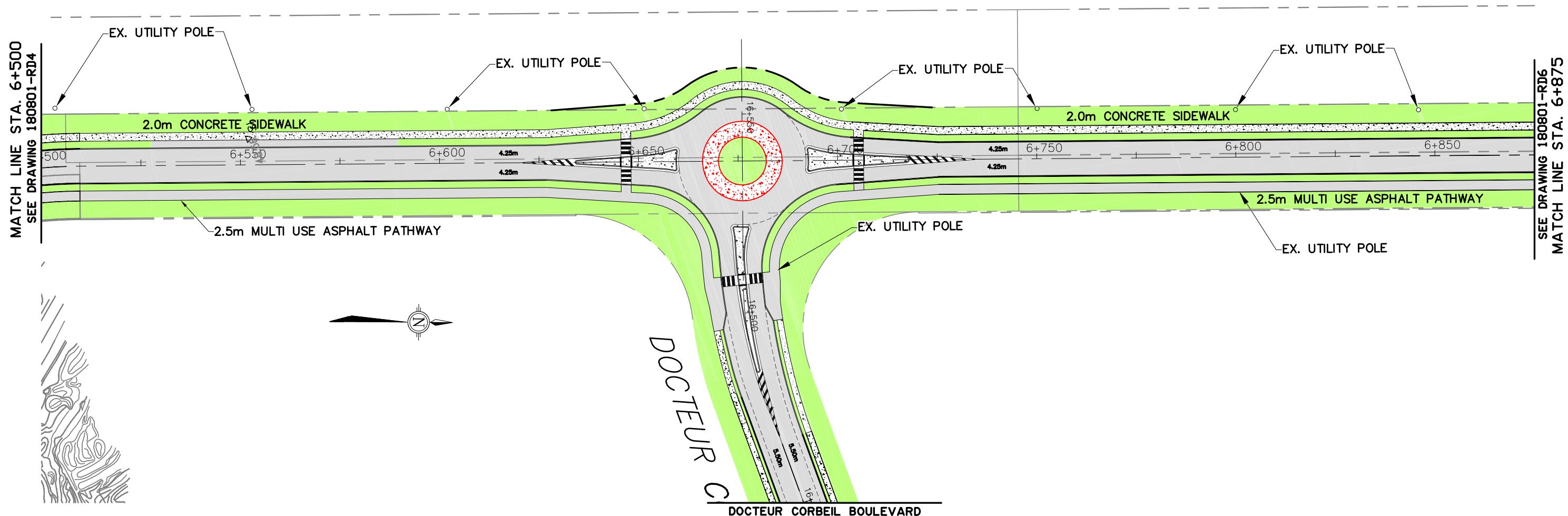
CITY OF CLARENCE-ROCKLAND
POUPART / ST-JEAN
ROAD SCHEMATIC PLAN

**PLAN
ST-JEAN STREET
STATION 3+125 TO STATION 3+750**

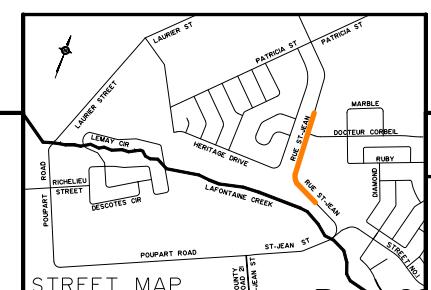
CLIENT No. |
PROJECT No. I8080
DATE OCTOBER, 201
DRAWING No. I80801-RD3



ST-JEAN STREET



| LEGEND: | |
|---|---|
| | GRASS AREA |
| | ASPHALT AREA (ROAD AND MULTI-USE PATHWAY) |
| | CONCRETE AREA |
| | OTHER MATERIAL |



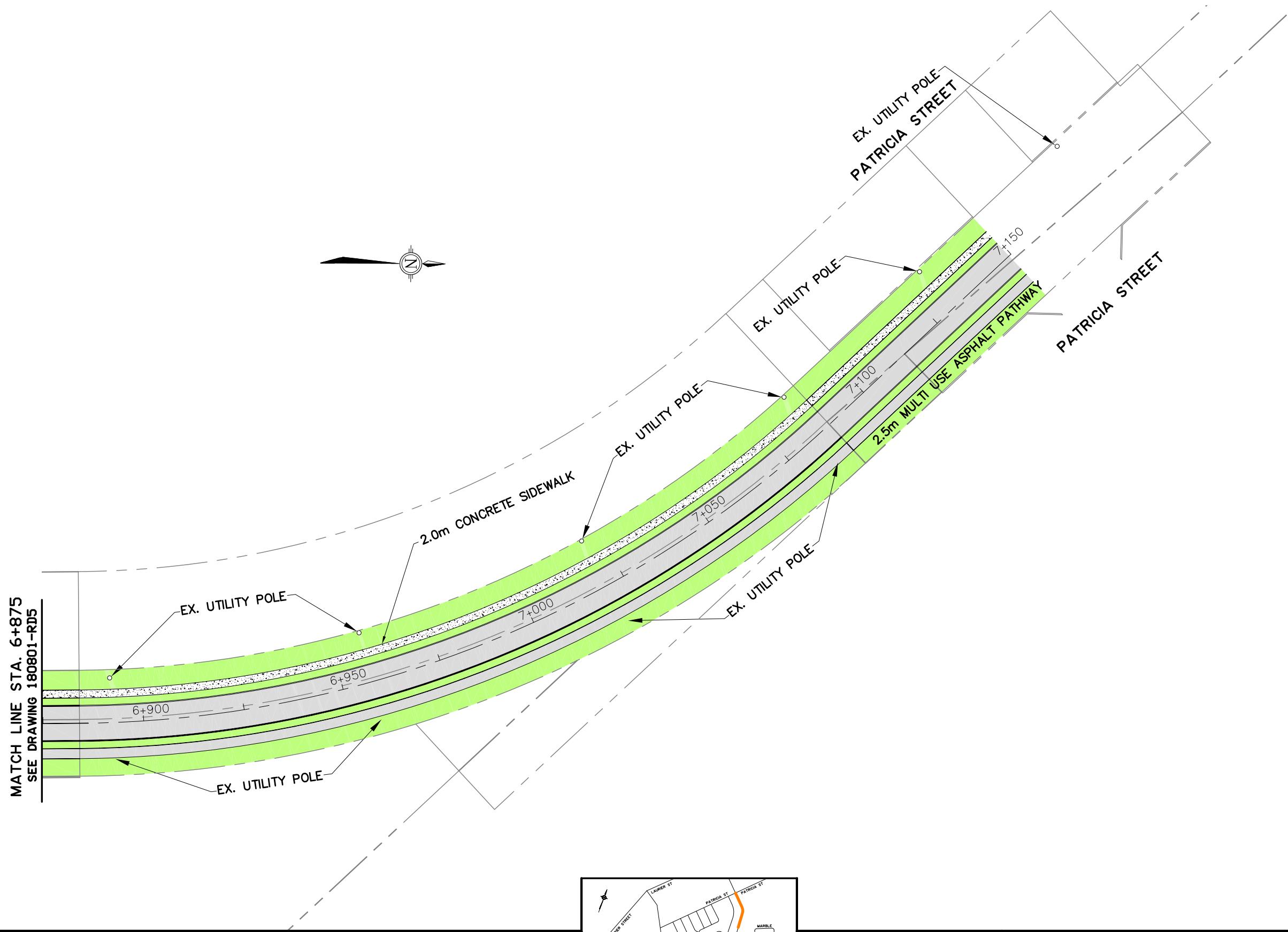
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ATREL Engineering Ltd
Engineers - Ingénieurs

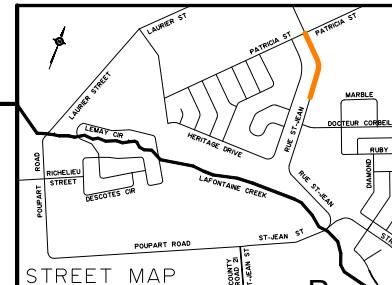
CITY OF CLARENCE-ROCKLAND
POUPART / ST-JEAN
ROAD SCHEMATIC PLAN
PLAN
ST-JEAN STREET
STATION 6+500 TO STATION 6+875

| | |
|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | 180801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | 180801-RD5 |



LEGEND:

- GRASS AREA
 - ASPHALT AREA (ROAD AND MULTI-USE PATHWAY)
 - CONCRETE AREA
 - OTHER MATERIAL



SCAL

| :

10m 0 10 20 30



ATREL Engineering Ltd
Engineers - Ingénieurs

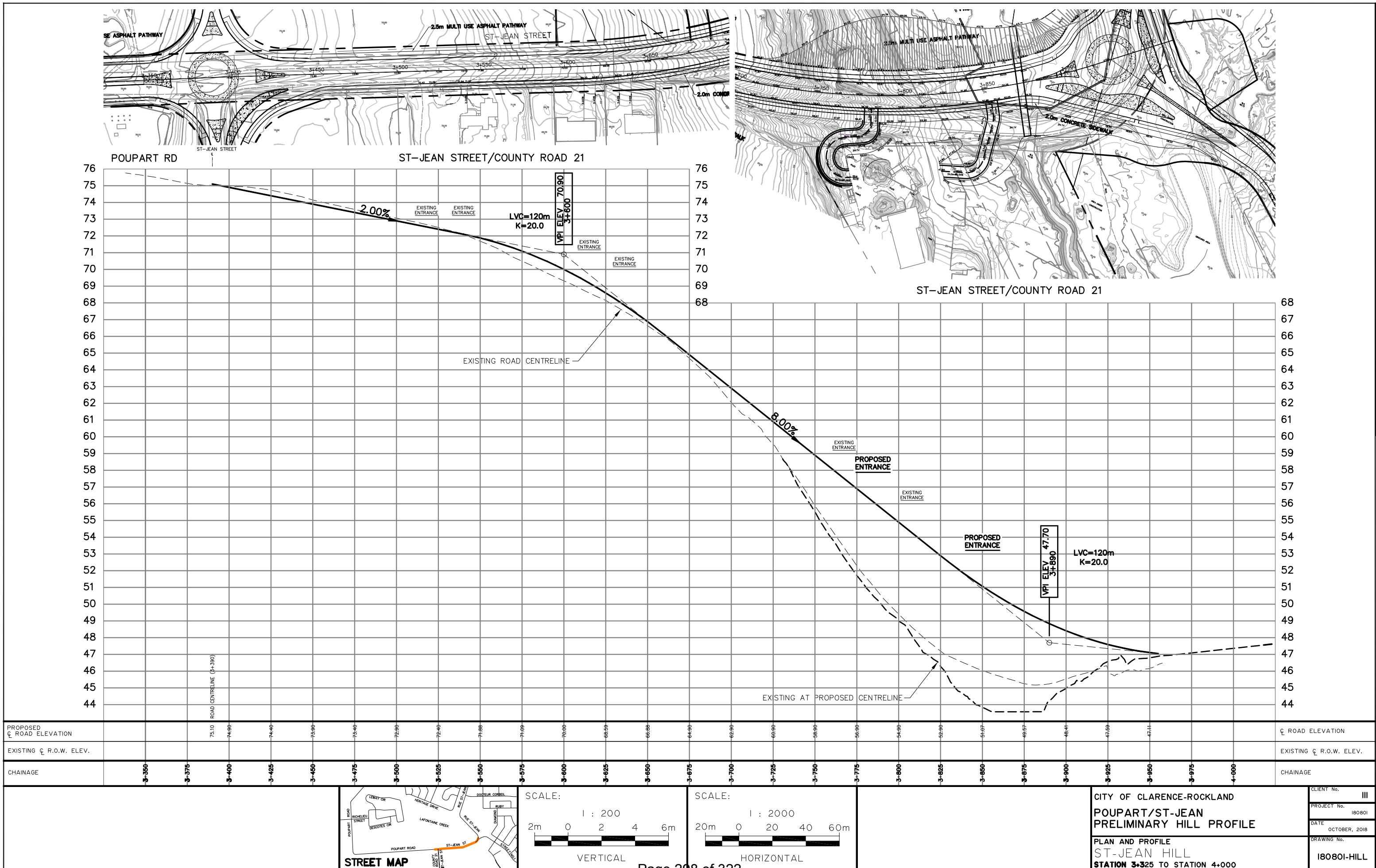
CITY OF CLARENCE-ROCKLAND
POUPART / ST-JEAN
ROAD SCHEMATIC PLAN

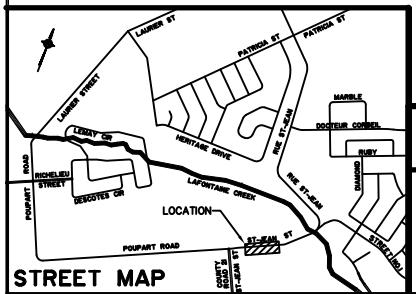
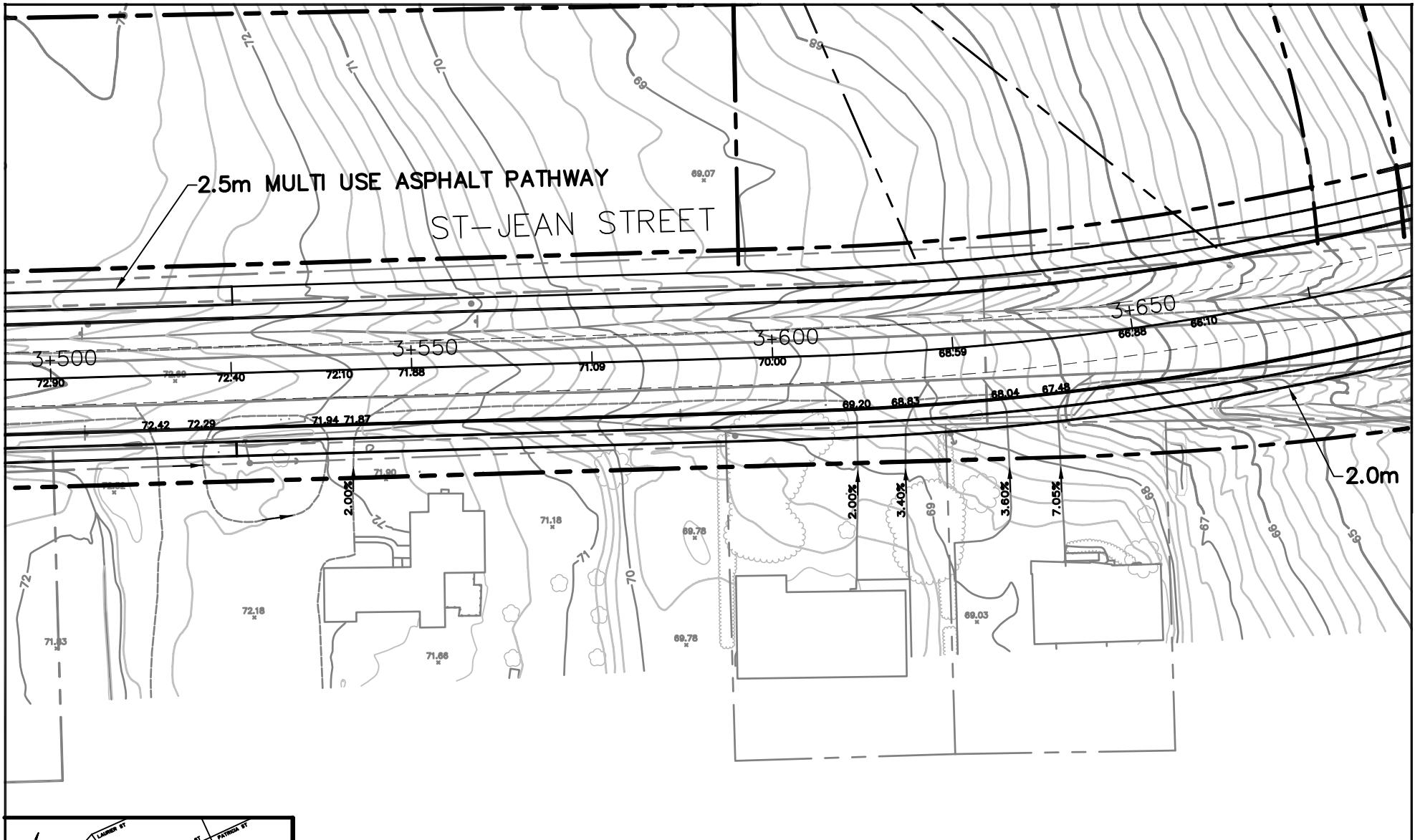
CLIENT No. III
PROJECT No. 180801
DATE OCTOBER, 2018
DRAWING No.
180801-RD6

APPENDIX "H"

St-Jean Hill Plans

180801-HILL - St-Jean Preliminary Hill Plan and Profile
180801-DS1 - St-Jean Residential Preliminary Driveway Slopes
180801-DS2 - St-Jean Commercial Preliminary Driveway Slopes





SCALE:

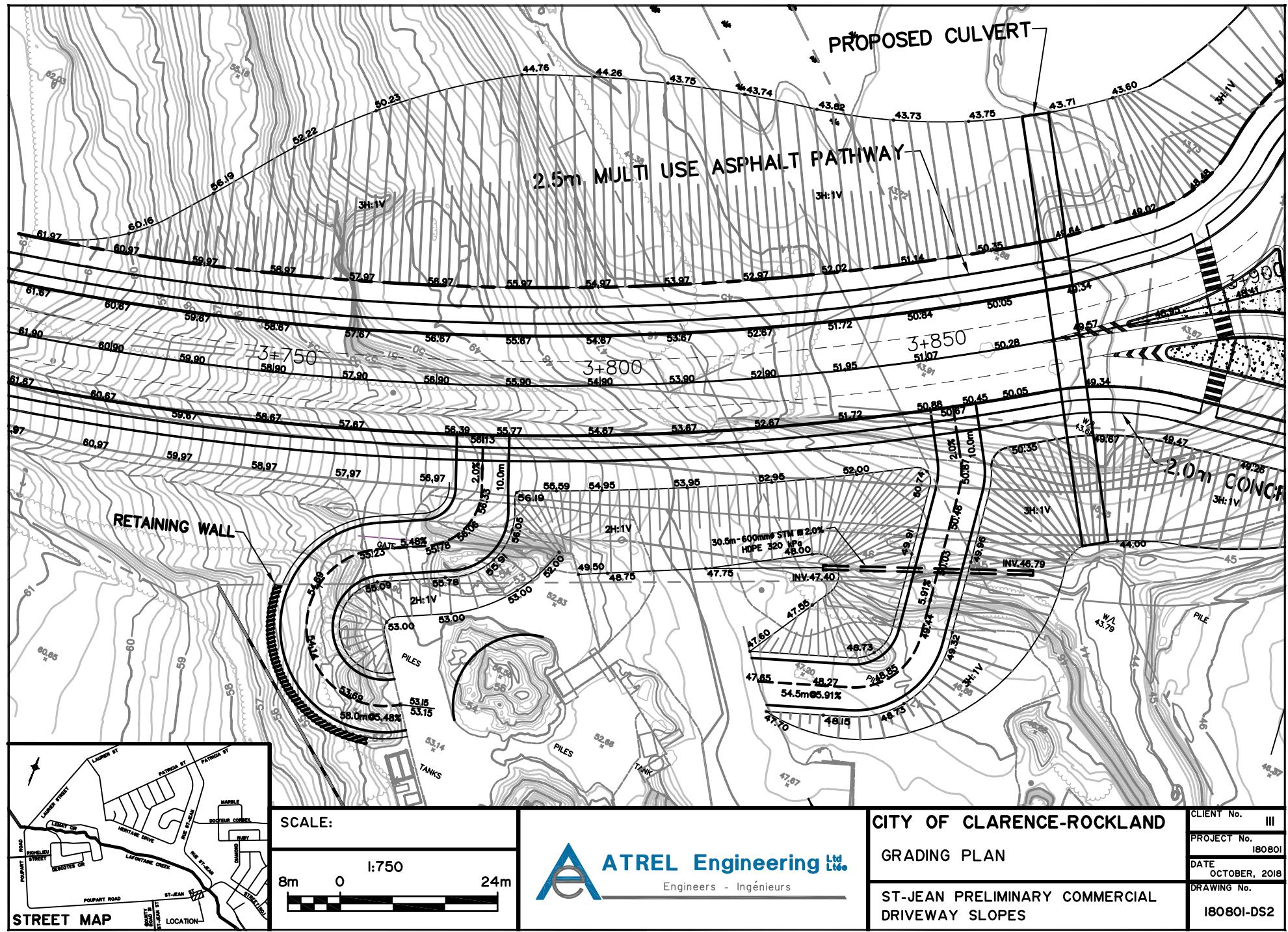
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CITY OF CLARENCE-ROCKLAND
GRADING PLAN

**ST-JEAN PRELIMINARY RESIDENTIAL
DRIVEWAY SLOPES**

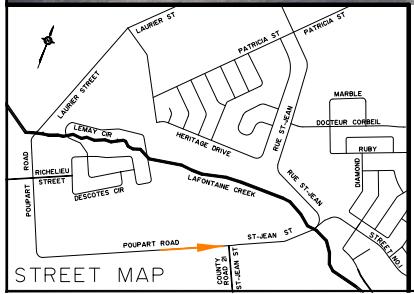
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|-------------|---------------|
| CLIENT No. | III |
| PROJECT No. | I80801 |
| DATE | OCTOBER, 2018 |
| DRAWING No. | I80801-DS1 |



APPENDIX "I"

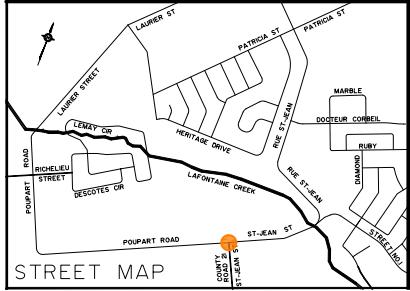
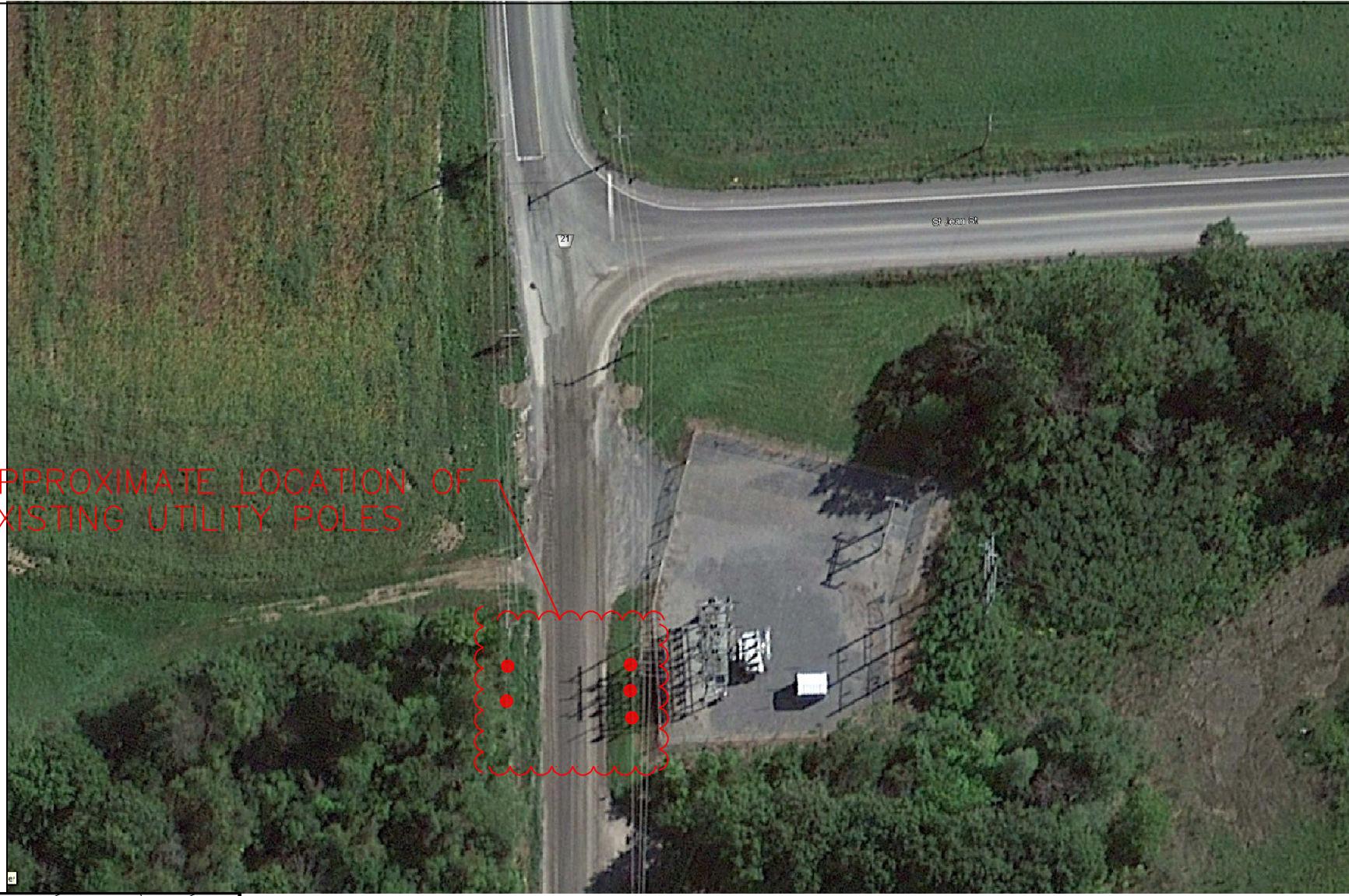
Hydro Station Sketches

180801-HS1 - Hydro Station Street View
180801-HS2 - Hydro Station Top View



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| | | |
|-----------------------------|-------------|---------------|
| CITY OF CLARENCE-ROCKLAND | CLIENT No. | III |
| TRANSPORTATION IMPACT STUDY | PROJECT No. | 180801 |
| PLAN | DATE | OCTOBER, 2018 |
| HYDRO STATION STREET VIEW | DRAWING No. | 180801-HSI |



| | |
|-----------------------------|------------------------|
| CITY OF CLARENCE-ROCKLAND | CLIENT No. III |
| TRANSPORTATION IMPACT STUDY | PROJECT No. I8080I |
| PLAN | DATE OCTOBER, 2018 |
| HYDRO STATION TOP VIEW | DRAWING No. I8080I-HS2 |

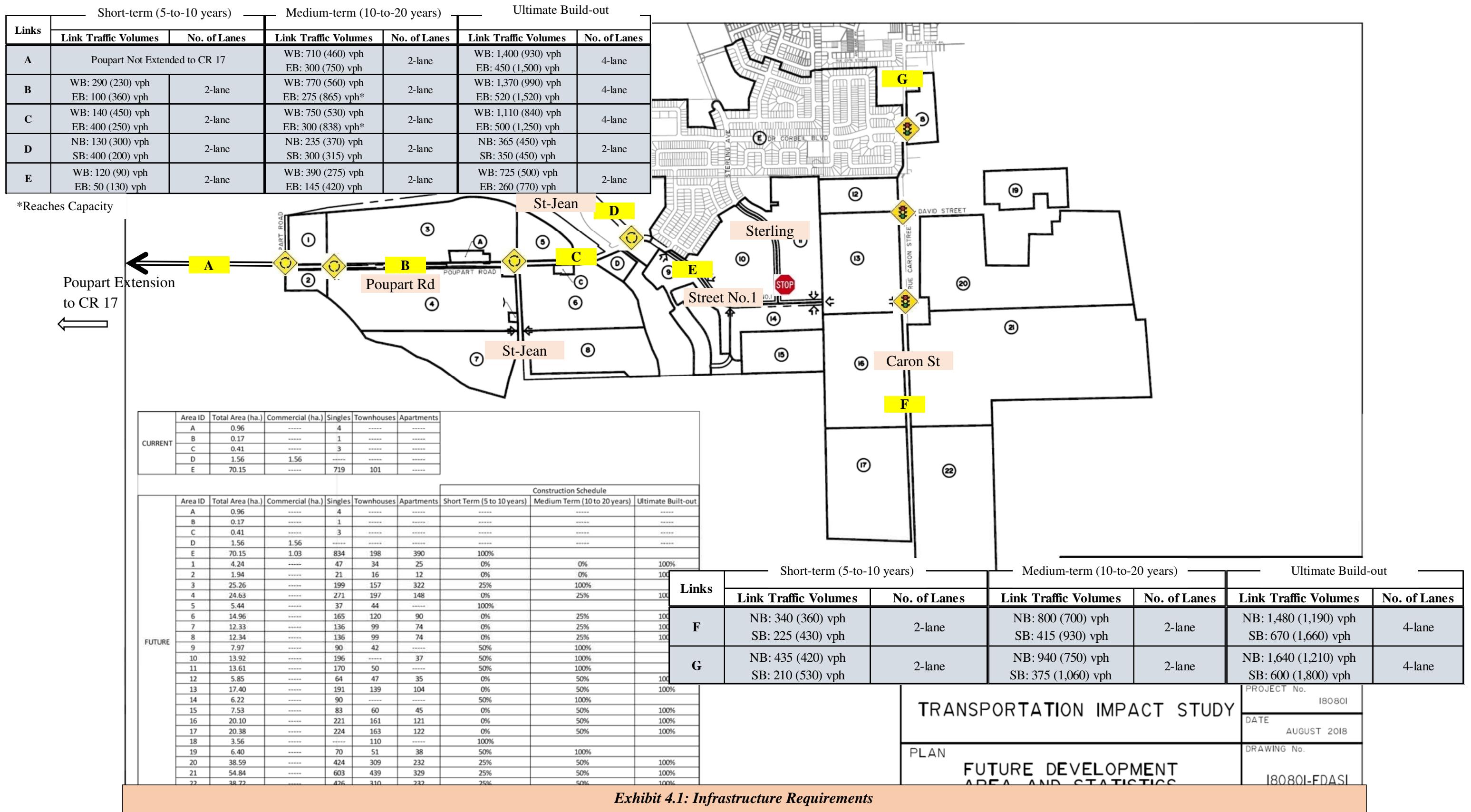


Exhibit 4.1: Infrastructure Requirements



REPORT N° HR 2019-08

| | |
|---------------------|------------------------|
| Date | 26/02/2019 |
| Submitted by | Gerry Lalonde |
| Subject | Council Group Benefits |
| File N° | HR 2019-08 |

1) **NATURE/GOAL :**

The nature of this report is to provide additional information to Council regarding participation in the Ontario Municipal Employees Retirement System (OMERS) and Great West Life (GWL) group benefits in regard to the Head of Council and Councillors.

2) **DIRECTIVE/PREVIOUS POLICY :**

Council through the Mayor requested information in regards to the cost associated for Council's participation in OMERS and GWL.

3) **DEPARTMENT'S RECOMMENDATION :**

That report HR 2019-08 be received for information.

4) **BACKGROUND :**

The Head of Council and Councillors have not participated in the OMERS and GWL programs in the past.

5) **DISCUSSION :**

Great West Life (GWL)

Group insurance provides a mechanism for employers to provide employee benefits as part of an employee's total compensation package outside of government-provided benefit programs.

Group insurance benefits currently provided by the City of Clarence-Rockland to employees include;

- Short Term Disability Insurance
- Long Term Disability Insurance
- Health Insurance
- Dental Insurance
- Life Insurance
- Dependant Life Insurance

For most employees the City pays 90% of the premium of the insurance plans provided to employees. The employee must pay 10% of the premiums.

Ontario Municipal Employees Retirement System (OMERS)

OMERS allow only two enrollment options;

1. Mayor on his own
2. All council members including the Mayor.

A by-law would be required to authorize the Mayor or all of Council's participation in the program. Note that Council members are not allowed to participate in the program if the mayor does not participate.

6) CONSULTATION :

N/a

7) RECOMMENDATIONS OR COMMENTS FROM COMMITTEE/ OTHER DEPARTMENTS:

N/a

8) FINANCIAL IMPACT (expenses/material/etc.) :

The cost for the Ontario Municipal Employees Retirement System (OMERS) is equal to 9% of the gross salary for both the employee and the City. The total cost to the City for adding OMERS for the Head of Council and Councillors is \$26,104 annually.

| Ontario Municipal Employees Retirement System (OMERS) | | | | | |
|---|---------|------------|---|---------|------------|
| Cost to Employee | | | Cost to City | | |
| | Per Pay | Annualized | | Per Pay | Annualized |
| Mayor | \$ 180 | \$ 4,680 | | \$ 180 | \$ 4,680 |
| Councillor | \$ 103 | \$ 2,678 | | \$ 103 | \$ 2,678 |
| Total cost (Mayor + 8 Councillors) | | \$ 26,104 | Total cost (Mayor + 8 Councillors) | | \$ 26,104 |

Depending on the option chosen by Council for group insurance, the annual cost to the City could vary between \$13,590 to \$34,974.

Great West Life (GWL)

| Option Plan 1- Life & ADD Flat \$20,000 | | | |
|--|-------------|---|-------------|
| Cost to Employee | | | |
| Single Coverage | | Family Plan | |
| Per Pay | Annualized | Per Pay | Annualized |
| \$ 6.46 | \$ 168.00 | \$ 16.23 | \$ 422.00 |
| Cost to City | | | |
| Single Coverage | | Family Plan | |
| Per Pay | Annualized | Per Pay | Annualized |
| \$ 58.08 | \$ 1,510.00 | \$ 146.08 | \$ 3,798.00 |
| Total cost (Mayor+ 8 Councillors) | \$ 13,590 |  | \$ 34,182 |

| Option Plan 2- Life & ADD Flat \$50,000 | | | |
|--|-------------|---|-------------|
| Cost to Employee | | | |
| Single Coverage | | Family Plan | |
| Per Pay | Annualized | Per Pay | Annualized |
| \$ 6.81 | \$ 177.00 | \$ 16.58 | \$ 431.00 |
| Cost to City | | | |
| Single Coverage | | Family Plan | |
| Per Pay | Annualized | Per Pay | Annualized |
| \$ 61.46 | \$ 1,598.00 | \$ 149.46 | \$ 3,886.00 |
| Total cost (Mayor+ 8 Councillors) | \$ 14,382 |  | \$ 34,974 |

Recommended funding source, contingency.

9) LEGAL IMPLICATIONS:

N/a

10) RISK MANAGEMENT:

N/a

11) STRATEGIC IMPLICATIONS:

Strategic Pillar- Health and Wellness

12) SUPPORTING DOCUMENTS:

Option Plan 1- Life & ADD Flat \$20,000

Option Plan 2- Life & ADD Flat \$50,000

City of Clarence Rockland**Option Plan 1 - Life & ADD Flat \$20,000
Member Council - Benefits****LIFE INSURANCE**

| | |
|----------------|-------------------------------|
| Benefit amount | Great West Life Policy 136826 |
| Reduction | Flat \$20,000 |
| Termination | 50% at age 65 |

AD&D

| | |
|----------------|------------------|
| Benefit amount | SSQ Policy 1NH00 |
| Reduction | Equal to Life |
| Termination | 50% at age 65 |

DEPENDENT LIFE

| | |
|----------------|-----------------------------------|
| Benefit amount | Great West Life Policy 136826 |
| Termination | Spouse - \$15,000 & Child \$2,000 |

EXTENDED HEALTH CARE

| | |
|--|---|
| Deductible | Great West Life Policy 136826 |
| Reimbursement | N/A |
| Maximums | 100% - Vision care and out of country emergency |
| Vision Care | 90% - all other expenses |
| Eye Examinations | \$15,000 per calendar year drug expenses |
| Hospital | \$300 every 24 months |
| Drug Plan Description | 1 exam every 24 months |
| - Exclusions | Semi-Private |
| - Limitations | Drugs legally requiring a prescription |
| Private Duty Nursing | Erectile dysfunction drugs |
| Chiropractor | Smoking Cessations \$500 per lifetime |
| Osteopath, Physiotherapist and Podiatrists | \$5,000 to a maximum of 12 months |
| Psychologists/Social Workers | \$1,100 per calendar year combined with all other paramedical practitioners |
| Speech Therapist, Naturopath, Massage Therapist, Acupuncture, occupational Therapist | \$1,100 per calendar year combined with all other paramedical practitioners |
| Custom-made orthopaedic Shoes or modifications | \$1,100 per calendar year combined with Orthotics |
| Custom-made orthotics | \$100 per calendar year combined with Orthopaedic shoes |
| Hearing Aids | \$1,000 every 5 years |
| Medical Equip. & Supplies | Eligible |
| Termination | End of term |
| TRAVEL | Great West Life Policy 136826 |
| Benefit Maximum | Unlimited |
| Trip Duration | Equal to OHIP |
| Termination | End of term |
| DENTAL | Great West Life Policy 136826 |
| Benefit | Basic - 90% Major - 50% |
| Maximum | Basic & Major - \$3,000 per calendar year combined |
| ODA Fee Schedule | Current |
| Recall Frequency | Twice per calendar year |
| Termination | End of term |

City of Clarence Rockland**Option Plan 2 - Life & ADD Flat \$50,000****Member Council - Benefits**

| LIFE INSURANCE | |
|--|---|
| Benefit amount | Great West Life Policy 136826 |
| Reduction | Flat \$50,000 |
| Termination | 50% at age 65 |
| <hr/> | |
| AD&D | End of term |
| Benefit amount | SSQ Policy 1NH00 |
| Reduction | Equal to Life |
| Termination | 50% at age 65 |
| <hr/> | |
| DEPENDENT LIFE | Earliest of age 80 or end of term |
| Benefit amount | Great West Life Policy 136826 |
| Termination | Spouse - \$15,000 & Child \$2,000 |
| <hr/> | |
| EXTENDED HEALTH CARE | End of term |
| Deductible | Great West Life Policy 136826 |
| Reimbursement | N/A |
| Maximums | 100% - Vision care and out of country emergency |
| Vision Care | 90% - all other expenses |
| Eye Examinations | \$15,000 per calendar year drug expenses |
| Hospital | \$300 every 24 months |
| Drug Plan Description | 1 exam every 24 months |
| - Exclusions | Semi-Private |
| - Limitations | Drugs legally requiring a prescription |
| Private Duty Nursing | Erectile dysfunction drugs |
| Chiropractor | Smoking Cessations \$500 per lifetime |
| Osteopath, Physiotherapist and Podiatrists | \$5,000 to a maximum of 12 months |
| Psychologists/Social Workers | \$1,100 per calendar year combined with all other paramedical practitioners |
| Speech Therapist, Naturopath, Massage Therapist, Acupuncture, occupational Therapist | \$1,100 per calendar year combined with all other paramedical practitioners |
| Custom-made orthopaedic Shoes or modifications | \$1,100 per calendar year combined with Orthotics |
| Custom-made orthotics | \$100 per calendar year combined with Orthopaedic shoes |
| Hearing Aids | \$1,000 every 5 years |
| Medical Equip. & Supplies | Eligible |
| Termination | End of term |
| <hr/> | |
| TRAVEL | Great West Life Policy 136826 |
| Benefit Maximum | Unlimited |
| Trip Duration | Equal to OHIP |
| Termination | End of term |
| <hr/> | |
| DENTAL | Great West Life Policy 136826 |
| Benefit | Basic - 90% Major - 50% |
| Maximum | Basic & Major - \$3,000 per calendar year combined |
| ODA Fee Schedule | Current |
| Recall Frequency | Twice per calendar year |
| Termination | End of term |



REPORT N° PRO2019-009

| | |
|--------------|--|
| Date | 19/03/2019 |
| Submitted by | Brian Wilson |
| Subject | Protective Services – Monthly Report (February 2019) |
| File N° | Click here to enter text. |

1) **NATURE/GOAL :**

To advise council on the activities performed by the Protective Services Department.

2) **DIRECTIVE/PREVIOUS POLICY :**

None.

3) **DEPARTMENT'S RECOMMENDATION :**

THAT Report No. PRO2019-009 in regards to monthly statistics, be received as information.

QUE le rapport No. PRO2019-009 au sujet des statistiques mensuel, soit reçu à titre d'information.

4) **MONTHLY STATISTICS :**

For the month of February 2019, the Protective Services Department did perform the following:

Fire Department

Incidents:

| Call Type | # of Calls (Feb) | 2019 YTD | 2018 YTD |
|---------------------------|------------------|----------|----------|
| Fire – Residential | 3 | 3 | |
| Fire – Commercial | | | |
| Fire – Outdoor | | | |
| Fire – Chimney | 1 | 2 | 1 |
| Fire – Vehicle | 1 | 2 | |
| Fire – Outbuilding | | | |
| Fire – Other (e.g. steam) | | | 2 |
| Burning Complaint | | | 1 |
| Fire Alarms (Cooking) | 2 | 3 | 4 |
| Fire Alarms (Malicious) | | | 1 |
| Fire Alarms (Accidental) | | 3 | 4 |
| Fire Alarms (Faulty Eq.) | | 3 | 3 |
| Fire Alarms (Other) | | | 2 |
| CO Alarm (CO found) | 1 | 2 | 2 |
| CO Alarm (No CO found) | 7 | 10 | 3 |

| | | | |
|-----------------------|-----------|-----------|----|
| MVC - extrication | | 1 | 2 |
| MVC - no extrication | 5 | 10 | 5 |
| Medical - VSA | 2 | 6 | 6 |
| Medical - Unconscious | 2 | 6 | 7 |
| Medical - Other | 2 | 8 | 12 |
| Cancelled On Route | | | 3 |
| Other | 5 | 11 | |
| Mutual Aid | | | |
| TOTAL | 31 | 70 | 60 |

Fire department response times are detailed in the attached report, and are summarized below:

| February – Weekday Incidents | | | |
|--|---------------|-------------------------------------|---------------|
| District | # of P1 Calls | Avg. First Arriving Unit (P1 calls) | # of P2 Calls |
| 1A Bourget Rural | 2 | 9:56 mins | |
| 1B Bourget Urban | | | |
| 1C Bourget Rural | | | |
| 2A Clarence-Creek Rural | 1 | 0:01 mins | |
| 2B Clarence-Creek Urban | | | |
| 2C Clarence-Creek Rural | | | |
| 3A Rockland Rural | 3 | 5:43 mins | |
| 3B Rockland Urban | 6 | 2:14 mins | 3 |
| (P1 = priority one, lights & sirens / P2 = priority two, no lights/sirens) | | | |

| February – Evening/Weekend/Holiday Incidents | | | |
|--|---------------|-------------------------------------|---------------|
| District | # of P1 Calls | Avg. First Arriving Unit (P1 calls) | # of P2 Calls |
| 1A Bourget Rural | 3 | 14:08 mins | 2 |
| 1B Bourget Urban | | | |
| 1C Bourget Rural | | | |
| 2A Clarence-Creek Rural | 1 | 16:53 mins | |
| 2B Clarence-Creek Urban | | | |
| 2C Clarence-Creek Rural | | | |
| 3A Rockland Rural | 2 | 10:45 mins | 1 |
| 3B Rockland Urban | 3 | 9:01 mins | 4 |
| (P1 = priority one, lights & sirens / P2 = priority two, no lights/sirens) | | | |

Prevention / Public Education:

| | February | YTD |
|-----------------------------|----------|-----|
| Fire Inspections Completed | 23 | 28 |
| Public Education Activities | 2 | 2 |

Training:

| | February | YTD |
|------------------------------------|----------|-----|
| Training Courses Offered | 5 | 13 |
| Training Hours Worked (incl. prep) | 325 | 652 |

- The following topics were covered during training in February:

- o Mental health and substance abuse
- o Medical refresher training
- o Traffic control and incident scene safety
- o NFPA 1041 Fire Instructor Level 1
- o Training committee meeting (2 hours)

Meetings (evening meetings / committee meetings):

| | February | YTD (Hours) |
|--|----------|----------------|
| CRFD Executive Meetings | 4 | 7 |
| Meetings with UCPR Paramedics | | 2.5 |
| Conservation Authority Meetings | 4 | 4 |
| Meeting with NGOs (Ontario211, Red Cross) | 1.5 | 1.5 |
| Essentials of Municipal Fire Protection Workshop | 8 | 8 |
| Regional Chief's Meetings | 3 | 3 |

Municipal Enforcement

| | February | 2019 YTD | 2018 YTD |
|----------------------------------|----------|-------------|-------------|
| Officers hours worked | 579 | 1249 | 1012 |
| OT hours worked (1.5) | 12.5 | 61 | 47 |
| OT hours for On Call (1.0) | 0 | 0 | 24 |
| Hours on snow enforcement | 37 | 137 | 22.5 |
| OT hours on snow enforcement | 12.5 | 61 | 32.5 |
| Hours on Taxi Administration | 5 | 8 | 47 |
| Hours on Civic Addressing | 1 | 3 | 180 |
| # of parking tickets issued | 23 | 125 | 114 |
| # of hours on Business Licensing | 5 | 10 | 19 |
| # of parking warnings issued | 43 | 70 | 85 |
| # of Part I tickets issued | 3 | 3 | 2 |
| # of Part III summons issued | 0 | 0 | 1 |
| # of dogs caught at large | 10 | 18 | 19 |
| # of complaints handled | 186 | 515 | 112 |

February 2019

| # | Incident Date | Incident Type | District | Apparatus | | | Staffing | PRIORITY 1/2 | Dispatch Time | Responding Time | Arrival Time | Total Response Time | Overall Response Time | | | | | | |
|-------------------------------|-------------------|------------------------------------|---------------------|----------------|---------------------|------------|----------|-----------------|---------------|-----------------|--------------|---------------------|-----------------------|--|--|--|--|--|--|
| Bourget Rural | | | | | | | | | | | | | | | | | | | |
| 19-043 | February 3, 2019 | Fire - Vehicle | 1A (Bourget Rural) | Primary | Pumper 1 (Bourget) | 4 FF (Vol) | 1 | 2:04:55 AM | 2:14:11 AM | 2:20:03 AM | 0:15:08 | 0:15:08 | 0:15:08 | | | | | | |
| | | | | First Arriving | Same | | | | 2:14:11 AM | 2:20:03 AM | 0:15:08 | | | | | | | | |
| 19-046 | February 5, 2019 | Medical - Other | 1A (Bourget Rural) | Primary | Squad 1 (Bourget) | 2 FF (Vol) | 1 | 11:17:41 AM | 11:19:47 AM | 11:29:56 AM | 0:12:15 | 0:12:15 | 0:12:15 | | | | | | |
| | | | | First Arriving | Same | | | | 11:19:47 AM | 11:29:56 AM | 0:12:15 | | | | | | | | |
| 19-053 | February 13, 2019 | Vehicle Collision - Medical | 1A (Bourget Rural) | Primary | Pumper 1 (Bourget) | 3 FF (Vol) | 1 | 1:47:51 PM | 1:52:58 PM | 1:55:28 PM | 0:07:37 | 0:07:37 | 0:07:37 | | | | | | |
| | | | | First Arriving | Same | | | | 1:52:58 PM | 1:55:28 PM | 0:07:37 | | | | | | | | |
| 19-055 | February 14, 2019 | Carbon Monoxide - False | 1A (Bourget Rural) | Primary | Pumper 1 (Bourget) | 6 FF (Vol) | 2 | 8:51:35 PM | 9:04:01 PM | 9:06:36 PM | 0:15:01 | 0:15:01 | 0:15:01 | | | | | | |
| | | | | First Arriving | Same | | | | 9:04:01 PM | 9:06:36 PM | 0:15:01 | | | | | | | | |
| 19-058 | February 16, 2019 | Carbon Monoxide - False | 1A (Bourget Rural) | Primary | Pumper 1 (Bourget) | 5 FF (Vol) | 2 | 6:44:07 PM | 6:54:19 PM | 7:03:30 PM | 0:19:23 | 0:19:23 | 0:19:23 | | | | | | |
| | | | | First Arriving | Same | | | | 6:54:19 PM | 7:03:30 PM | 0:19:23 | | | | | | | | |
| 19-062 | February 22, 2019 | Medical - Unconscious | 1A (Bourget Rural) | Primary | Squad 1 (Bourget) | | 1 | 10:13:25 PM | 10:20:31 PM | 10:26:32 PM | 0:13:07 | 0:13:07 | 0:13:07 | | | | | | |
| | | | | First Arriving | Same | | | | 10:20:31 PM | 10:26:32 PM | 0:13:07 | | | | | | | | |
| 19-066 | February 23, 2019 | Fire - Residence | 1A (Bourget Rural) | Primary | Pumper 1 (Bourget) | 1 FF (Vol) | 1 | 8:09:00 PM | 8:18:13 PM | 8:23:36 PM | 0:14:36 | 0:14:10 | 0:14:10 | | | | | | |
| | | | | First Arriving | Tanker 1 (Bourget) | 1 FF (Vol) | 1 | | 8:23:03 PM | 8:23:10 PM | 0:14:10 | | | | | | | | |
| Bourget -Rural | | | | | | | | | | | | | | | | | | | |
| Clarence-Creek Rural | | | | | | | | | | | | | | | | | | | |
| 19-045 | February 3, 2019 | Other | 2A (Clarence Rural) | Primary | Pumper 2 (Clarence) | 4 FF (Vol) | 1 | 11:07:29 PM | 11:17:44 PM | 11:24:22 PM | 0:16:53 | 0:16:53 | 0:16:53 | | | | | | |
| | | | | First Arriving | Same | | | | 11:17:44 PM | 11:24:22 PM | 0:16:53 | | | | | | | | |
| 19-064 | February 25, 2019 | Vehicle Collision - Medical | 2A (Clarence Rural) | Primary | Pumper 3 (Rockland) | 2 FF (FT) | 1 | 2:13:40 PM | 2:16:12 PM | 2:24:17 PM | 0:10:37 | 0:00:01 | 0:00:01 | | | | | | |
| | | | | First Arriving | Car 2 (Deputy) | 1 FF (FT) | 1 | | 2:13:40 PM | 2:13:41 PM | 0:00:01 | | | | | | | | |
| Clarence-Creek Village | | | | | | | | | | | | | | | | | | | |
| Clarence-Creek Rural | | | | | | | | | | | | | | | | | | | |
| Rockland Rural | | | | | | | | | | | | | | | | | | | |
| 19-041 | February 1, 2019 | Fire - Chimney | 3A (Rockland Rural) | Primary | Pumper 3 (Rockland) | 3 FF (Vol) | 1 | 5:56:55 PM | 6:06:50 PM | 6:14:55 PM | 0:18:00 | 0:14:52 | 0:14:52 | | | | | | |
| | | | | First Arriving | Tanker 2 (Clarence) | 2 FF (Vol) | 1 | | 6:02:18 PM | 6:11:47 PM | 0:14:52 | | | | | | | | |
| 19-051 | February 11, 2019 | Medical - VSA | 3A (Rockland Rural) | Primary | Squad 3 (Rockland) | 2 FF (FT) | 1 | 11:06:48 AM | 11:08:02 AM | 11:11:59 AM | 0:05:11 | 0:05:11 | 0:05:11 | | | | | | |
| | | | | First Arriving | Same | | | | 11:08:02 AM | 11:11:59 AM | 0:05:11 | | | | | | | | |
| 19-054 | February 14, 2019 | Vehicle Collision - Spills/Cleanup | 3A (Rockland Rural) | Primary | Pumper 3 (Rockland) | 3 FF (FT) | 1 | 1:06:31 PM | 1:09:09 PM | cancelled | cancelled | 0:04:33 | 0:04:33 | | | | | | |
| | | | | First Arriving | Car 1 (Chief) | 1 FF (FT) | | | 1:07:36 PM | 1:11:04 PM | 0:04:33 | | | | | | | | |
| 19-056 | February 15, 2019 | Medical - Other | 3A (Rockland Rural) | Primary | Squad 3 (Rockland) | 3 FF (Vol) | 1 | 5:13:30 AM | 5:28:37 AM | 5:33:50 AM | 0:20:20 | 0:06:37 | 0:06:37 | | | | | | |
| | | | | First Arriving | Car 1 (Chief) | 1 FF (FT) | 1 | | 5:16:15 AM | 5:20:07 AM | 0:06:37 | | | | | | | | |
| 19-060 | February 19, 2019 | Fire - Residence | 3A (Rockland Rural) | Primary | Pumper 3 (Rockland) | 1 FF (FT) | 1 | 12:03:28 PM | 12:08:42 PM | 12:13:12 PM | 0:09:44 | 0:07:24 | 0:07:24 | | | | | | |
| | | | | First Arriving | Car 2 (Deputy) | 1 FF (FT) | 1 | | 12:06:43 PM | 12:10:52 PM | 0:07:24 | | | | | | | | |
| 19-069 | February 27, 2019 | Carbon Monoxide - False | 3A (Rockland Rural) | Primary | Pumper 3 (Rockland) | 5 FF (Vol) | 2 | 9:25:47 PM | 9:40:06 PM | 9:47:49 PM | 0:22:02 | 0:22:02 | 0:22:02 | | | | | | |
| | | | | First Arriving | Same | | | | 9:40:06 PM | 9:47:49 PM | 0:22:02 | | | | | | | | |
| Rockland Urban | | | | | | | | | | | | | | | | | | | |
| 19-040 | February 1, 2019 | Alarms - Cooking Incident | 3B (Rockland Urban) | Primary | Pumper 3 (Rockland) | | 1 | 8:37:12 AM | cancelled | cancelled | cancelled | 0:01:23 | 0:01:23 | | | | | | |
| | | | | First Arriving | Car 1 (Chief) | 1 FF (FT) | 1 | | 8:37:25 AM | 8:38:35 AM | 0:01:23 | | | | | | | | |
| 19-042 | February 1, 2019 | Carbon Monoxide - Actual | 3B (Rockland Urban) | Primary | Pumper 3 (Rockland) | 5 FF (Vol) | 2 | 10:10:51 PM | 10:20:54 PM | 10:23:03 PM | 0:12:12 | 0:12:12 | 0:12:12 | | | | | | |
| | | | | First Arriving | Same | | | | 10:20:54 PM | 10:23:03 PM | 0:12:12 | | | | | | | | |
| 19-044 | February 5, 2019 | Vehicle Collision - Medical | 3B (Rockland Urban) | Primary | Pumper 3 (Rockland) | 2 FF (FT) | 1 | 3:53:47 PM | 3:56:00 PM | 3:56:44 PM | 0:02:57 | 0:01:45 | 0:01:45 | | | | | | |
| | | | | First Arriving | Car 1 (Chief) | 1 FF (FT) | 1 | | 3:54:47 PM | 3:55:32 PM | 0:01:45 | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

| Incident # | Date | Description | Station Involved | First Arriving | Vehicle | FF (Vol) | Units | Arrival Time | Departure Time | Duration | |
|------------|-------------------|-----------------------------|---------------------|----------------|---------------------|------------|-------|--------------|----------------|----------|---------|
| 19-051 | February 13, 2019 | Medical - Unconscious | 3B (Rockland Urban) | Primary | Tanker 2 (Clarence) | 2 FF (Vol) | 1 | 2:10:57 PM | 5:46:45 PM | 0:17:02 | 0:02:00 |
| | | | | First Arriving | Squad 3 (Rockland) | 3 FF (FT) | 1 | | 2:11:36 PM | 0:03:24 | |
| 19-057 | February 15, 2019 | Alarms - Cooking Incident | 3B (Rockland Urban) | Primary | Car 2 (Deputy) | 1 FF (FT) | 1 | 8:48:40 AM | 2:12:15 PM | 0:02:00 | 0:04:28 |
| | | | | First Arriving | Pumper 3 (Rockland) | 2 FF (FT) | 1 | | 8:51:02 AM | 0:04:51 | |
| 19-059 | February 17, 2019 | Carbon Monoxide - False | 3B (Rockland Urban) | Primary | Car 1 (Chief) | 1 FF (Vol) | 1 | 4:47:56 | 8:49:59 AM | 0:04:28 | 0:19:20 |
| | | | | First Arriving | Squad 3 (Rockland) | 2 FF (Vol) | 2 | | 5:02:28 AM | 0:19:20 | |
| 19-061 | February 19, 2019 | Vehicle Collision - Medical | 3B (Rockland Urban) | Primary | Same | | | 16:18:42 | 5:02:28 AM | 0:19:20 | 0:02:20 |
| | | | | First Arriving | Squad 3 (Rockland) | 3 FF (FT) | 1 | | 4:20:51 PM | 0:02:20 | |
| 19-063 | February 24, 2019 | Fire - Residence | 3B (Rockland Urban) | Primary | Same | | | 18:10:23 | 4:20:33 PM | 0:02:20 | 0:05:03 |
| | | | | First Arriving | Pumper 3 (Rockland) | 6 FF (Vol) | 1 | | 4:21:02 PM | 0:02:20 | |
| 19-065 | February 26, 2019 | Other | 3B (Rockland Urban) | Primary | Car 3 (Prevention) | 1 FF (FT) | 2 | 9:31:31 | 6:17:38 PM | 0:13:10 | 0:03:15 |
| | | | | First Arriving | Same | | | | 6:23:33 PM | 0:05:03 | |
| 19-067 | February 25, 2019 | Carbon Monoxide - False | 3B (Rockland Urban) | Primary | Rescue 3 (Rockland) | 4 FF (Vol) | 2 | 14:37:07 | 9:31:31 AM | 0:03:15 | 0:04:36 |
| | | | | First Arriving | Same | | | | 9:34:46 AM | 0:04:36 | |
| 19-068 | February 26, 2019 | Other | 3B (Rockland Urban) | Primary | Rescue 3 (Rockland) | 2 FF (FT) | 1 | 11:36:44 | 2:37:37 PM | 0:04:36 | 0:01:28 |
| | | | | First Arriving | Same | | | | 2:41:43 PM | 0:01:28 | |
| 19-070 | February 27, 2019 | Other | 3B (Rockland Urban) | Primary | Pumper 3 (Rockland) | 3 FF (Vol) | 2 | 16:02:57 | 11:36:45 AM | 0:01:28 | 0:17:25 |
| | | | | First Arriving | Car 3 (Prevention) | 1 FF (FT) | | | 11:38:12 AM | 0:22:15 | |

PLANNING AND CONSTRUCTION DEPARTMENT
Construction Division

| Month / Mois | Total of building permits issued / Total des permis de construction émis | Total permits issued Rockland / Total permis émis Rockland | Total permits issued Villages / Total permis émis villages | Total value of all construction / Total valeur de la construction | # residential units in Rockland / # unités résidentielles - Rockland | # residential units in rural / # unités résidentielles - rural | # residential units in villages / # unités résidentielles - villages | Total of all residential units / Total des unités résidentielles | Residential permit fees / Frais de permis résidentiels | # of commercial permits Rockland / # de permis commerciaux Rockland | # of commercial permits Clarence / # de permis commerciaux Clarence | Total number of all commercial permits / Nombre total de permis commerciaux | Commercial permit fees / Frais pour permis commerce | Total value of commercial construction / Valeur total pour construction commerciale | |
|------------------------------|---|---|---|--|---|---|---|---|---|--|--|--|--|--|-----------------|
| January | 9 | 6 | 0 | 3 | \$ 1,572,600.00 | 5 | 1 | 0 | 6 | \$ 22,246.00 | 0 | 0 | 0 | \$ - | |
| February | 18 | 12 | 2 | 4 | \$ 6,163,553.00 | 11 | 1 | 0 | 12 | \$ 23,786.80 | 2 | 2 | 4 | \$ 2,529.60 | \$ 3,450,000.00 |
| March | | | | | | | | | | | | | | | |
| April | | | | | | | | | | | | | | | |
| May | | | | | | | | | | | | | | | |
| June | | | | | | | | | | | | | | | |
| July | | | | | | | | | | | | | | | |
| August | | | | | | | | | | | | | | | |
| September | | | | | | | | | | | | | | | |
| October | | | | | | | | | | | | | | | |
| November | | | | | | | | | | | | | | | |
| December | | | | | | | | | | | | | | | |
| Total | 27 | 18 | 2 | 7 | \$ 7,736,153.00 | 16 | 2 | 0 | 18 | \$ 46,032.80 | 2 | 2 | 4 | \$ 2,529.60 | \$ 3,450,000.00 |
| COMPARAISON WITH 2018 | | | | | | | | | | | | | | | |
| Jan-Feb 18 | 29 | 20 | 5 | 4 | \$ 3,468,551.08 | 9 | 1 | 1 | 11 | \$ 20,976.60 | 3 | 3 | 6 | \$ 1,575.90 | \$ 243,500.00 |
| Fev 18 | 21 | 16 | 4 | 1 | \$ 2,042,551.08 | 8 | 0 | 0 | 8 | \$ 15,380.40 | 3 | 3 | 6 | \$ 1,575.90 | \$ 243,500.00 |

28 FEV 2019